

Wave Propagation for communication

- 1) Bridge course \rightarrow 1st semester M.Tech./M.S./Ph.D.
- 2) Recommended Text \rightarrow R.K. Shergaonkar
Matthew N.O. Sadiku

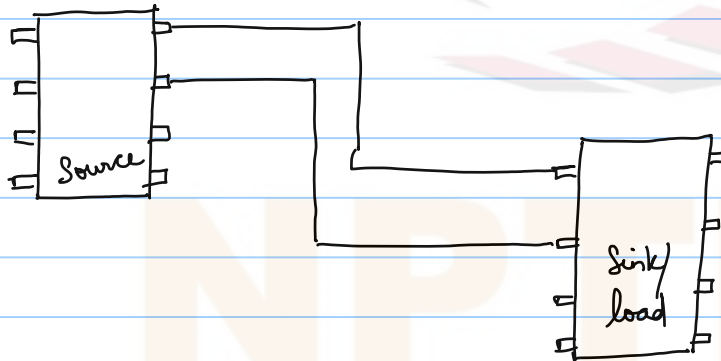
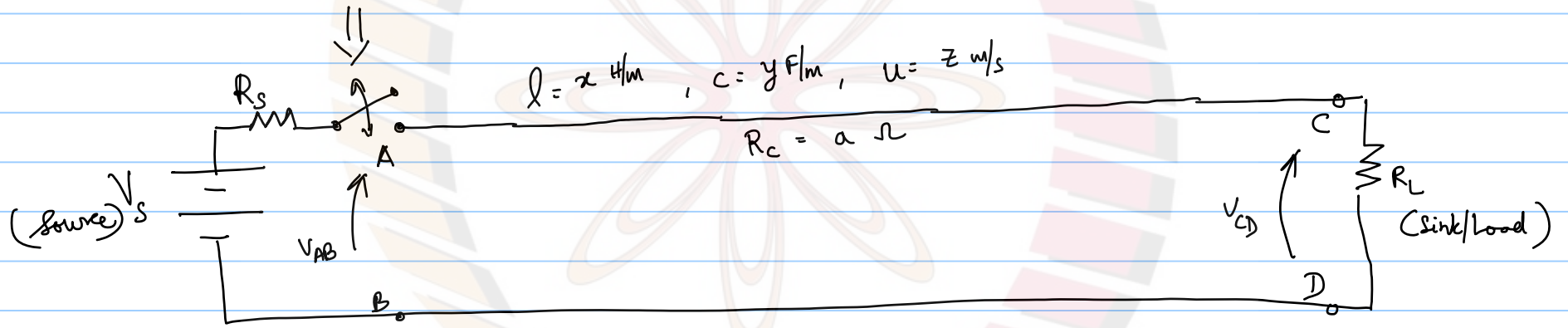
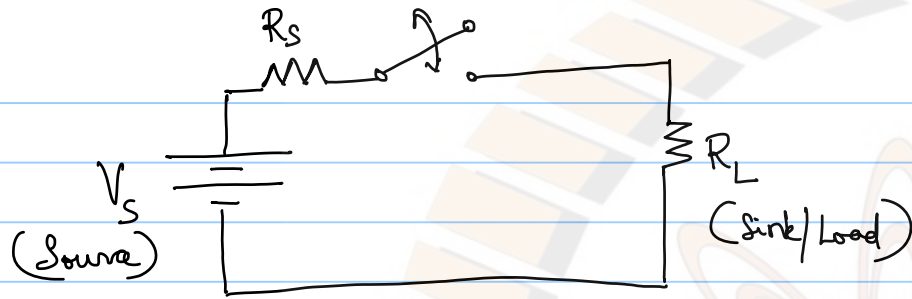
- 3) Quiz - 1 (50 minutes) \rightarrow 15 marks
Quiz - 2 (") \rightarrow 25 marks
Final exam (180 minutes) \rightarrow 50 marks
Homeworks \rightarrow 10 marks

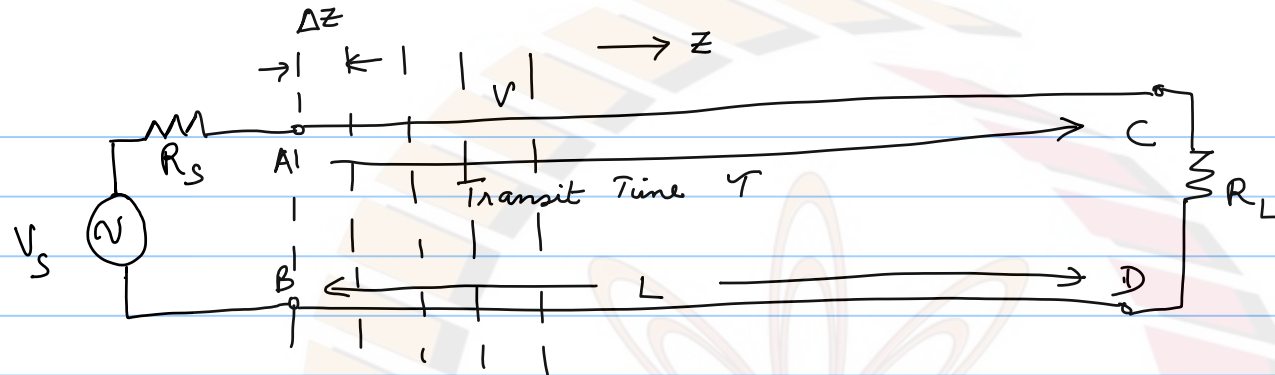
- 4) TA_s \rightarrow 1) Ankit Arora
2) Pratyush Pushkar
3) Nirjhar Kumar

- 5) Transmission Lines & Waves

NPTTEL

1)





$$\text{Transit time } \tau = \frac{L}{v}$$

(i) Frequency of source V_S is very low (f_s)

$$v = \downarrow f_s \lambda_s$$

$$\Rightarrow \lambda_s \uparrow$$

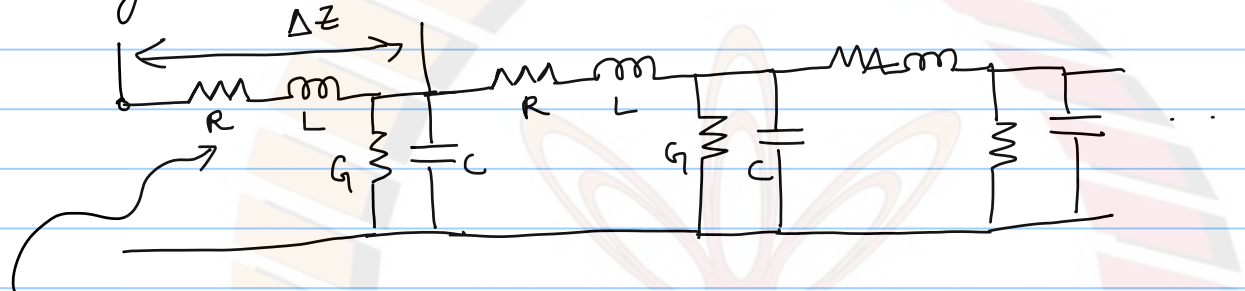
Low frequency circuit analysis could be used.

(ii) Frequency of source V_S to be high,

$$v = \uparrow f_s \lambda_s$$

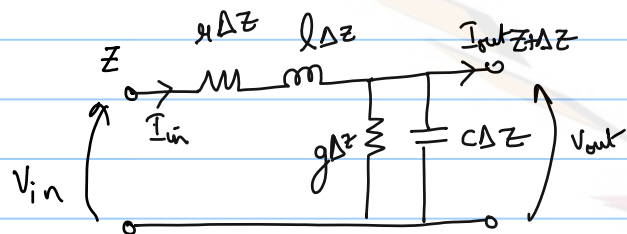
$$\Rightarrow \lambda_s \downarrow$$

Phenomenological model :-



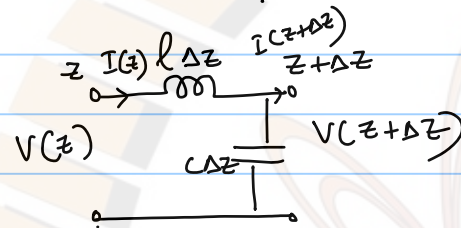
Distributed Resistance $\Rightarrow R = r \Delta z \leftarrow m$
 $\hookrightarrow \Omega/m$

Distributed Inductance $\Rightarrow L = l \Delta z \hookrightarrow H/m$
 $\parallel rly \quad G = g \Delta z \leftarrow s/m$
 $C = c \Delta z \hookrightarrow F/m$



Assume $r = 0$
 & $g = 0$ } Lossless approximation

Lossless Transmission Line:-



KVL,

$$V(z) - (l\Delta z) \frac{dI}{dt} - V(z + \Delta z) = 0$$

$$V(z) - (l\Delta z) \frac{\partial I}{\partial t} - V(z + \Delta z) = 0$$

$$V(z + \Delta z) - V(z) = -l\Delta z \frac{\partial I}{\partial t}$$

$$\Rightarrow \frac{V(z + \Delta z) - V(z)}{\Delta z} = -l \frac{\partial I}{\partial t}$$

If $\Delta z \rightarrow 0$,

$$\boxed{\frac{\partial V}{\partial z} = -l \frac{\partial I}{\partial t}}$$

KCL,

$$I(z) - C \Delta z \frac{\partial V}{\partial t} - I(z + \Delta z) = 0$$

$$\Rightarrow \frac{I(z + \Delta z) - I(z)}{\Delta z} = -C \frac{\partial V}{\partial t}$$

$\Delta z \rightarrow 0,$

$$\boxed{\frac{\partial I}{\partial z} = -C \frac{\partial V}{\partial t}}$$

Telegrapher's equations.

NPTTEL

i)

$$\frac{\partial V}{\partial z} = -l \frac{\partial I}{\partial t}$$

$$\frac{\partial I}{\partial z} = -c \frac{\partial V}{\partial t}$$

$$\begin{aligned} \rightarrow \frac{\partial^2 V}{\partial z^2} &= -l \frac{\partial}{\partial z} \left(\frac{\partial I}{\partial t} \right) \\ &= -l \frac{\partial}{\partial t} \left(\frac{\partial I}{\partial z} \right) \\ &= -l \frac{\partial}{\partial t} (-c) \frac{\partial V}{\partial t} \end{aligned}$$

$$\boxed{\frac{\partial^2 V}{\partial z^2} = lc \frac{\partial^2 V}{\partial t^2}}$$

Dimensional analysis \Rightarrow LHS units V/m^2
RHS units

$$\Rightarrow lc = \frac{1}{v^2} \frac{\partial^2 V}{\partial t^2} \rightarrow v/s^2$$

$u \rightarrow$ velocity (m/s)

$$\hookrightarrow \frac{1}{\sqrt{\mu\epsilon}}$$

11th dy,

$$\boxed{\frac{\partial^2 I}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 I}{\partial t^2}}$$

$$\boxed{\frac{\partial^2 V}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 V}{\partial t^2}}$$

wave equations

General Solution:-

$$V(z, t) = f^+ \left(t - \frac{z}{u} \right) + f^- \left(t + \frac{z}{u} \right)$$

\nwarrow forward \swarrow Backward

If $V(z, t) = f^+ \left(t - \frac{z}{u} \right)$

$$\frac{\partial V}{\partial z} = \frac{\partial}{\partial z} \left[f^+ \left(t - \frac{z}{u} \right) \right]$$

$$\text{Let } t - \frac{z}{u} = s$$

$$\Rightarrow \frac{\partial s}{\partial z} = -\frac{1}{u}$$

$$\begin{aligned} \frac{\partial V}{\partial z} &= \frac{\partial}{\partial z} (f^+(s)) \\ &= \frac{\partial f^+(s)}{\partial s} \frac{\partial s}{\partial z} \\ &= -\frac{1}{u} \frac{\partial f^+(s)}{\partial s} \end{aligned}$$

$$\begin{aligned} \text{Now, } \frac{\partial^2 V}{\partial z^2} &= \frac{\partial}{\partial z} \left(-\frac{1}{u} \frac{\partial f^+(s)}{\partial s} \right) \\ &= -\frac{1}{u} \frac{\partial}{\partial z} \left(\frac{\partial f^+(s)}{\partial s} \right) \\ &= -\frac{1}{u} \frac{\partial^2 f^+(s)}{\partial s^2} \frac{\partial s}{\partial z} \\ &= \frac{1}{u^2} \frac{\partial^2 f^+(s)}{\partial s^2} = \frac{1}{u^2} \frac{d^2}{ds^2} f^+(s) \end{aligned}$$

RHS of voltage wave equation,

$$\frac{1}{u^2} \frac{\partial^2 V}{\partial t^2} = \frac{1}{u^2} \frac{\partial^2}{\partial t^2} (f^+(s))$$

$$s = t - \frac{z}{u}$$

$$\frac{\partial s}{\partial t} = 1$$

$$\text{RHS} = \frac{1}{u^2} \frac{\partial^2}{\partial t^2} f^+(s)$$

$$= \frac{1}{u^2} \frac{\partial}{\partial t} \left(\frac{\partial}{\partial t} f^+(s) \right)$$

$$= \frac{1}{u^2} \frac{\partial}{\partial t} \left(\frac{\partial f^+(s)}{\partial s} \frac{\partial s}{\partial t} \right)$$

$$= \frac{1}{u^2} \frac{\partial^2 f^+(s)}{\partial s^2}$$

$$= \frac{1}{u^2} \frac{d^2 f^+(s)}{ds^2}$$

$$V(z, t) = f^+ \left(t - \frac{z}{u} \right)$$

$$\text{Let } u = 1 \text{ m/s}$$

$$\Rightarrow S = 1 - \frac{0}{1} = 1$$

$$\text{Let at } t = 1 \text{ s, } z = 0 \text{ m}$$

Then at $t = 2 \text{ s}$, what is z ?

$$t - \frac{z}{u} \Rightarrow 2 - \frac{z}{1} = S$$

$$= z = 2 - S = 2 - 1 = 1 \text{ m}$$

$$\text{Given: } V(z, t) = f^+ \left(t - \frac{z}{u} \right)$$

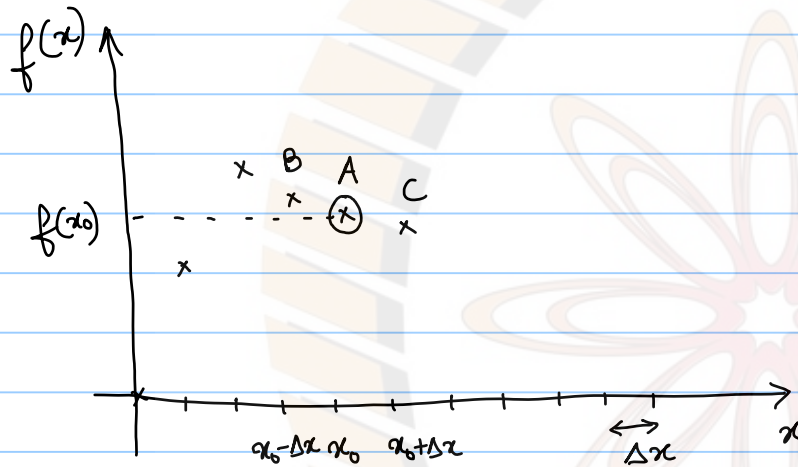
$$\frac{\partial V}{\partial z} = -L \frac{\partial I}{\partial t} \Rightarrow I(z, t) = \frac{1}{L u} f^+ \left(t - \frac{z}{u} \right)$$

