

Module 1 : Conduction

Lecture 7 : 1D unsteady conduction (contd.)

Objectives

In this class:

- The solution to the 1D transient problem is completed. A general procedure obtaining the orthogonal functions required for completion of the solution is discussed.
- A 'fuzzy' argument is developed for justifying the the $Bi < 0.1$ 'rule of the thumb' for using the lumped model.

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- Simplification of the equⁿ (6.32) therefore yields:

$$\lambda \tan \lambda = Bi \Rightarrow \cot \lambda = \frac{\lambda}{Bi} \tag{7.1}$$

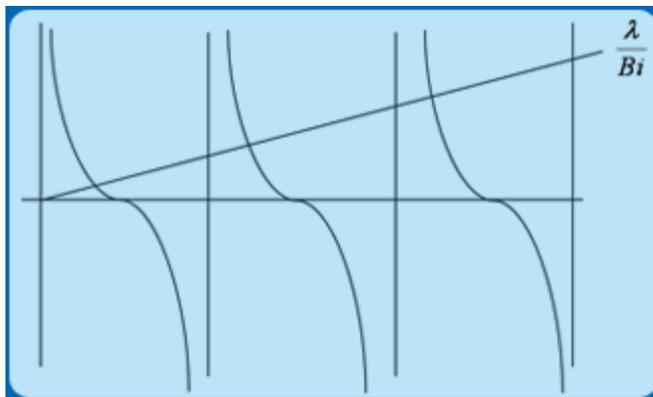
- Need to find out the roots of this equation
- Graphically plot the following curves:

$$y = \cot \lambda; y = \frac{\lambda}{Bi}$$

- Intersection of the curves gives the roots of the equation (7.1)

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- The graphical procedure explained on the previous slide is shown below:



e.g. $Bi = 0.1$

$$\lambda_1 = 0.31$$

$$\lambda_2 = 3.17$$

$$\lambda_3 = 6.3$$

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- Can directly use a root finding routine to solve equⁿ (7.1) without the above graphical method.

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- The λ s have been obtained but still one constant 'A' is to be determined and a condition (equⁿ (6.23)) available. Using this gives:

$$1 = Ae^{-\lambda^2 t^*} \cos \lambda x^* \Big|_{t^*=0} \tag{7.2}$$

- Just like in the previous 2D steady conduction problem a single λ and A will not satisfy the condition and therefore attempt a series solution.

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- The solution is therefore assumed as:

$$\theta^* = \sum A_n e^{-\lambda_n^2 t^*} \cos \lambda_n x^* \quad (7.3)$$

- Use the initial condition to get:

$$1 = \sum_1^{\infty} A_n \cos \lambda_n x^* \quad (7.4)$$

- Recall that in the previous case a trigonometric identity given by equⁿ (6.12) was used to obtain the solution. If λ_n s were integer constants the identity would be useful here.

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- However λ_n s are fractions ($Bi = 0.1$, $\lambda_1 = 0.31$, $\lambda_2 = 3.17$ etc.). Therefore try to see if the methodology used earlier will work for this situation also.
- The idea is to see if the series solution can be manipulated so that the constants can be easily evaluated i.e. many terms become zero and only a single term remains that can be used to evaluate the constant. We now look at a generalized procedure for this.

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- Look again at the original differential equⁿ and boundary conditions (6.27), (6.29), (6.31):

$$F'' + \lambda^2 F = 0; \quad (7.5)$$

$$F'|_{x^*=1} = -BiF'|_{x^*=1}; F'|_{x^*=0} = 0. \quad (7.6)$$

- Let F_m and F_n be solutions corresponding to the solutions λ_m , λ_n which will satisfy the above equations. Therefore:

$$F_m'' + \lambda_m^2 F_m = 0 \quad (7.7)$$

$$F_n'' + \lambda_n^2 F_n = 0 \quad (7.8)$$

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- Multiply equⁿ(7.5) with F_n and equⁿ(7.6) with F_m :

$$F_m'' + \lambda_m^2 F_m = 0 \quad \times F_n \quad (7.9)$$

$$F_n'' + \lambda_n^2 F_n = 0 \quad \times F_m \quad (7.10)$$

- Subtract equⁿ (7.10) from (7.9) to get:

$$F_m'' F_n - F_n'' F_m + (\lambda_m^2 - \lambda_n^2) F_m F_n = 0$$

- Rewrite the above equⁿ to get:

$$\frac{d}{dx} (F_m' F_n - F_n' F_m) + (\lambda_m^2 - \lambda_n^2) F_m F_n = 0 \quad (7.11)$$

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- Now integrate the equⁿ (7.9) between 0 and 1 to get:

$$\begin{aligned}
& (F_m' F_n - F_n' F_m) \Big|_0^1 + (\lambda_m^2 - \lambda_n^2) \int_0^1 F_m F_n dx^* = 0 \\
& (F_m' F_n - F_n' F_m) \Big|_1 - (F_m' F_n - F_n' F_m) \Big|_0 \\
& \quad + (\lambda_m^2 - \lambda_n^2) \int_0^1 F_m F_n dx^* = 0
\end{aligned} \tag{7.12}$$