↑
units of resistance

$$L u = L \frac{1}{\sqrt{L C}} = \sqrt{\frac{L}{C}} \Omega \quad (\text{Characteristic Resistance})$$

$$= R_c$$

Introduction to Finite Differences :-



$$1) \quad f(x_0 + \Delta x) = f(x_0) + \frac{\Delta x}{1!} f'(x_0) + \frac{\Delta x^2}{2!} f''(x_0) + \frac{\Delta x^3}{3!} f'''(x_0) + \dots \quad \text{--- (1)}$$

$$\Rightarrow \quad \frac{\Delta x}{1!} f'(x_0) = f(x_0 + \Delta x) - f(x_0) - \frac{\Delta x^2}{2!} f''(x_0) - \frac{\Delta x^3}{3!} f'''(x_0) + \dots \quad \Delta x \rightarrow \text{small}$$

$$\Rightarrow \quad f'(x_0) \cong \frac{f(x_0 + \Delta x) - f(x_0)}{\Delta x}$$

$$O(E) \cong \frac{\Delta x^2}{2! (\Delta x)} \\ \cong \frac{\Delta x}{2}$$

Forward Differencing -

$$2) \quad f(x_0 - \Delta x) = f(x_0) - \frac{\Delta x}{1!} f'(x_0) + \frac{\Delta x^2}{2!} f''(x_0) - \frac{\Delta x^3}{3!} f'''(x_0) + \dots \quad \text{--- (2)}$$

$$\Rightarrow \frac{\Delta x}{1!} f'(x_0) = f(x_0) - f(x_0 - \Delta x) + \frac{\Delta x^2}{2!} f''(x_0) - \frac{\Delta x^3}{3!} f'''(x_0) + \dots$$

$$\Rightarrow f'(x_0) \cong \frac{f(x_0) - f(x_0 - \Delta x)}{\Delta x} \quad O(E) \cong \frac{\Delta x^2}{2! (\Delta x)} \cong \frac{\Delta x}{2}$$

Backward Differencing.

$$3) \quad \textcircled{1} - \textcircled{2},$$

$$f(x_0 + \Delta x) - f(x_0 - \Delta x) = \frac{2\Delta x}{1!} f'(x_0) + \frac{2\Delta x^3}{3!} f'''(x_0) + \dots$$

$$\Rightarrow \frac{2\Delta x}{1!} f'(x_0) \cong f(x_0 + \Delta x) - f(x_0 - \Delta x)$$

$$\Rightarrow f'(x_0) \cong \frac{f(x_0 + \Delta x) - f(x_0 - \Delta x)}{2\Delta x} \quad \rightarrow \quad O(E) \cong \frac{2\Delta x^3}{3! (2\Delta x)} \cong \frac{\Delta x^2}{6}$$

Central Differencing

4) ① + ②,

$$f(x_0 + \Delta x) + f(x_0 - \Delta x) = 2f(x_0) + \frac{2\Delta x^2}{2!} f''(x_0) + \frac{2\Delta x^4}{4!} f^{(4)}(x_0) + \dots$$

$$\Rightarrow \frac{2\Delta x^2}{2!} f''(x_0) = f(x_0 + \Delta x) + f(x_0 - \Delta x) - 2f(x_0) - \frac{2\Delta x^4}{4!} f^{(4)}(x_0) - \dots$$

$$\Rightarrow f''(x_0) \cong \frac{f(x_0 + \Delta x) + f(x_0 - \Delta x) - 2f(x_0)}{\Delta x^2}$$

$$O(E) \cong \frac{2\Delta x^4}{4! \Delta x^2} \\ \cong \frac{\Delta x^2}{12}$$

3) $\frac{d^2 V}{dx^2} = 0$ (Laplace's equation)

$$\Rightarrow V(x_0 + \Delta x) + V(x_0 - \Delta x) - 2V(x_0) = 0$$

$$\Rightarrow V(x_0) = \frac{V(x_0 + \Delta x) + V(x_0 - \Delta x)}{2}$$

4) If x & y are independent variables & $v(x, y)$,

$$\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} = 0$$

$$\frac{\partial^2 v}{\partial x^2} \approx \frac{f(x_0 + \Delta x, y_0) + f(x_0 - \Delta x, y_0) - 2f(x_0, y_0)}{\Delta x^2} \quad \text{--- (a)}$$

$$\frac{\partial^2 v}{\partial y^2} \approx \frac{f(x_0, y_0 + \Delta y) + f(x_0, y_0 - \Delta y) - 2f(x_0, y_0)}{\Delta y^2} \quad \text{--- (b)}$$

$$\text{Let } \Delta x = \Delta y = h,$$

$$(a) + (b) = 0$$

$$f(x_0 + \Delta x, y_0) + f(x_0 - \Delta x, y_0) - 2f(x_0, y_0) + f(x_0, y_0 + \Delta y) + f(x_0, y_0 - \Delta y) - 2f(x_0, y_0) = 0$$

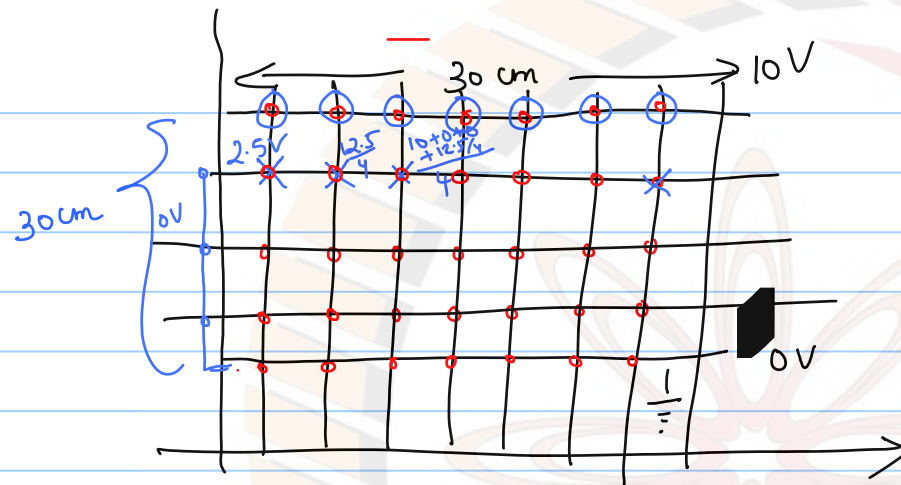
$$4 V(x_0, y_0) = V(x_0 + \Delta x, y_0) + V(x_0 - \Delta x, y_0) + V(x_0, y_0 + \Delta y) + V(x_0, y_0 - \Delta y)$$

$$\Rightarrow V(x_0, y_0) = \frac{1}{4} [V(x_0, y_0 + \Delta y) + V(x_0, y_0 - \Delta y) + V(x_0 + \Delta x, y_0) + V(x_0 - \Delta x, y_0)]$$

$$\begin{array}{ccc} x & \bullet & x \\ (x_0 - \Delta x, y_0) & (x_0, y_0) & (x_0 + \Delta x, y_0) \end{array}$$

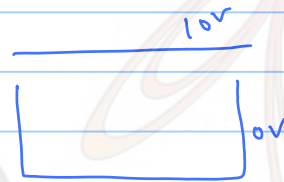
$$\begin{array}{c} x \\ (x_0, y_0 - \Delta y) \end{array}$$

5)



$$V(30, 30) = \text{Zeros}$$

$$V(\text{at all } x, 30) = 10$$



$$\frac{\partial V}{\partial x} = 0; \text{ Neumann condition}$$

$$\frac{\partial^2 V}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 V}{\partial t^2}$$

Here, there are 2 independent variables.

$$\frac{V(z_0 + \Delta z, t_0) + V(z_0 - \Delta z, t_0) - 2V(z_0, t_0)}{\Delta z^2} = \frac{1}{\Delta t^2 u^2} \left\{ \begin{aligned} &V(z_0, t_0 + \Delta t) \\ &+ V(z_0, t_0 - \Delta t) \\ &- 2V(z_0, t_0) \end{aligned} \right\}$$

$$\Rightarrow V(z_0, t_0 + \Delta t) = -V(z_0, t_0 - \Delta t) + 2V(z_0, t_0) + \frac{u^2 \Delta t^2}{\Delta z^2} \left\{ \begin{aligned} &V(z_0 + \Delta z, t_0) + \\ &V(z_0 - \Delta z, t_0) \\ &- 2V(z_0, t_0) \end{aligned} \right\}$$

NPTTEL

$$1) \quad \text{Let } v(z, t) = f^-\left(t + \frac{z}{u}\right)$$

$$\frac{\partial v}{\partial z} = -\ell \frac{\partial I}{\partial t}$$

$$\text{Let } s = t + \frac{z}{u}, \quad f^-(s) \Rightarrow f^-$$

$$\rightarrow \text{LHS} \Rightarrow \frac{\partial v}{\partial z} = \frac{dv}{ds} \frac{\partial s}{\partial z} = \frac{df^-}{ds} \left(\frac{1}{u}\right)$$

RHS

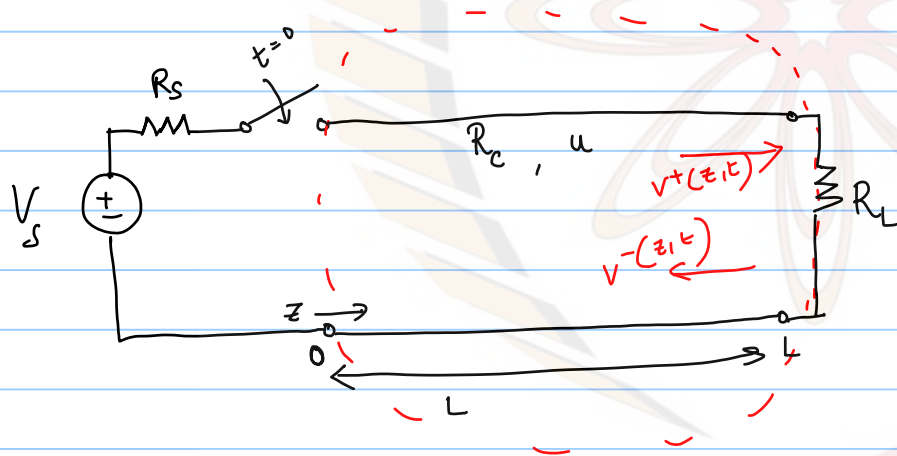
$$\frac{\partial I}{\partial t} = \frac{dI}{ds} \frac{\partial s}{\partial t} = \frac{dI}{ds} (1) = \frac{dI}{ds}$$

$$\underline{\text{LHS} = \text{RHS}} \Rightarrow \frac{df^-}{ds} \left(\frac{1}{u}\right) = -\ell \frac{dI}{ds}$$

$$\Rightarrow I = \frac{-1}{\ell u} f^-(s) \Rightarrow \frac{-1}{\ell u} f^-\left(t + \frac{z}{u}\right)$$

$$I = \frac{-1}{R_c} f^-\left(t + \frac{z}{u}\right)$$

$$= \frac{-1}{R_c} V(z, t)$$



$$V(z, t) = V^+(z, t) + V^-(z, t)$$

$$I(z, t) = \frac{1}{R_c} V^+(z, t) - \frac{1}{R_c} V^-(z, t)$$

Reflection coefficient " Γ " = $\frac{V^-}{V^+}$

At $z = L$,

$$V(L, t) = R_L (I(L, t))$$

$$V^+(L, t) + V^-(L, t) = R_L \left[\frac{1}{R_c} V^+(L, t) - \frac{1}{R_c} V^-(L, t) \right]$$

Rearranging this equation,

$$V^- = \left(\frac{R_L - R_c}{R_L + R_c} \right) V^+$$

Voltage Reflection coefficient at the load end,

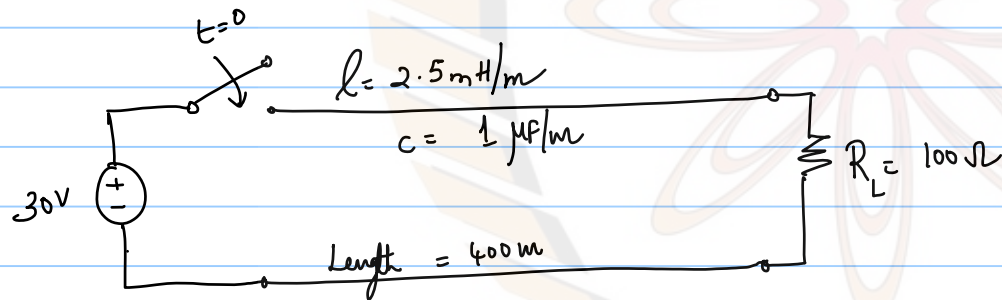
$$\Gamma_{z=L} = \frac{R_L - R_c}{R_L + R_c}$$

If $R_L \gg R_c$, $\Gamma_L \approx \frac{R_L}{R_L} \approx 1$

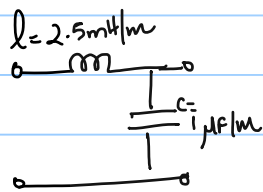
If $R_L \ll R_c$, $\Gamma_L \approx -1$

If $R_L = R_c$, $\Gamma_L = 0$

1)



Solu:-



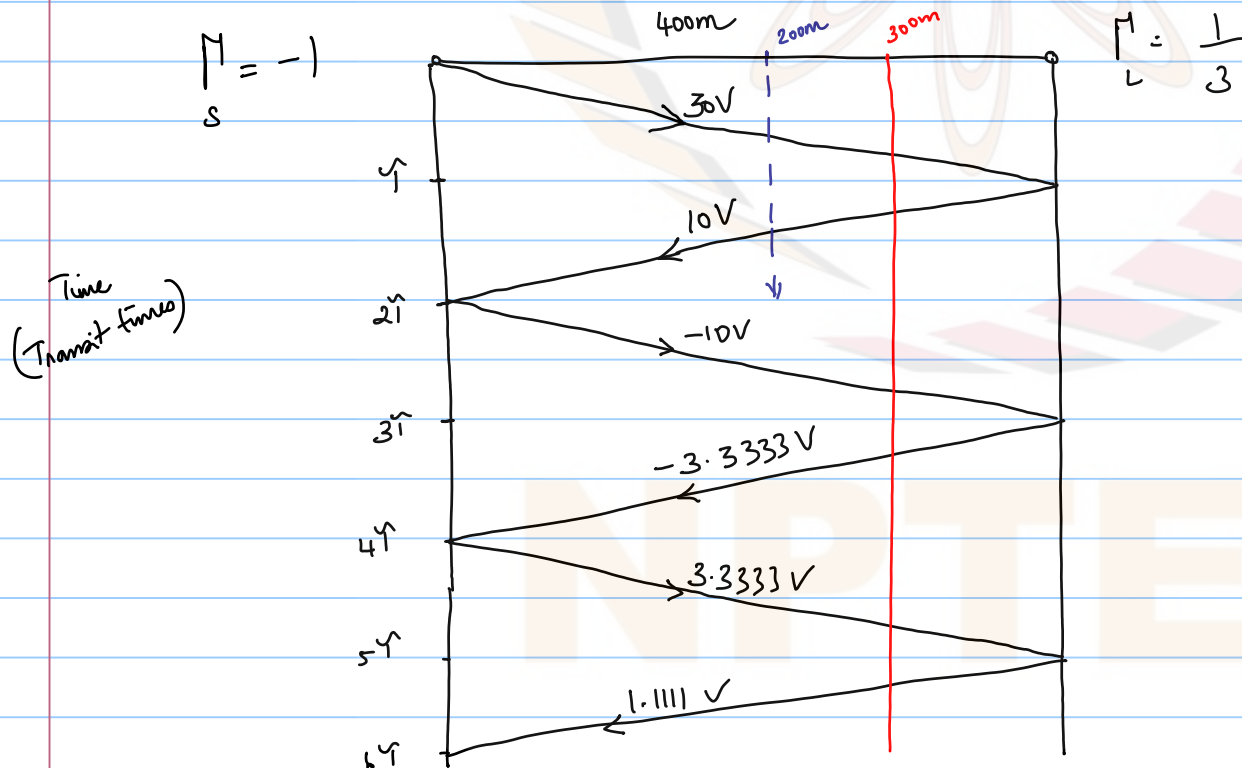
$$u = \frac{1}{\sqrt{lc}} = \frac{1}{\sqrt{2.5 \times 10^{-3} \times 1 \times 10^{-6}}} = 2 \times 10^4 \text{ m/s}$$

$$\gamma = \frac{L}{u} = \frac{400 \text{ m}}{2 \times 10^4 \text{ m/s}} = 2 \times 10^{-2} \text{ s}$$

$$\Gamma_L = \frac{R_L - R_C}{R_L + R_C} = \frac{100 - 50}{100 + 50} = \frac{1}{3}$$

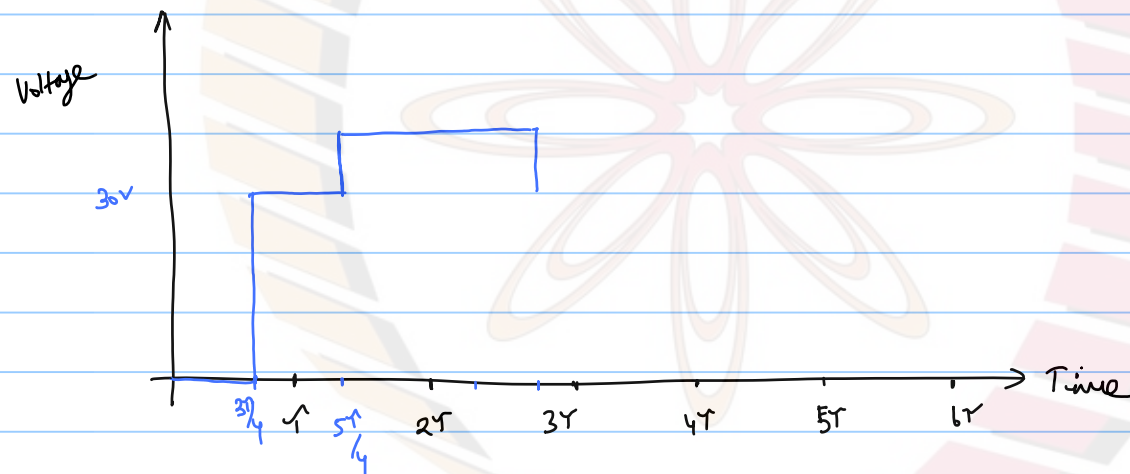
$$\Gamma_S = \frac{R_S - R_C}{R_S + R_C} = \frac{0 - 50}{0 + 50} = -1$$

Bounce Diagram:-



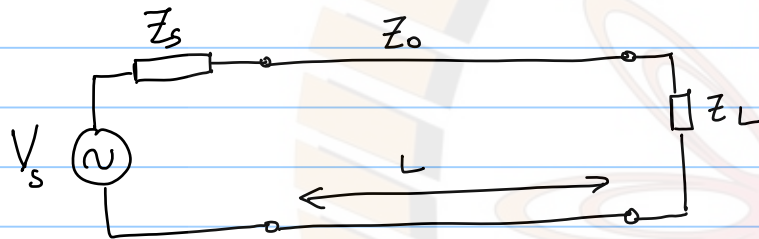
At $z=200\text{m}$, after 2 transit times,
 $V=40\text{V}$

At $z=300\text{m}$, draw evolution of voltage,



AC signal in a lossless transmission line

1)



2)

$$\frac{\partial^2 V(z,t)}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 V(z,t)}{\partial t^2}$$

$$\frac{\partial^2 I(z,t)}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 I(z,t)}{\partial t^2}$$

3)

$$V(z,t) = \text{Re} \left\{ V(z) e^{j\omega t} \right\}$$

$$I(z,t) = \text{Re} \left\{ I(z) e^{j\omega t} \right\}$$

$$4) \quad \frac{\partial^2 v}{\partial z^2} = \frac{1}{u^2} (j\omega)^2 v(z) e^{j\omega t}$$

$$= \left[\frac{1}{u^2} (j\omega)^2 \right] v(z)$$

$$\text{Let } \beta = \omega \sqrt{LC} \Rightarrow \frac{\partial^2 v}{\partial z^2} + \beta^2 v(z) = 0$$

$$\hookrightarrow \text{radians/m (Phase constant)} \quad \beta = \frac{2\pi}{\lambda}$$

$$5) \quad V(z) = \underset{\substack{\uparrow \\ \text{forward}}}{V^+ e^{-j\beta z}} + \underset{\substack{\uparrow \\ \text{backward}}}{V^- e^{+j\beta z}}$$

$$6) \quad I(z) = \frac{1}{Z_0} V^+ e^{-j\beta z} - \frac{1}{Z_0} V^- e^{+j\beta z}$$

7)

$$V(z, t) = \operatorname{Re} \left\{ |V^+| e^{-j\beta z} e^{j\omega t} \right\}$$

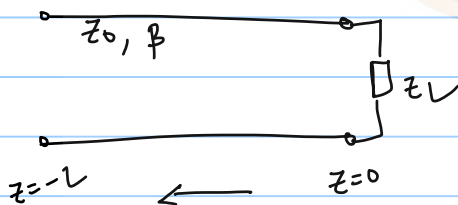
$$= |V^+| \cos(\omega t - \beta z)$$

$$= |V^+| \cos \left(\omega \left(t - \frac{\beta}{\omega} z \right) \right)$$

$$= |V^+| \cos \left(\omega \left(t - \frac{z}{u} \right) \right)$$

$$u = \frac{\omega}{\beta} \rightarrow \text{Phase velocity}$$

8)



$$V(z=0) = V_L = I(z=0) z_L$$

$$V_0^+ + V_0^- = \frac{1}{z_0} [V_0^+ - V_0^-] z_L$$

$$\frac{V_o^-}{V_o^+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \Gamma_L \Big|_{z=0}$$

Let $Z_L = \infty$ (open circuit)

$$V(z) = V_o^+ \left(e^{-j\beta z} + \frac{V_o^-}{V_o^+} e^{+j\beta z} \right)$$

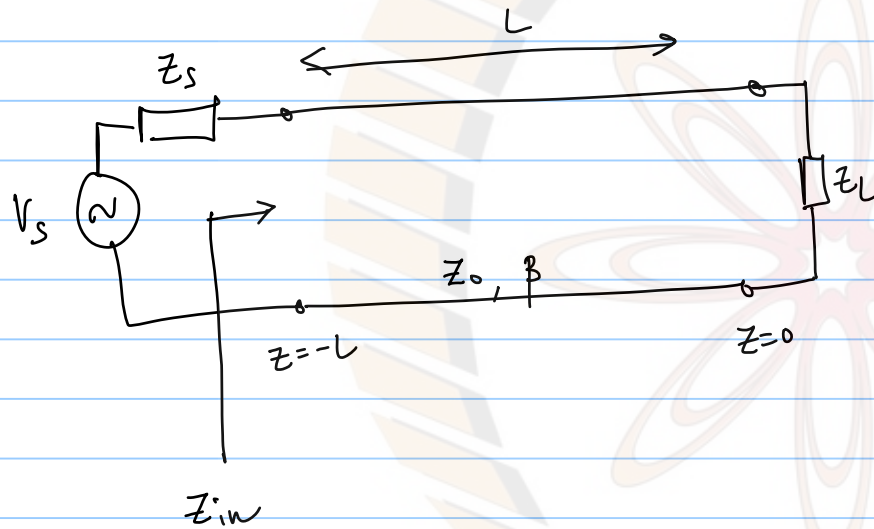
$\uparrow \Gamma_L \Big|_{z=0} = 1$

$$= 2V_o^+ \cos(\beta z)$$

$$I(z) = \frac{V_o^+}{Z_0} \left(e^{-j\beta z} - \frac{V_o^-}{V_o^+} e^{+j\beta z} \right)$$

$\uparrow \Gamma_L \Big|_{z=0} = -1$

$$= -j \frac{2V_0^+}{Z_0} \sin(\beta z)$$



$$V(-L) = V_0^+ \left(e^{+j\beta L} + \frac{V_0^-}{V_0^+} e^{-j\beta L} \right)$$

$$= V_0^+ \left(e^{+j\beta L} + \Gamma_L e^{-j\beta L} \right)$$

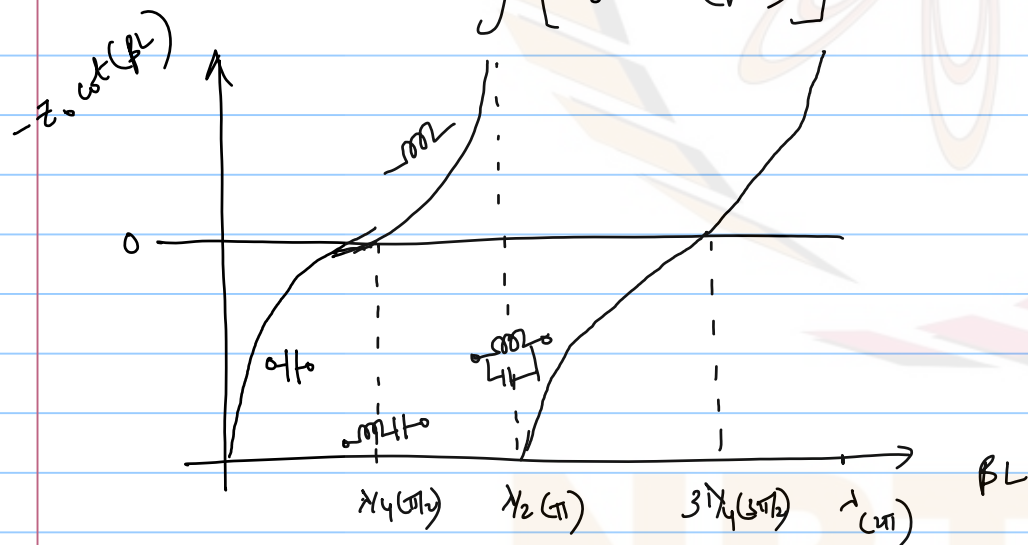
$$I(-L) = \frac{V_0^+}{Z_0} \left(e^{+j\beta L} - \Gamma_L e^{-j\beta L} \right)$$

$$Z_{in} = Z_0 \left[\frac{Z_L + j Z_0 \tan(\beta L)}{Z_0 + j Z_L \tan(\beta L)} \right] \quad \text{electrical length}$$

Open ckt load,
 $Z_L = \infty$,

$$Z_{in} = Z_0 (-j \cot(\beta L)) \Omega$$

$$= -j [Z_0 \cot(\beta L)]$$



(ii) SC, $Z_L = 0$

$$Z_{in} = jZ_0 \tan(\beta L)$$

(iii) $Z_L = Z_0$,

$$Z_{in} = Z_0 //$$

NPTTEL

$$1) \quad \frac{\partial v}{\partial z} = -\ell \frac{\partial i}{\partial t}$$

$$\frac{v(z+1, t) - v(z, t)}{\Delta z} = -\ell \left(\frac{i(z, t+1) - i(z, t)}{\Delta t} \right)$$

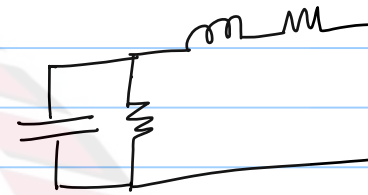
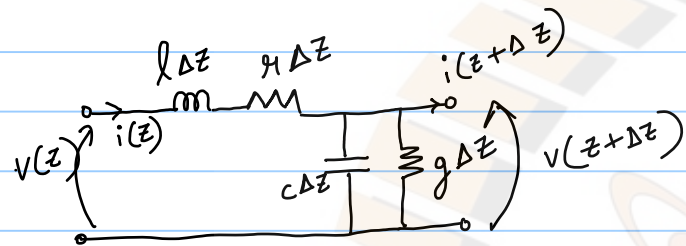
$$\Rightarrow i(z, t+1) = i(z, t) - \frac{\Delta t}{\ell \Delta z} (v(z+1, t) - v(z, t))$$

$$2) \quad \frac{\partial i}{\partial z} = -c \frac{\partial v}{\partial t}$$

$$\frac{i(z, t) - i(z-1, t)}{\Delta z} = -c \frac{v(z, t+1) - v(z, t)}{\Delta t}$$

$$\Rightarrow v(z, t+1) = v(z, t) - \frac{\Delta t}{c \Delta z} \{ i(z, t) - i(z-1, t) \}$$

1)



KVL :-

$$V(z) - (j\omega L \Delta z) i(z) - L \Delta z \frac{\partial i}{\partial t} - V(z + \Delta z) = 0$$

Rearrange,

$$V(z + \Delta z) - V(z) = -j\omega L \Delta z i(z) - L \Delta z \frac{\partial i}{\partial t}$$

$$\Rightarrow \frac{V(z + \Delta z) - V(z)}{\Delta z} = -j\omega i(z) - L \frac{\partial i}{\partial t}$$

As $\Delta z \rightarrow 0$,

$$\Rightarrow \boxed{\frac{\partial V}{\partial z} = -j\omega i(z) - L \frac{\partial i}{\partial t}}$$

KCL :-

$$i(z) - (g\Delta z) - c\Delta z \frac{\partial v}{\partial t} - i(z+\Delta z) = 0$$

Rearrange & apply $\Delta z \rightarrow 0$,

$$\boxed{\frac{\partial i}{\partial z} = -g v - c \frac{\partial v}{\partial t}}$$

$$\frac{\partial v}{\partial z} = -g i - l \frac{\partial i}{\partial t}$$

$$\frac{v(z+\Delta z, t) - v(z, t)}{\Delta z} = \underbrace{-g i(z)}_{\text{circled in orange}} - l \frac{i(z, t+\Delta t) - i(z, t)}{\Delta t}$$

NPTTEL

$$\frac{\partial V}{\partial z} = - (r + j\omega l) I$$

$$\frac{\partial I}{\partial z} = - (g + j\omega c) V$$

Telegrapher's eqns in frequency domain

$$\frac{\partial^2 V}{\partial z^2} = (r + j\omega l)(g + j\omega c) V$$

Wave eqn in frequency domain

(Series Impedance)
Z

(Parallel admittance)
Y

$$\frac{\partial^2 V}{\partial z^2} = \gamma^2 V$$

$$\gamma = \sqrt{(r + j\omega l)(g + j\omega c)}$$

Propagation constant $\rightarrow \alpha + j\beta$

$$\Rightarrow V(z) = V^+ e^{-\gamma z} + V^- e^{+\gamma z}$$

Attenuation Constant

Phase Constant

$$\Rightarrow V^+ e^{-\gamma z} = V^+ e^{-j\beta z} \left(e^{-\alpha z} \right) \quad \begin{matrix} \text{positive} \\ \swarrow \end{matrix}$$

$$V^+ e^{-\gamma z} = |V^+| \underbrace{e^{-\alpha z}}_{\text{attenuation}} \underbrace{e^{-j\beta z}}_{\text{Phase}}$$

Multiplying both sides with $e^{j\omega t}$,
 phase $\rightarrow (\omega t - \beta z)$

$\alpha \rightarrow \text{Nepers/m}$

If $\alpha = 1 \text{ Np/m}$, the amplitude drops to $\frac{1}{e}$ over a distance of 1m.