- Since F_m and F_n are solutions to the equations (7.5) and (7.6):

$$\begin{aligned}
F_m \Big|_{x^*=1} &= -Bi F_m \Big|_{x^*=1}; F_m \Big|_{x^*=0} = 0 \\
F_n \Big|_{x^*=1} &= -Bi F_n \Big|_{x^*=1}; F_n \Big|_{x^*=0} = 0
\end{aligned} \tag{7.13}$$

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- Using equⁿ (7.13) in equⁿ (7.12) gives:

$$\begin{aligned}
& (-Bi F_m F_n + Bi F_n F_m) \Big|_1 - (0 - 0) = (\lambda_n^2 - \lambda_m^2) \int_0^1 F_m F_n dx^* \\
\Rightarrow 0 &= (\lambda_n^2 - \lambda_m^2) \int_0^1 F_m F_n dx^*
\end{aligned} \tag{7.14}$$

- For $\lambda_m = \lambda_n$ the integral in the equⁿ (7.14) is of the 0/0 form and approaches a finite value whereas for $\lambda_m \neq \lambda_n$ the integral in equⁿ (7.14) is zero i.e.: $\int_0^1 F_m F_n dx^* = 0$ for $\lambda_m \neq \lambda_n$

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- Recall that for the present situation F_m and F_n are $\cos(\lambda_m x)$ and $\cos(\lambda_n x)$ respectively.
- Now return to the solution of the unsteady problem: (equⁿ (7.4))

$$1 = \sum_1^{\infty} A_n \cos \lambda_n x^*$$

- Use the property of the functions just derived to proceed to evaluate the unknown constants A_n .

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- Multiply both sides with $\cos(\lambda_n x)$ and integrate:

$$\begin{aligned}
\int_0^1 1 \cdot \cos \lambda_m x^* dx^* &= \sum_1^{\infty} \int_0^1 A_n \cos \lambda_n x^* \cos \lambda_m x^* dx^* \\
\Rightarrow \frac{\sin \lambda_m}{\lambda_m} &= A_m \int_0^1 \cos^2 \lambda_m x^* dx^* = \frac{A_m}{2} \int_0^1 [1 + \cos 2\lambda_m x^*] dx^* \\
&= \frac{A_m}{2} \left[x^* + \frac{\sin 2\lambda_m x^*}{2\lambda_m} \right]_0^1 \\
\Rightarrow A_m &= \frac{2 \sin \lambda_m}{\lambda_m + \sin \lambda_m \cos \lambda_m}
\end{aligned} \tag{7.15}$$

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- Final solution is (equⁿ (7.3) earlier obtained) :

$$\theta^* = \sum_1^{\infty} A_m e^{-\lambda_m^2 t^*} \cos \lambda x^* \quad (7.3)$$

- Where:

$$\theta^* = \frac{\theta}{\theta_i} = \frac{T - T_{\infty}}{T_i - T_{\infty}}; x^* = \frac{x}{L}; t^* = \frac{t}{t_0}$$

$$A_m = \frac{2 \sin \lambda_m}{\lambda_m + \sin \lambda_m \cos \lambda_m}$$

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- Note that once again the summation solution was obtained just like in the 2D case with two space dimensions. Here we had to look at the differential equation to obtain a methodology for determining the constants of the infinite series since the solution was not obtainable from trigonometry. This is a generalized methodology and would have worked even for the earlier case.

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- For $t^* > 0.2$ the full series can be approximated by the first term with little error. Therefore:

$$\theta^* = A_1 e^{-\lambda_1^2 t^*} \cos \lambda x^*$$

$$\theta^* = \theta_0^* \cos \lambda x^*$$

- θ_0^* is the mid plane temperature and is a function of time only.
- At $x^*=1$, $\theta^* = \theta_0^* \cos \lambda$ which is the temperature variation at the boundary of the slab.

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- Let the temperature of the end of the slab be always 95 % of the centerline value. Then:

$$\cos \lambda = 0.95 \Rightarrow \lambda = 0.32$$

- Using equⁿ (7.1):

$$\cot \lambda = \lambda / Bi \Rightarrow Bi = 0.1$$

- Thus a Biot number of 0.1 results in a temperature difference of 5 % between the center and one end of the slab.

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- If this 5 % variation is ignored then the temperature between the center and the boundary can be assumed to be the same which is the lumped approach (zero dimension). Therefore if the $Bi < 0.1$ the lumped approach can be used and this approximation yields quick and reasonably accurate results. We have not proved anything only demonstrated the 'thumb rule'.

Recap

In this class:

- The solution to the 1D transient problem is completed. A general procedure obtaining the orthogonal functions required for completion of the solution is discussed.
- A 'fuzzy' argument is developed for justifying the the $Bi < 0.1$ 'rule of the thumb' for using the lumped model.