Propagation length = The distance over which the amplitude drops to $\frac{1}{e}$.
 $"L" = \frac{1}{\alpha}$

$$\begin{array}{lcl} \text{Input power} & = & I_n \\ \text{output " } & = & I_{out} \end{array}$$

$$\text{Relative output power in dB} = 10 \log_{10} \left(\frac{I_{out}}{I_n} \right)$$

$$\begin{array}{lcl} \text{Input voltage} & = & |V^+| \\ \text{Output " } & = & |V^+| e^{-\alpha z} \end{array}$$

$$\begin{aligned} \text{dB} &= 10 \log_{10} \left(\frac{|V^+| e^{-\alpha z}}{|V^+|} \right)^2 \\ &= 20 \log_{10} \frac{|V^+| e^{-\alpha z}}{|V^+|} \end{aligned}$$

$$\text{If } \alpha = 1 \text{ Np/m}, \quad z = 1 \text{ m},$$

$$\text{dB} = -8.68 \text{ dB}$$

$$\frac{V(z+\Delta z) - V(z)}{\Delta z}$$

$$V\left(z + \frac{\Delta z}{2}\right)$$

=

$$I(z)$$

$$\frac{u \Delta t}{\Delta z} \leq 1$$

$$\frac{u \Delta t}{\Delta z} = 1 \quad (\text{Magic time step criterion})$$

$$1) \quad \begin{aligned} V &= V^+ e^{-\gamma z} + V^- e^{\gamma z} \\ I &= I^+ e^{-\gamma z} + I^- e^{\gamma z} \end{aligned}$$

$$2) \quad \frac{d}{dz} (V^+ e^{-\gamma z} + V^- e^{\gamma z}) = -(\gamma + j\omega L) \{ I^+ e^{-\gamma z} + I^- e^{\gamma z} \}$$

3) Separate forward & backward parts on LHS & RHS and equate them

forward:- $-\gamma V^+ e^{-\gamma z} = -(\gamma + j\omega L) I^+ e^{-\gamma z}$

$$\Rightarrow \frac{V^+}{I^+} = \frac{\gamma + j\omega L}{\gamma} = \frac{\gamma + j\omega L}{\sqrt{(\gamma + j\omega L)(g + j\omega C)}}$$

$$Z_0 = \sqrt{\frac{\gamma + j\omega L}{g + j\omega C}} \quad \Omega$$

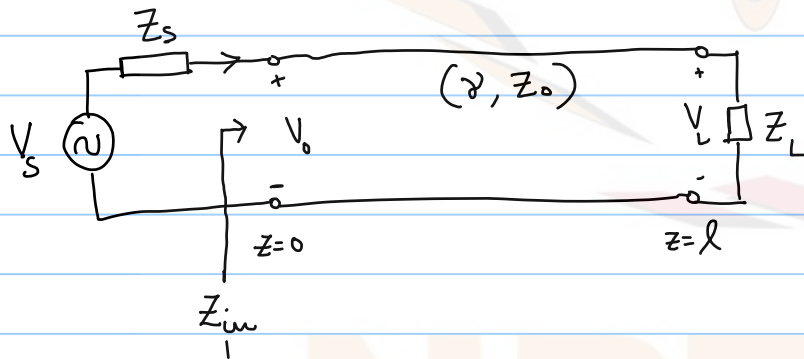
$$= \sqrt{\frac{\text{Series Impedance}}{\text{Parallel Admittance}}}$$

Equate the backward terms,

$$\gamma V^- e^{\gamma z} = -(\kappa + j\omega l) I^- e^{\gamma z}$$

$$\Rightarrow \frac{V^-}{I^-} = \frac{-(\kappa + j\omega l)}{\gamma}$$

$$= -\sqrt{\frac{\kappa + j\omega l}{\gamma + j\omega c}}$$



In the transmission line section,

$$V(z) = V_o^+ e^{-\gamma z} + V_o^- e^{+\gamma z} \quad \text{--- (1)}$$

$$I(z) = \frac{V_o^+}{Z_o} e^{-\gamma z} - \frac{V_o^-}{Z_o} e^{+\gamma z} \quad \text{--- (2)}$$

$$V(z=0) = V_o$$

$$I(z=0) = I_o$$

Add (1) & (2), with $z=0$ (source side)

$$V_o = V_o^+ + V_o^-$$

$$I_o Z_o = V_o^+ - V_o^-$$

$$V_o + I_o Z_o = 2V_o^+$$

$$\Rightarrow V_o^+ = \frac{1}{2} (V_o + I_o Z_o)$$

①-②,

$$V_o^- = \frac{1}{2} (V_o - I_o Z_o)$$

At the load side,

$$V_L = V(z=l)$$

$$I_L = I(z=l)$$

$$V_o^+ = \frac{1}{2} (V_L + Z_o I_L) e^{j\omega l} \quad \text{--- ③}$$

$$V_o^- = \frac{1}{2} (V_L - Z_o I_L) e^{-j\omega l} \quad \text{--- ④}$$

$$Z_{in} = \frac{V(z)}{I(z)} \text{ at input side}$$

$$= \frac{Z_o (V_o^+ + V_o^-)}{V_o^+ - V_o^-}$$

$$Z_{in} = Z_0 \left[\frac{Z_L + Z_0 \tanh(\gamma l)}{Z_0 + Z_L \tanh(\gamma l)} \right]$$

Voltage Reflection Coefficient :-

$$\Gamma_L = \frac{V_0^- e^{\gamma l}}{V_0^+ e^{-\gamma l}}$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\Gamma(z) = \frac{V_0^- e^{\gamma z}}{V_0^+ e^{-\gamma z}} = \frac{V_0^-}{V_0^+} e^{2\gamma z}$$

$$\frac{V_{\max}}{V_{\min}} = \text{Voltage Standing Wave Ratio (VSWR)}$$

$$\frac{1 + |\Gamma_L|}{1 - |\Gamma_L|}$$

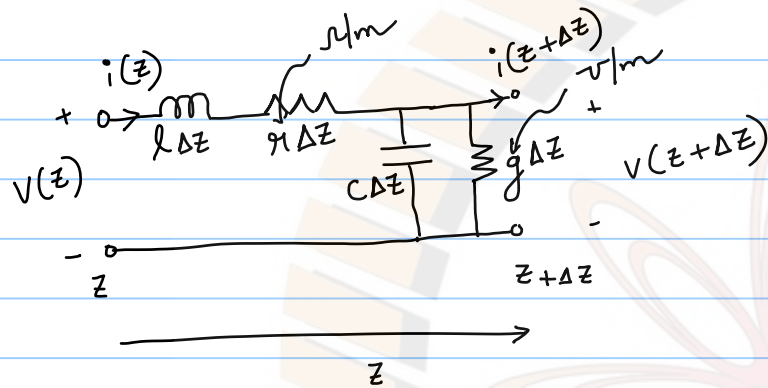
$$\text{If } \Gamma_L = 1,$$

$$\text{VSWR} = \frac{1+1}{1-1} = \infty$$

$$\Gamma_L = 0,$$

$$\text{VSWR} = \frac{1+0}{1-0} = 1$$

NPTTEL



KVL :-

$$V(z, t) - L \Delta z \left. \frac{\partial i}{\partial t} \right|_z - R \Delta z i(z, t) - V(z + \Delta z, t) = 0$$

$$\Rightarrow V(z + \Delta z, t) - V(z, t) = -R \Delta z i(z, t) - L \Delta z \left. \frac{\partial i}{\partial t} \right|_z$$

$$\Rightarrow \frac{V(z + \Delta z, t) - V(z, t)}{\Delta z} = -R i(z, t) - L \left. \frac{\partial i}{\partial t} \right|_z$$

Apply $\Delta z \rightarrow 0$

$$\Rightarrow \boxed{\frac{\partial V}{\partial z} = -R i - L \frac{\partial i}{\partial t}} \quad \text{--- (1)}$$

KCL :-

$$i(z,t) - c \Delta z \left. \frac{\partial v}{\partial t} \right|_{z+\Delta z} - g \Delta z v(z+\Delta z,t) - i(z+\Delta z,t) = 0$$

$$\Rightarrow \frac{i(z+\Delta z,t) - i(z,t)}{\Delta z} = -g v(z+\Delta z,t) - c \left. \frac{\partial v}{\partial t} \right|_{z+\Delta z}$$

Apply $\Delta z \rightarrow 0$,

$$\Rightarrow \boxed{\frac{\partial i}{\partial z} = -g v - c \frac{\partial v}{\partial t}} \quad \text{--- (2)}$$

For periodic sinusoidal excitation,

$$\frac{\partial v}{\partial z} = -(r + j\omega l) I$$

$$\frac{\partial I}{\partial z} = -(g + j\omega c) v$$

$$\frac{\partial^2 V}{\partial z^2} = (r + j\omega l)(g + j\omega c)V$$

If $\gamma = \sqrt{(r + j\omega l)(g + j\omega c)}$, then,

$$\frac{\partial^2 V}{\partial z^2} = \gamma^2 V$$

↑
complex

$\gamma \rightarrow$ Propagation constant (complex) /m

\swarrow
 $\alpha + j\beta$
 $\swarrow \quad \nwarrow$
 Attenuation constant Phase constant
 (Np/m)

$$V = V^+ e^{-\gamma z} + V^- e^{+\gamma z}$$

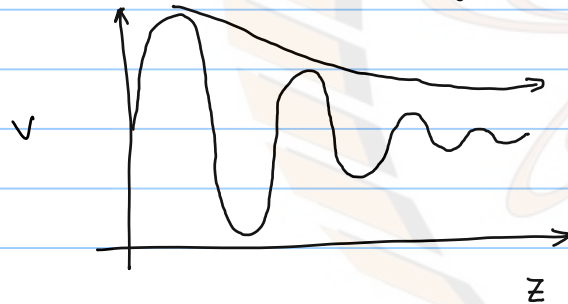
Forward wave, $V^+ e^{-\gamma z}$

$$\Rightarrow V^+ e^{-(\alpha + j\beta)z}$$

$$\Rightarrow \left[V^+ e^{-j\beta z} \right] e^{-\alpha z}$$

If $\alpha = 0$, \rightarrow Lossless transmission line

If $\alpha > 0$, \rightarrow Lossy transmission line



$$V^+ e^{-\gamma z} = |V^+| \underbrace{e^{-\alpha z}}_{\text{Amplitude}} \underbrace{e^{-j\beta z}}_{\text{Phase}}$$

If $\alpha = 1 \text{ Neper/m (Np/m)}$, the amplitude of the wave drops to $\frac{1}{e}$ over a distance of 1m.

Propagation Length :-

The distance over which the amplitude drops to $\frac{1}{e}$ its original value

$$\text{Propagation Length } L = \frac{1}{\alpha} \quad (\text{m})$$

$$\begin{aligned} \text{If input power} &= P_{in} \quad (\text{W}) \\ \text{output power} &= P_{out} \quad (\text{W}) \end{aligned}$$

$$10 \log_{10} \left[\frac{P_{out}}{P_{in}} \right] \quad \text{dB}$$

$$\Rightarrow 10 \log_{10} \left[\frac{|V^+| e^{-\alpha z}}{|V^+|} \right]^2$$

$$\Rightarrow 20 \log_{10} \left[e^{-\alpha z} \right]$$

$$\text{If } \alpha = 1 \text{ Np/m}, \quad \text{If } z = 1 \text{ m},$$
$$\Rightarrow -8.68 \text{ dB/m}$$

NPTTEL

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$= \frac{\frac{Z_L}{Z_0} - 1}{\frac{Z_L}{Z_0} + 1}$$

Say, $Z_L = 50 \Omega$ $\Gamma = \frac{2-1}{2+1} = \frac{1}{3}$
 $Z_0 = 25 \Omega$

or
 $Z_L = 100 \Omega$ $\Gamma = \frac{2-1}{2+1} = \frac{1}{3}$
 $Z_0 = 50 \Omega$

$\frac{Z_L}{Z_0} \rightarrow$ Normalized Impedance

Lossless Transmission Line $\Rightarrow Z_0$ is Real Ω

Let $Z_L = R + jX$
 \uparrow \uparrow \uparrow
 (passive) \uparrow \uparrow \uparrow
 +ve or -ve

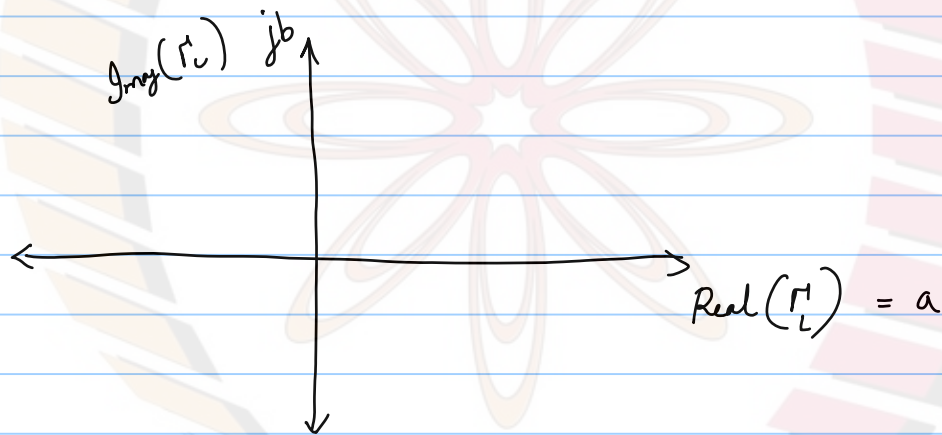
$$\frac{Z_L}{Z_0} = \frac{R}{Z_0} + j \frac{X}{Z_0}$$

$$\bar{Z}_L = r + jx$$

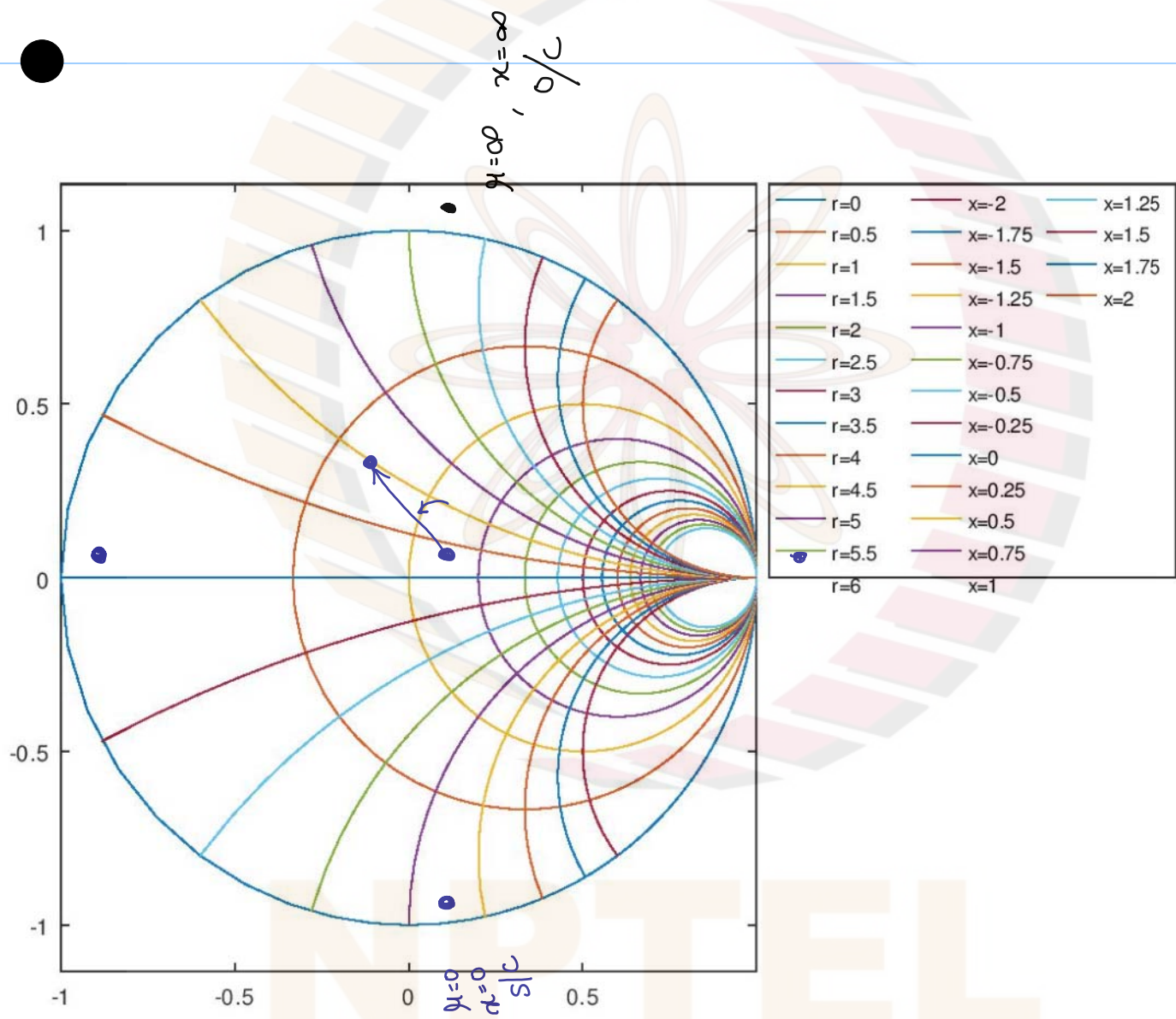
$$\Gamma_L = \frac{\bar{Z}_L - 1}{\bar{Z}_L + 1} = \frac{y + jx - 1}{y + jx + 1} = \frac{y - 1 + jx}{y + 1 + jx}$$

\downarrow
 $a + jb$

$$\bar{Z}_L = y + jx$$



NPTTEL



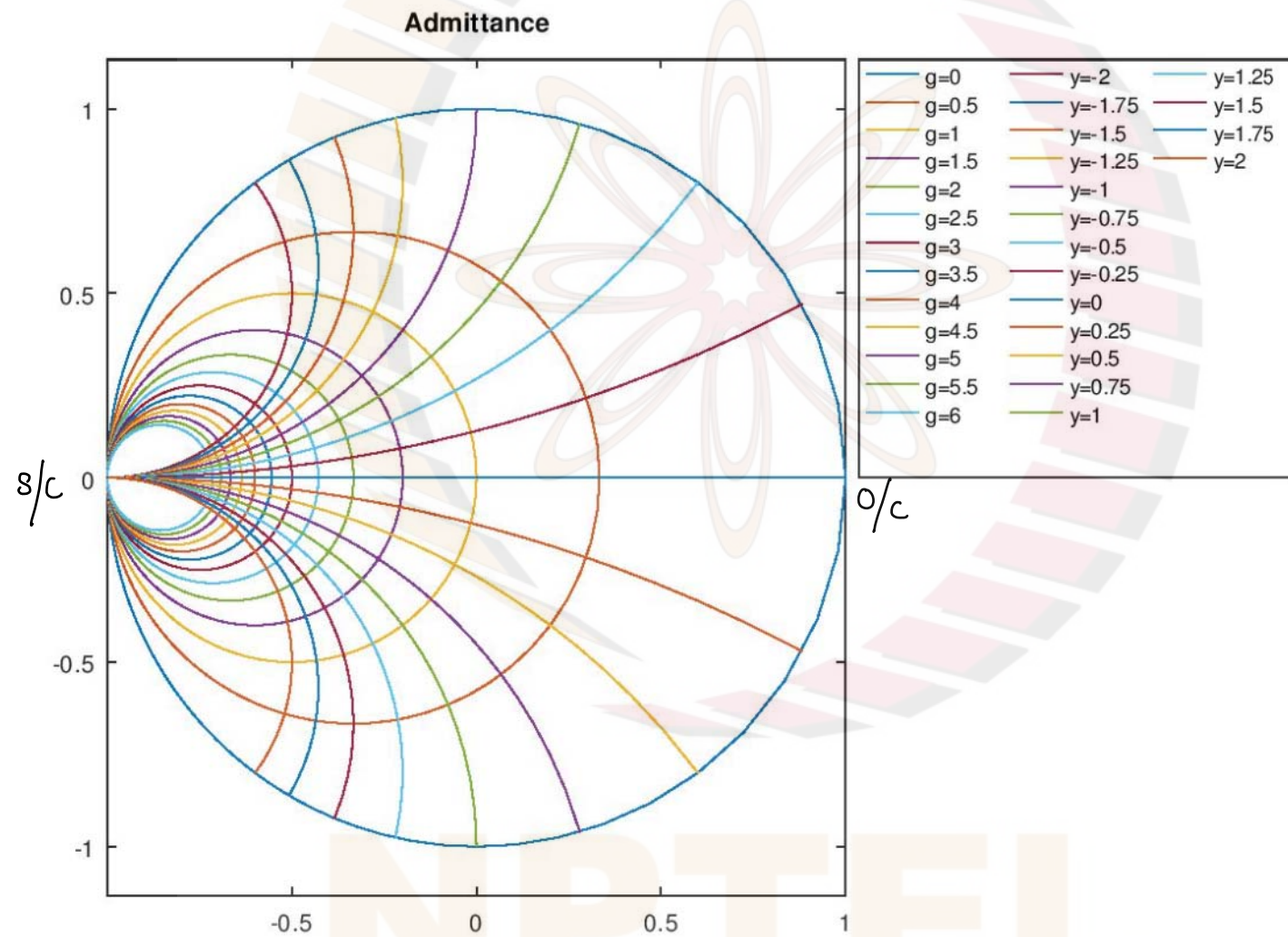
$\gamma_0 \rightarrow$ Characteristic Admittance

$\gamma_L \rightarrow$ Load admittance

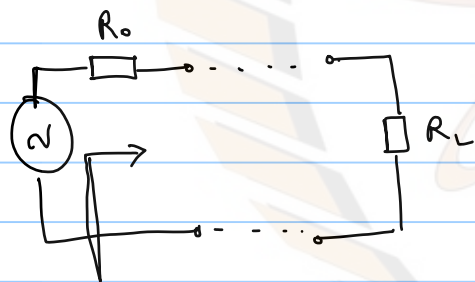
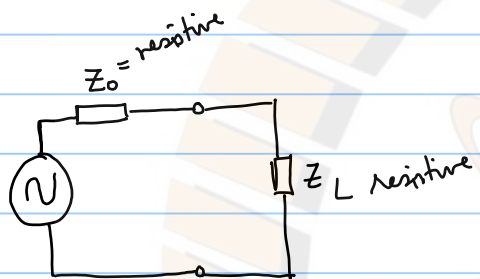
$g + jy$

$$\begin{aligned} \Gamma_L &= \frac{\frac{Z_L}{Z_0} - 1}{\frac{Z_L}{Z_0} + 1} = \frac{\frac{\gamma_0}{\gamma_L} - 1}{\frac{\gamma_0}{\gamma_L} + 1} = \frac{\gamma_0 - \gamma_L}{\gamma_0 + \gamma_L} \\ &= \frac{1 - \frac{\gamma_L}{\gamma_0}}{1 + \frac{\gamma_L}{\gamma_0}} \\ &= \frac{1 - \bar{\gamma}_L}{1 + \bar{\gamma}_L} \\ &= \frac{-(\bar{\gamma}_L - 1)}{(\bar{\gamma}_L + 1)} = \frac{-(g + jy - 1)}{(g + jy + 1)} \end{aligned}$$

NPTTEL



SimSmith



NPTTEL

$$I_{\max} = \frac{V_{\max}}{Z_0}, \quad I_{\min} = \frac{V_{\min}}{Z_0}$$

$$\left| Z_{in} \right|_{\min} = \frac{V_{\min}}{I_{\max}} = \frac{Z_0}{VSWR}$$

$$\left| Z_{in} \right|_{\max} = \frac{V_{\max}}{I_{\min}} = (VSWR) Z_0$$

NPTTEL

1) For a transmission line,

$$r = 0.1 \, \Omega/m$$

$$l = 0.2 \, \mu H/m$$

$$c = 10 \, pF/m$$

$$g = 0.02 \, S/m$$

Solu:- Complex propagation constant γ :-

$$\gamma = \sqrt{(r + j\omega l)(g + j\omega c)}$$

$$\left\{ \sqrt{Z_{\text{series}} Y_{\text{parallel}}} \right\}$$

(i) At 1 MHz frequency,

$$= \sqrt{(0.1 + j(2\pi \times 1 \times 10^6) \times (0.2 \times 10^{-6})) (0.02 + j(2\pi \times 1 \times 10^6) \times (10 \times 10^{-12}))}$$

$$= \frac{0.117}{\alpha} + j \frac{0.108}{\beta} \text{ /m}$$

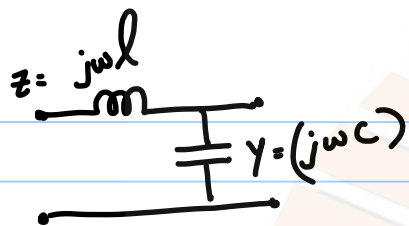
(ii) γ at 1 GHz

$$\begin{aligned} \gamma &= \sqrt{(R + j\omega L)(G + j\omega C)} \\ &= \frac{1.4}{\alpha} + j \frac{9}{\beta} \text{ /m} \end{aligned}$$

(iii) The ratio of propagation lengths

$$\begin{aligned} \frac{L_{1\text{MHz}}}{L_{1\text{GHz}}} &= \frac{\left(\frac{1}{0.117} \right)}{\left(\frac{1}{1.4} \right)} \\ &\cong 11 \text{ or } 12 \end{aligned}$$

1)

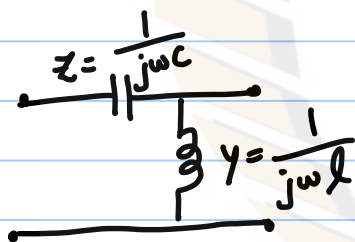


$$\gamma = \sqrt{zy} = j\omega\sqrt{lc}$$

$$\Rightarrow \beta = \omega\sqrt{lc}$$

$$V_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{lc}}$$

Say:-



$$\gamma = \sqrt{zy} = \frac{1}{j\omega\sqrt{lc}} = \frac{-j}{\omega\sqrt{lc}}$$

$$\Rightarrow \beta = \frac{-1}{\omega\sqrt{lc}}$$

$$V_p = \frac{\omega}{\beta} = -\omega^2\sqrt{lc}$$

(Metamaterials)

NPTTEL

Maxwell's equations, plane waves, interfaces

i)

$$\underline{\nabla} \cdot \underline{D}(t) = \rho(t)$$

$$\underline{\nabla} \cdot \underline{B}(t) = 0$$

$$\underline{\nabla} \times \underline{E}(t) = -\frac{\partial \underline{B}(t)}{\partial t}$$

$$\underline{\nabla} \times \underline{H}(t) = \underline{J}(t) + \frac{\partial \underline{D}(t)}{\partial t}$$

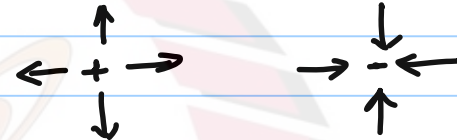
↳ Conduction current density

$$\underline{B}(t) = \mu(t) * \underline{H}(t)$$

↳ (H/m) ↳ A/m

$$\underline{D}(t) = \epsilon(t) * \underline{E}(t)$$

↳ (F/m) ↳ V/m



- | | | | |
|----|-----------------|---|-----------------------|
| a) | Isotropic Media | - | Vacuum |
| b) | Anisotropic " | - | Crystalline materials |

- c) Frequency Independent - Vacuum
 d) Frequency dependent - Any material other than vacuum

Let $\rho = 0$, $J = 0$

$$\begin{aligned}\nabla \times (\nabla \times \underline{E}) &= -\mu \left[\nabla \times \frac{\partial \underline{H}}{\partial t} \right] \\ &= -\mu \left[\frac{\partial}{\partial t} (\nabla \times \underline{H}) \right]\end{aligned}$$

↳ $\frac{\text{LHS}}{\epsilon_0} \nabla (\nabla \cdot \underline{E}) - \nabla^2 \underline{E} = -\nabla^2 \underline{E}$

$$\begin{aligned}\underline{\text{RHS}} &= -\mu \frac{\partial}{\partial t} \left[\frac{\partial \underline{D}}{\partial t} \right] = -\mu \frac{\partial^2 \underline{D}}{\partial t^2} \\ &= -\mu \epsilon \frac{\partial^2 \underline{E}}{\partial t^2}\end{aligned}$$

$$\underline{LHS = RHS} \Rightarrow$$

$$\boxed{\nabla^2 \underline{E} = \mu \epsilon \frac{\partial^2 \underline{E}}{\partial t^2}}$$

$$\begin{array}{c} \text{V/m} \\ \text{1/m}^2 \end{array} \quad \begin{array}{c} \text{V/m} \\ \text{1/s}^2 \end{array}$$

$$\Rightarrow \frac{1}{\sqrt{\epsilon \mu}} \text{ - units of m/s}$$

$$\begin{array}{lcl} \Rightarrow \epsilon & \rightarrow & \text{Vacuum } \epsilon_0 \quad 8.854 \times 10^{-12} \\ \mu & \rightarrow & \text{Vacuum } \mu_0 \quad 4\pi \times 10^{-7} \\ & & \text{Velocity in vacuum } \approx 3 \times 10^8 \text{ m/s} \end{array}$$

NPTTEL

$$\underline{\nabla} \times \underline{E}(t) = - \frac{\partial \underline{B}(t)}{\partial t}$$

$$\underline{E} = E_x \hat{x} + E_y \hat{y} + E_z \hat{z}$$

Direction of propagation $+z$

$$\begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \cancel{\frac{\partial}{\partial x}} & \cancel{\frac{\partial}{\partial y}} & \cancel{\frac{\partial}{\partial z}} \\ E_x & \cancel{E_y} & \cancel{E_z} \end{vmatrix} = \hat{i} (0 - 0) - \hat{j} \left(0 - \frac{\partial E_x}{\partial z} \right) + \hat{k} (0 - 0)$$

$$= \hat{j} \frac{\partial E_x}{\partial z}$$

$$-\mu \frac{\partial H_y}{\partial t}$$

E_x H_y z direction propagation

$$\frac{\partial E_x}{\partial z} = -\mu \frac{\partial H_y}{\partial t}$$

$$\frac{\partial H_y}{\partial z} = -\epsilon \frac{\partial E_x}{\partial t}$$

$$\frac{\partial^2 E_x}{\partial z^2} = \frac{1}{c^2} \frac{\partial^2 E_x}{\partial t^2}$$

$$c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

$$E_x(z, t) = f^+(t - \frac{z}{u}) + f^-(t + \frac{z}{u})$$

$$H_y(z, t) = \frac{1}{\mu_0 c} f^+(t - \frac{z}{u})$$

↳ "Ω"

$$\mu_0 c = \mu_0 \frac{1}{\sqrt{\epsilon_0 \mu_0}} = \sqrt{\frac{\mu_0}{\epsilon_0}} \quad \Omega$$

$$\frac{\partial v}{\partial z} = -l \frac{\partial i}{\partial t}$$

$$\frac{\partial i}{\partial z} = -c \frac{\partial v}{\partial t}$$

$$\frac{\partial^2 v}{\partial z^2} = \frac{1}{u^2} \frac{\partial^2 v}{\partial t^2}$$

$$u = \frac{1}{\sqrt{lc}}$$

$$v(z, t) = f^+(t - \frac{z}{u}) + f^-(t + \frac{z}{u})$$

$$\text{Forward } i(z, t) = \frac{1}{lu} f^+(t - \frac{z}{u})$$

↳ "Ω"

$$lu = l \frac{1}{\sqrt{lc}} = \sqrt{\frac{l}{c}} \quad \Omega \quad \text{"R}_c \text{" or "Z}_0 \text{"}$$

In the case of vacuum,

$$\eta_0 \cong 377 \Omega$$

$$\eta_0 = \frac{E_x^+}{H_y^+}$$

$$v(z,t) = v^+(z,t) + v^-(z,t)$$
$$i(z,t) = \frac{1}{Z_0} v^+(z,t) - \frac{1}{Z_0} v^-(z,t)$$

In the simulation, on the right edge, $E_n = 0$ (Perfect Electric Conductor)

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}}$$

$$Z_n = \sqrt{\frac{\mu_0 \mu_n}{\epsilon_0 \epsilon_n}}$$

$$\mu = \mu_0 \mu_n$$

$$\epsilon = \epsilon_0 \epsilon_n$$

(for vacuum $\mu_n = 1$)
for other media, $\mu_n \geq 1$

$$Z_m = \sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_m}}$$

$$\epsilon_m > 1$$

$$= \frac{Z_0}{\sqrt{\epsilon_m}}$$

$$C = \frac{1}{\sqrt{\epsilon_0 \mu_0}}$$

$$C_m = \frac{1}{\sqrt{\epsilon_0 \epsilon_m \mu_0 \mu_m}}$$

$\uparrow \qquad \qquad \uparrow$

NPTTEL

1) Velocity of the electromagnetic wave $c = \frac{1}{\sqrt{\mu\epsilon}} = \frac{1}{\sqrt{\mu_r \mu_0 \epsilon_r \epsilon_0}}$

For vacuum, $\epsilon_0 = 8.854 \times 10^{-12} \text{ F/m}$
 $\mu_0 = 4\pi \times 10^{-7} \text{ H/m}$

Velocity $c_0 \cong 3 \times 10^8 \text{ m/s}$
 (vacuum)

2) Characteristic impedance $\eta = \sqrt{\frac{\mu}{\epsilon}}$, for vacuum, $\eta_0 \cong 377 \Omega$ or $120 \pi \Omega$

3) Travel direction or propagation direction $\rightarrow z$
 E-field $\rightarrow E_x \hat{x}$

$$E(x, y, z, t) = E_x(z) \hat{x} e^{j\omega t}$$

$$\Rightarrow \frac{\partial}{\partial x} = 0, \quad \frac{\partial}{\partial y} = 0$$

$$\Rightarrow \frac{d^2 E_x(z)}{dz^2} = \underbrace{-\omega^2 \mu \epsilon}_{\gamma^2} E_x(z)$$

$\gamma \rightarrow$ Propagation constant

$$\gamma = j\omega \sqrt{\mu \epsilon} = j\beta \quad \uparrow \text{phase constant}$$

$$E_x = E_x^+ e^{-j\beta z} + E_x^- e^{+j\beta z}$$

$$E_x(t) = \left[E_x^+ e^{-j\beta z} + E_x^- e^{+j\beta z} \right] e^{j\omega t}$$

$$\nabla \times \underline{E} = -j\omega\mu \underline{H}$$

$$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \cancel{\frac{\partial}{\partial x}} & \cancel{\frac{\partial}{\partial y}} & \frac{\partial}{\partial z} \\ E_x & \cancel{E_y} & \cancel{E_z} \end{vmatrix} = -j\omega\mu \underline{H}$$

$$-\hat{y} \left(-\frac{\partial}{\partial z} E_x \right) = -j\omega\mu H_y$$

$$-j\beta E_x^+ e^{-j\beta z} + j\beta E_x^- e^{+j\beta z} = -j\omega\mu H_y$$

$$\Rightarrow H_y = \frac{\beta}{\omega\mu} E_x^+ e^{-j\beta z} - \frac{\beta}{\omega\mu} E_x^- e^{+j\beta z}$$

$$\eta = \frac{E_x^+}{H_y^+}$$

E-field can be decomposed to E_x, E_y

H-field " " " " H_x, H_y

TEM waves

$$|\underline{H}| = \sqrt{H_x^2 + H_y^2}$$

$$= \sqrt{\left(\frac{E_y}{\eta}\right)^2 + \left(\frac{E_x}{\eta}\right)^2}$$

$$= \frac{|\underline{E}|}{\eta}$$

NPTTEL

Polarization \rightarrow The temporal evolution of E-field at a given location in space.

$+z \rightarrow$ Direction of travel

$$E_x = \operatorname{Re} \left\{ E_{x0} e^{j\omega t - j\beta z} \right\}$$
$$E_y = \operatorname{Re} \left\{ E_{y0} e^{j\omega t - j\beta z + j\phi} \right\}$$

$\phi \rightarrow +ve \rightarrow E_y$ lead E_x by ϕ

$\phi \rightarrow -ve \rightarrow E_y$ lags E_x by ϕ

$$\underline{E} = E_{x0} \cos(\omega t) \hat{x} + E_{y0} \cos(\omega t + \phi) \hat{y}$$

$$\Rightarrow \cos(\omega t) = \frac{E_x}{E_{x0}}$$

$$\sin(\omega t) = \sqrt{1 - \left(\frac{E_x}{E_{x0}} \right)^2}$$

$$\frac{E_y}{E_{y0}} = \cos(\omega t + \phi)$$

$$\frac{E_x}{E_{x0}} = \cos(\omega t) \cos(\phi) - \sin(\omega t) \sin(\phi)$$

$$\frac{E_x}{E_{x0}} \cos \phi - \sqrt{1 - \frac{E_x^2}{E_{x0}^2}} \sin \phi$$

$$\cos^2 \phi + \sin^2 \phi = 1$$

$$\left(\frac{E_x}{E_{x0}} \right)^2 - \frac{2E_x E_y \cos \phi}{E_{x0} E_{y0}} + \left(\frac{E_y}{E_{y0}} \right)^2 = \sin^2 \phi$$

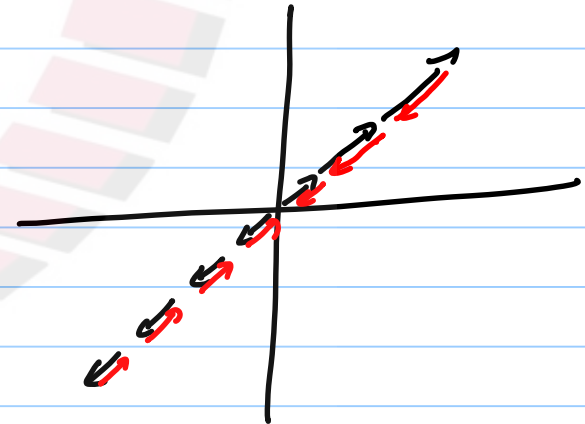
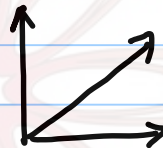
1)

$$E_x \neq E_y, \quad \phi = 0$$

$$\frac{E_x}{E_{x0}} = \frac{E_y}{E_{y0}}$$

$$\Rightarrow E_y = \left(\frac{E_{y0}}{E_{x0}} \right) E_x \quad (\text{Resembles } y = mx)$$

Linear polarization



Linear polarization

$$\phi = 0 \text{ or } \pi \text{ or } 2\pi \text{ or } 3\pi \dots \dots$$
$$\pm m\pi$$

Elliptical Polarization

$$\phi \neq 0, \quad E_{x0} = E_{y0} \text{ or } E_{x0} \neq E_{y0}$$

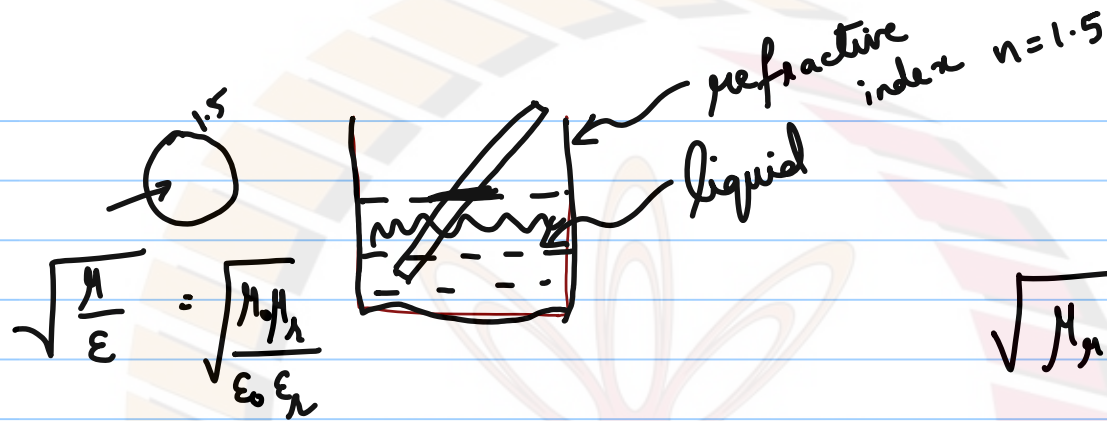
$$\phi = \pi/2, \quad E_{x0} \neq E_{y0}$$

Circular Polarization

$$\phi = \pm \text{odd multiple of } \pi/2$$
$$E_{x0} = E_{y0}$$

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$$1) \quad \nabla \times \underline{E} = -j\omega\mu_0\mu_r \underline{H}$$

$$\nabla \times \underline{H} = \underline{J} + j\omega\epsilon_0\epsilon_r \underline{E}$$

2) If the medium has a conductivity σ ,

$$\underline{J} = \sigma \underline{E}$$

$$\nabla \times \underline{H} = \sigma \underline{E} + j\omega\epsilon_0\epsilon_r \underline{E}$$

$$= (\sigma + j\omega\epsilon_0\epsilon_r) \underline{E}$$

$$= j\omega\epsilon_0 \underbrace{\left(\epsilon_r - j \frac{\sigma}{\omega\epsilon_0} \right)}_{\epsilon_{rc}} \underline{E}$$

$$= j\omega\epsilon_0 \epsilon_{rc} \underline{E}$$

ϵ_{rc} Relative permittivity of
 conductive medium
 { Complex Permittivity }

$$3) \quad \epsilon_{nc} \longrightarrow \left(\epsilon_r - \frac{j\sigma}{\omega \epsilon_0} \right)$$

$\epsilon_{nc} \rightarrow$ Complex / Frequency Dependent

$\underline{J} = \sigma \underline{E}$ is a characteristic of a conductor

$\epsilon_0 \epsilon_r \underline{E}$ is a characteristic of a dielectric

$$4) \quad \frac{\text{Conduction current density}}{\text{Displacement current density}} \gg 1$$

$$\text{or} \quad \frac{\sigma}{\omega \epsilon_0 \epsilon_r} \gg 1 \quad \longrightarrow \text{Good conductors}$$

$$\text{If} \quad \frac{\sigma}{\omega \epsilon_0 \epsilon_r} \ll 1 \quad \longrightarrow \text{Good dielectric}$$

If $\frac{\sigma}{\omega \epsilon_0 \epsilon_r} \approx 1 \rightarrow$ Neither good dielectric nor good conductor

5)

Copper,

$$\epsilon_r \approx 1$$

$$\sigma = 5.6 \times 10^7 \text{ } \Omega/\text{m}$$

$$f_T \text{ (Transition frequency)} \approx 10^{18} \text{ Hz}$$

Sea water, $\epsilon_r \approx 80$

$$\sigma = 10^{-3} \text{ } \Omega/\text{m}$$

$$f_T \approx 225 \text{ kHz}$$

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$$6) \quad \begin{aligned} \nabla^2 \underline{E} &= -\omega^2 \mu_0 \mu_r \epsilon_0 \epsilon_{rc} \underline{E} \\ \nabla^2 \underline{H} &= -\omega^2 \mu_0 \mu_r \epsilon_0 \epsilon_{rc} \underline{H} \end{aligned}$$

→ RHS → $j\omega \mu_0 \mu_r (\sigma + j\omega \epsilon_0 \epsilon_r) \underline{E}$

For majority of materials,

$$\mu_r = 1$$

7) For a plane wave, traveling in z -direction, x -polarized

$$\begin{aligned} \frac{\partial^2 E_x}{\partial z^2} &= -\omega^2 \mu_0 \epsilon_0 \epsilon_{rc} E_x \\ &= \gamma^2 E_x \end{aligned}$$

$$\begin{aligned}
 \Rightarrow \gamma &= \sqrt{-\omega^2 \mu_0 \epsilon_0 \epsilon_r} \\
 &= j\omega \sqrt{\mu_0 \epsilon_0} \sqrt{\epsilon_r} \\
 &= j\omega \sqrt{\mu_0 \epsilon_0} \left\{ \epsilon_r - j \frac{\sigma}{\omega \epsilon_0} \right\}^{1/2}
 \end{aligned}$$

$$\alpha = \operatorname{Re}\{\gamma\} = \omega \sqrt{\frac{\mu_0 \epsilon_0 \epsilon_r}{2}} \left[\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon_0^2 \epsilon_r^2}} - 1 \right]^{1/2}$$

$$\beta = \operatorname{Im}\{\gamma\} = \omega \sqrt{\frac{\mu_0 \epsilon_0 \epsilon_r}{2}} \left[\sqrt{1 + \frac{\sigma^2}{\omega^2 \epsilon_0^2 \epsilon_r^2}} + 1 \right]^{1/2}$$

Loss tangent

$$\tan \delta = \frac{\sigma}{\omega \epsilon_0 \epsilon_r}$$

$$\sigma \gg \omega \epsilon_0 \epsilon_r$$

$$\gamma \approx \sqrt{j\omega\mu_0\sigma}$$

$$\sqrt{j} = \sqrt{e^{j\pi/2}} = e^{j\pi/4} = \cos\pi/4 + j\sin\pi/4 = \frac{1}{\sqrt{2}} + j\frac{1}{\sqrt{2}}$$

$$\gamma = \sqrt{\omega\mu_0\sigma} \left\{ \frac{1+j}{\sqrt{2}} \right\}$$

$$\alpha = \beta = \sqrt{\frac{\omega\mu_0\sigma}{2}}$$

$$, \quad \omega \uparrow, \alpha \uparrow, \beta \uparrow$$

$$\sigma \uparrow, \alpha \uparrow, \beta \uparrow$$

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Power
density

$$\underline{P} = \underline{E} \times \underline{H}$$

Net power

$$W = \oint_S (\underline{E} \times \underline{H}) \cdot d\hat{a}$$

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1) $\underbrace{\underline{E}}_{V/m} \times \underbrace{\underline{H}}_{A/m} = \underbrace{\underline{P}}_{W/m^2}$ (Power density)

(VA/m^2 if there is a phase difference between \underline{E} & \underline{H})

2) Net outward power = $W = \oint_S (\underline{E} \times \underline{H}) \cdot d\hat{a}$

3) Instantaneous fields :-

$$\underline{E}(x, y, z, t) = \text{Re} \left\{ E_0(x, y, z) e^{j\omega t} e^{j\phi_e} \right\} \hat{e}$$

$$\underline{H}(x, y, z, t) = \text{Re} \left\{ H_0(x, y, z) e^{j\omega t} e^{j\phi_h} \right\} \hat{h}$$

E-field $\rightarrow E_0(x, y, z) \cos(\phi_e + \omega t) \hat{e}$

H-field $\rightarrow H_0(x, y, z) \cos(\phi_h + \omega t) \hat{h}$

Instantaneous power,

$$\begin{aligned}\underline{P} &= \underline{E} \times \underline{H} \\ &= E_0 H_0 \cos(\omega t + \phi_e) \cos(\omega t + \phi_h) (\hat{e} \times \hat{h}) \\ &= \frac{E_0 H_0}{2} \left\{ \cos(\phi_e - \phi_h) + \cos(2\omega t + \phi_e + \phi_h) \right\} (\hat{e} \times \hat{h})\end{aligned}$$

Instantaneous power could be positive, negative or zero.
Drawing conclusions is not easy.

Average power density:

$$\begin{aligned}\underline{P}_{av} &= \frac{1}{T} \int \underline{P} dt \\ &= \frac{1}{2} \operatorname{Re} \left\{ \left[E_0 e^{j\phi_e} e^{j\omega t} \hat{e} \right] \times \left[H_0 e^{-j\phi_h} e^{-j\omega t} \hat{h} \right] \right\}\end{aligned}$$

$$\sim \left\{ \left(\frac{1}{2} \epsilon_0 H_0 \omega (\phi_e - \phi_h) \hat{e} \times \hat{h} \right) \right\}$$

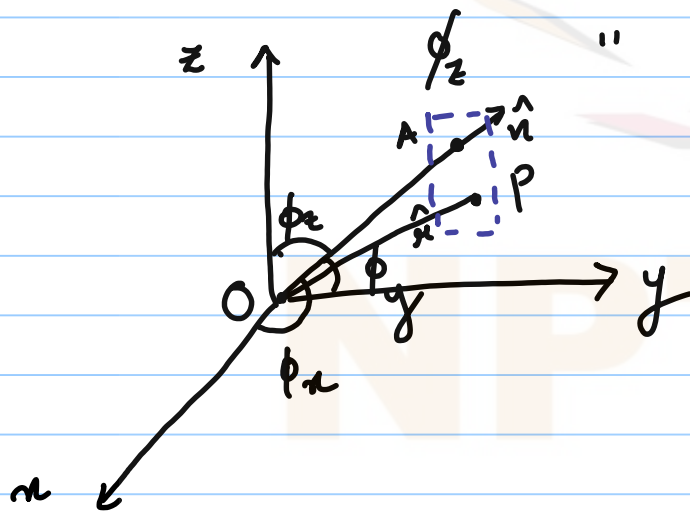
$$= \frac{1}{2} \operatorname{Re} \left\{ \underline{E} \times \underline{H}^* \right\}$$

A plane wave travels in an arbitrary direction

$\hat{n} \rightarrow$ angles ϕ_x w.r.t x axis

ϕ_y " y axis

ϕ_z " z axis



$$\hat{n} = \cos\phi_x \hat{x} + \cos\phi_y \hat{y} + \cos\phi_z \hat{z}$$

$$\vec{r} = x \hat{x} + y \hat{y} + z \hat{z}$$

$$\underline{k} = \beta \hat{n} = \beta \cos\phi_x \hat{x} + \beta \cos\phi_y \hat{y} + \beta \cos\phi_z \hat{z}$$

\downarrow
 $\frac{2\pi}{\lambda}$

$$\underline{E} \cdot \underline{k} = 0 \quad \text{or} \quad \underline{E} \cdot \hat{n} = 0.$$

for a z-directed plane EM wave,

$$\underline{k} = \beta \left(\cos\phi_x \hat{x} + \cos\phi_y \hat{y} + \cos\phi_z \hat{z} \right)$$

$$= \beta \left(\cos\frac{\pi}{2} \hat{x} + \cos\frac{\pi}{2} \hat{y} + \cos(0) \hat{z} \right)$$

$$= \beta \hat{z}$$

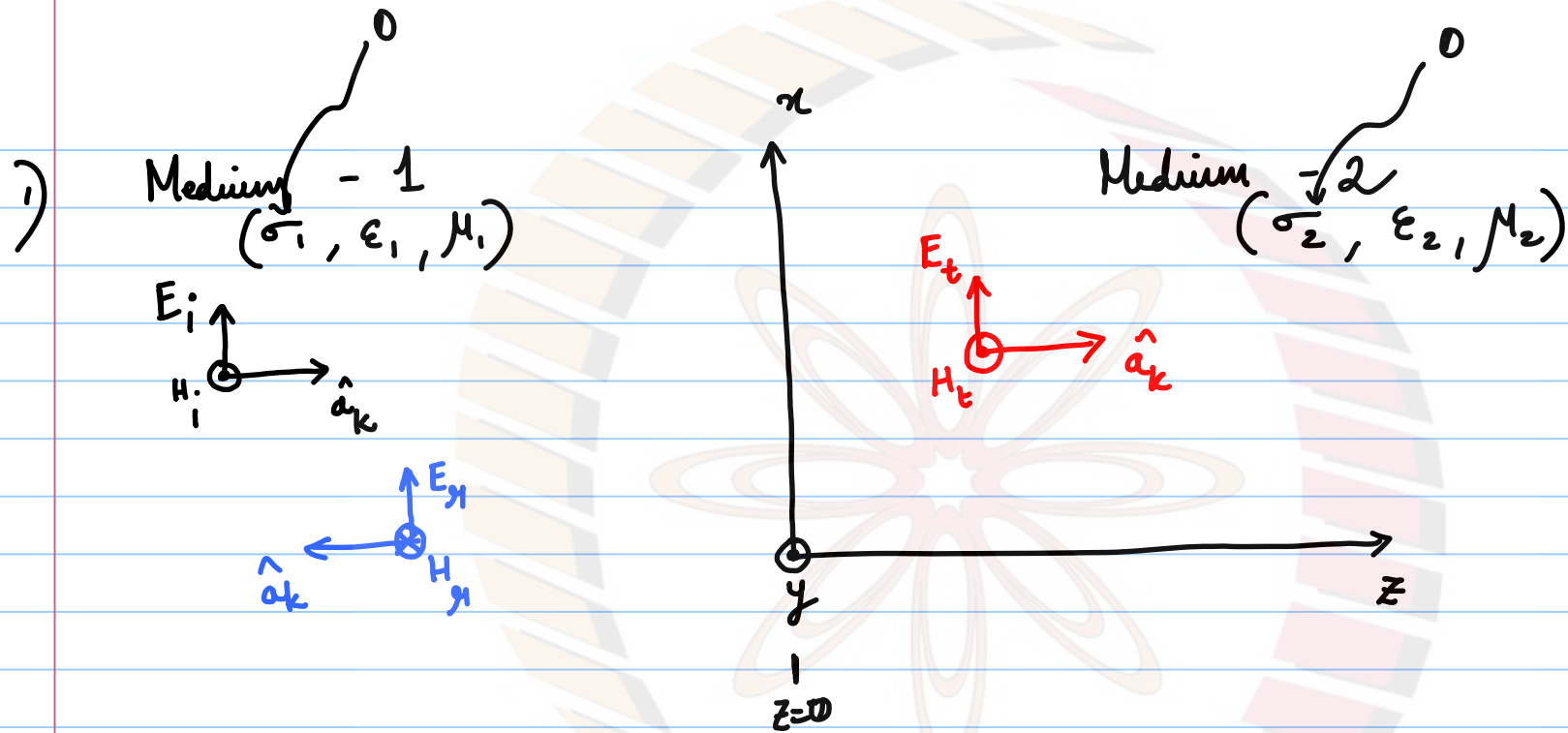
$$\begin{aligned} \underline{E} &= \underline{E}_0 e^{-j\beta \hat{n} \cdot \underline{r}} \\ &= \underline{E}_0 e^{-j\beta \hat{n} \cdot \underline{r}} \quad \underline{k} = \underline{E}_0 e^{-j\underline{k} \cdot \underline{r}} \end{aligned}$$

$$\begin{aligned} \underline{E} &= \underline{E}_0 e^{-j\underline{k} \cdot \underline{r}} \\ &= \underline{E}_0 e^{-j\beta(x \cos \phi_x)} e^{-j\beta(y \cos \phi_y)} e^{-j\beta(z \cos \phi_z)} \end{aligned}$$

$$\frac{\omega}{k} \rightarrow \text{phase velocity}$$

$$V_{pz} = \frac{\omega}{k_z} = \frac{\omega}{\beta \cos \phi_z} = \frac{V_0}{\cos \phi_z}$$

$$\text{Group velocity} = \frac{d\omega}{dk} \quad \text{cannot be higher than } c.$$



2)

$$\begin{aligned}
 E_i(z) &= E_{i0} e^{-\gamma_1 z} \hat{a}_x \\
 H_i(z) &= H_{i0} e^{-\gamma_1 z} \hat{a}_y \\
 &= \frac{E_{i0}}{\eta_1} e^{-\gamma_1 z} \hat{a}_y
 \end{aligned}
 \left. \vphantom{\begin{aligned} E_i(z) \\ H_i(z) \end{aligned}} \right\} \text{Incident field}$$

$$\begin{aligned}
 3) \quad E_r(z) &= E_{r0} e^{\gamma_1 z} \hat{a}_x \\
 H_r(z) &= H_{r0} e^{\gamma_1 z} (-\hat{a}_y) \\
 &= -\frac{E_{r0}}{\eta_1} e^{\gamma_1 z} \hat{a}_y
 \end{aligned}
 \quad \left. \vphantom{\begin{aligned} E_r(z) \\ H_r(z) \end{aligned}} \right\} \text{Reflected field}$$

$$\begin{aligned}
 4) \quad E_t(z) &= E_{t0} e^{-\gamma_2 z} \hat{a}_x \\
 H_t(z) &= H_{t0} e^{-\gamma_2 z} \hat{a}_y
 \end{aligned}$$

5) Total fields in Medium 1 :-

$$E_1 = E_i + E_r, \quad H_1 = H_i + H_r$$

In medium 2,

$$E_2 = E_t, \quad H_2 = H_t$$

b)

At $z = 0$,

$E_{\text{tangential}} \rightarrow \text{Continuous}$
 $H_{\text{tangential}} \rightarrow \text{Continuous}$

$$E_{1\text{tan}} = E_{2\text{tan}} \quad \& \quad H_{1\text{tan}} = H_{2\text{tan}}$$

$$E_i(0) + E_r(0) = E_t(0) \quad \text{--- (1)}$$

\uparrow
 $z=0$

$$H_i(0) + H_r(0) = H_t(0)$$

$$\frac{E_i(0)}{\eta_1} + \frac{E_r(0)}{\eta_1} = \frac{E_t(0)}{\eta_2} \quad \text{--- (2)}$$

$$\boxed{\frac{E_{r0}}{E_{i0}} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}}$$

$$= \Gamma$$

$$\boxed{\frac{E_{t0}}{E_{i0}} = \left(\frac{2\eta_2}{\eta_2 + \eta_1} \right)}$$

$$= \mathcal{T}$$

$$1 + \Gamma = \mathcal{T}$$

$$1 \text{ Medium} \rightarrow \sigma_1 = 0, \quad \eta_1 \neq 0$$

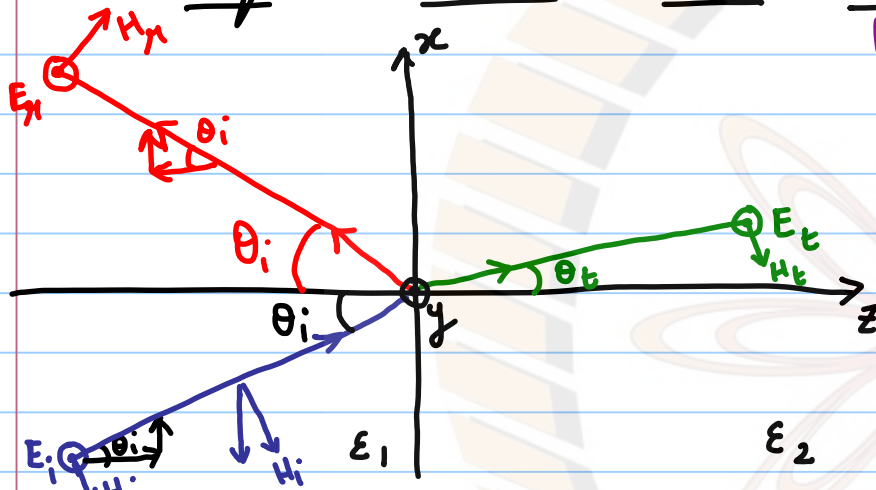
$$2 \text{ Medium} \rightarrow \sigma_2 = \infty$$

$$\Gamma = -1, \quad \mathcal{T} = 0$$

$$\begin{aligned} E_1 &= E_i + E_r = \left(E_{i0} e^{-\gamma_1 z} + E_{r0} e^{\gamma_1 z} \right) \hat{a}_x \\ &= E_{i0} e^{-j\beta_1 z} + E_{r0} e^{+j\beta_1 z} \\ &= E_{i0} e^{-j\beta_1 z} + -E_{i0} e^{+j\beta_1 z} \\ &= -2j E_{i0} \sin(\beta_1 z) \hat{a}_x \end{aligned}$$

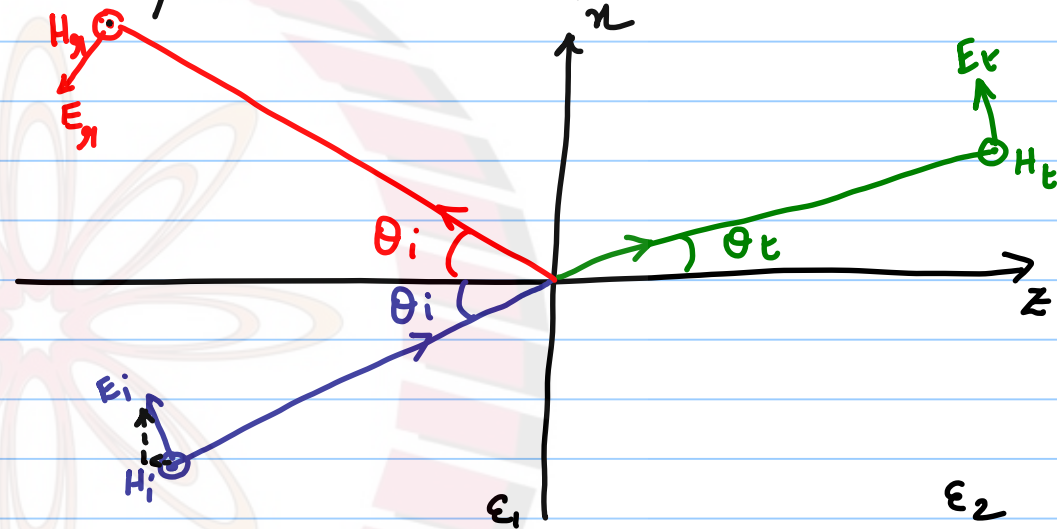
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Oblique Incidence on Dielectric/Dielectric interfaces



Plane of incidence :- xz plane

E-field :- \perp to plane of incidence
 \perp polarization



H-field :- \perp to plane of incidence.
 \parallel polarization

1) Incident wave :-

$$\text{E-field :- } \underline{E}_i = E_{i0} e^{-j \underline{k}_i \cdot \underline{r}}$$

$$\underline{k}_i = k_x \hat{x} + k_y \hat{y} + k_z \hat{z}$$

$$= \beta_1 \hat{n}$$

$$n_x, n_y, n_z$$

1) Incident wave :-

$$\text{E-field : } \underline{E}_i = E_{i0} e^{-j \underline{k}_i \cdot \underline{r}}$$

$$\underline{k}_i = k_x \hat{x} + k_y \hat{y} + k_z \hat{z}$$

$$= \beta_1 \hat{n}$$

$$n_x, n_y, n_z$$

$$n = [\sin \theta_i, 0, \cos \theta_i]$$

$$n = [\sin \theta_i, 0, \cos \theta_i]$$

$$\Rightarrow \underline{k}_i = \beta_1 (\sin \theta_i \hat{x} + 0 \hat{y} + \cos \theta_i \hat{z}) \Rightarrow k_i = \beta_1 \sin \theta_i \hat{x} + \beta_1 \cos \theta_i \hat{z}$$

$$= \beta_1 \sin \theta_i \hat{x} + \beta_1 \cos \theta_i \hat{z}$$

$$\text{Now, } \underline{r} = x \hat{x} + y \hat{y} + z \hat{z}$$

$$\Rightarrow \underline{E}_i = \underline{E}_{i0} e^{-j \beta_1 (x \sin \theta_i + z \cos \theta_i)} \Rightarrow \underline{E}_i = \underline{E}_{i0} e^{-j \beta_1 (x \sin \theta_i + z \cos \theta_i)}$$

2) Reflected Wave :-

$$\underline{E}_r = \underline{E}_{r0} e^{-j \underline{k}_r \cdot \underline{r}}$$

$$\underline{k}_r = \beta \hat{n}$$

$$n = [\sin \theta_i, 0, -\cos \theta_i]$$

$$\underline{k}_r = \beta (\sin \theta_i \hat{x} - \cos \theta_i \hat{z})$$

$$\underline{r} = x \hat{x} + y \hat{y} + z \hat{z}$$

$$\underline{E}_r = \underline{E}_{r0} e^{-j\beta_1 (x \sin \theta_i - z \cos \theta_i)}$$

$$\underline{E}_r = \underline{E}_{r0} e^{-j\beta_1 (x \sin \theta_i - z \cos \theta_i)}$$

3) Transmitted wave:-

E-field :- $\underline{E}_t = \underline{E}_{t0} e^{-j\underline{k}_t \cdot \underline{r}}$

$$\underline{E}_t = \underline{E}_{t0} e^{-j\beta_2 (x \sin \theta_t + z \cos \theta_t)}$$

$$\underline{E}_t = \underline{E}_{t0} e^{-j\beta_2 (x \sin \theta_t + z \cos \theta_t)}$$

$$3) |H_i| = \frac{|E_i|}{\eta_1}$$

$$|H_r| = \frac{|E_r|}{\eta_1}$$

$$|H_t| = \frac{|E_t|}{\eta_2}$$

The interface is at $z=0$
Apply boundary conditions

$$E_i + E_r = E_t$$

$$H_i \cos \theta_i - H_r \cos \theta_i = H_t \cos \theta_t$$

At $z=0$,

$$E_{i0} + E_{r0} = E_{t0} \quad \text{--- (1)}$$

$$\frac{E_{i0} \cos \theta_i}{\eta_1} - \frac{E_{r0} \cos \theta_i}{\eta_1} = \frac{E_{t0} \cos \theta_t}{\eta_2} \quad \text{--- (2)}$$

$$\Gamma_{\perp} = \frac{E_{r0}}{E_{i0}} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

$$\Uparrow_{\perp} = \frac{E_{t0}}{E_{i0}} = \frac{2 \eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

The interface is at $z=0$,
Apply boundary conditions:

At $z=0$,

$$E_{i0} \cos \theta_i - E_{r0} \cos \theta_i = E_{t0} \cos \theta_t \quad \text{--- (1)}$$

$$H_{i0} + H_{r0} = H_{t0} \quad \text{--- (2)}$$

$$\frac{E_{i0}}{\eta_1} + \frac{E_{r0}}{\eta_1} = \frac{E_{t0}}{\eta_2}$$

$$\Gamma_{\parallel} = \frac{E_{r0}}{E_{i0}} = \frac{\eta_1 \cos \theta_i - \eta_2 \cos \theta_t}{\eta_1 \cos \theta_i + \eta_2 \cos \theta_t}$$

$$\Uparrow_{\parallel} = \frac{E_{t0}}{E_{i0}} = \frac{2 \eta_2 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i}$$

For $\Gamma_{\perp} = 0$,

$$\eta_2 \cos \theta_i - \eta_1 \cos \theta_t = 0$$

Let $\theta_B = \theta_i$

$$\eta_2 \cos \theta_B - \eta_1 \cos \theta_t = 0$$

$$\Rightarrow \theta_{B_{\perp}} = \cos^{-1} \left\{ \frac{\eta_1}{\eta_2} \cos \theta_t \right\}$$

Brewster's angle

For $\Gamma_{\parallel} = 0$,

$$\eta_1 \cos \theta_i - \eta_2 \cos \theta_t = 0$$

Let $\theta_B = \theta_i$

$$\eta_1 \cos \theta_B - \eta_2 \cos \theta_t = 0$$

$$\Rightarrow \theta_{B_{\parallel}} = \cos^{-1} \left\{ \frac{\eta_2}{\eta_1} \cos \theta_t \right\}$$

Brewster's angle

Snell's law,

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$$\text{or } \sin \theta_t = \frac{n_1}{n_2} \sin \theta_i$$

$$\beta_1 = \frac{2\pi}{\lambda_0/n_1}, \quad \beta_2 = \frac{2\pi}{\lambda_0/n_2}$$

$$\Rightarrow \sin \theta_t = \frac{\beta_1}{\beta_2} \sin \theta_B$$

$$\cos \theta_t = \sqrt{1 - \frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_B}$$

$$\beta_1 = \omega \sqrt{\mu_1 \epsilon_1}, \quad \beta_2 = \omega \sqrt{\mu_2 \epsilon_2}$$

$$\Rightarrow \eta_2 \cos \theta_B - \eta_1 \sqrt{1 - \frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_B} = 0$$

$$\& \quad \eta_1 = \sqrt{\frac{\mu_1}{\epsilon_1}}, \quad \eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}}$$

$$\theta_{B_{\perp}} = \tan^{-1} \left\{ \sqrt{\frac{\mu_2}{\mu_1}} \sqrt{\frac{\mu_2 \epsilon_1 - \mu_1 \epsilon_2}{\mu_2 \epsilon_2 - \mu_1 \epsilon_1}} \right\}$$

For $\mu_1 = \mu_2 = \mu_0$, $\Rightarrow \theta_{B_{\perp}} = \tan^{-1} \left\{ \sqrt{\frac{\mu_0}{\mu_0} \left(\frac{\epsilon_1 - \epsilon_2}{\epsilon_2 - \epsilon_1} \right)} \right\}$

$$\theta_{B_{||}} = \tan^{-1} \left\{ \sqrt{\frac{\epsilon_2}{\epsilon_1}} \sqrt{\frac{\mu_1 \epsilon_2 - \mu_2 \epsilon_1}{\mu_2 \epsilon_2 - \mu_1 \epsilon_1}} \right\}$$

For $\mu_1 = \mu_2 = \mu_0$, $\theta_{B_{||}} = \tan^{-1} \left\{ \sqrt{\frac{\epsilon_2}{\epsilon_1}} \sqrt{\frac{\mu_0 \epsilon_2 - \mu_0 \epsilon_1}{\mu_0 \epsilon_2 - \mu_0 \epsilon_1}} \right\}$

Majority of the materials have $\mu_1 = \mu_2 = \mu_0$

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

or

$$\beta_1 \sin \theta_i = \beta_2 \sin \theta_t$$

$$\Rightarrow \sin \theta_t = \frac{\beta_1}{\beta_2} \sin \theta_i$$

$$\beta_1 = \frac{2\pi}{\lambda_0/n_1}$$

$$\beta_2 = \frac{2\pi}{\lambda_0/n_2}$$

If $\sin \theta_t = 1$, for a given material system (n_1, n_2), at a specific angle of incidence θ_i , that angle of incidence is called Critical Angle.

θ_t at $\theta_i = \theta_c$ is $\pi/2$.

$$\frac{\beta_1}{\beta_2} \sin \theta_i \geq 1$$

$$\frac{\omega \sqrt{\mu_1 \epsilon_1}}{\omega \sqrt{\mu_2 \epsilon_2}} \sin \theta_i \geq 1$$

$$\Rightarrow \sin \theta_i \geq \left(\frac{\sqrt{\mu_2 \epsilon_2}}{\sqrt{\mu_1 \epsilon_1}} \right)$$

$$\Rightarrow \sin \theta_i \geq \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\sqrt{\frac{\epsilon_2}{\epsilon_1}} < 1$$

$$\sqrt{\epsilon_2} < \sqrt{\epsilon_1}$$

$$\Gamma_{||} = \frac{E_{ro}}{E_{io}} = \frac{\eta_1 \cos \theta_i - \eta_2 \cos \theta_t}{\eta_1 \cos \theta_i + \eta_2 \cos \theta_t}$$

$$= \frac{\eta_1 \cos \theta_i - \eta_2 \sqrt{1 - \frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_i}}{\eta_1 \cos \theta_i + \eta_2 \sqrt{1 - \frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_i}}$$

$$= \frac{\eta_1 \cos \theta_i - j \eta_2 \sqrt{\frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_i - 1}}{\eta_1 \cos \theta_i + j \eta_2 \sqrt{\frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_i - 1}}$$

Let $\eta_1 \cos \theta_i = X$

Let $\eta_2 \sqrt{\frac{\beta_1^2}{\beta_2^2} \sin^2 \theta_i - 1} = Y$

$$= \frac{X - jY}{X + jY}$$

$$|\Gamma_{||}| = 1$$

Total Internal Reflection (TIR)

Also $|\Gamma_{\perp}| = 1$

$$E_i = E_{i\parallel} + E_{i\perp} e^{j\phi}$$

Let incident wave be linearly polarized,
 $\phi = 0$.

$E_{r\parallel}$ $E_{r\perp}$ with no phase.

Reflected wave \rightarrow linearly polarized
 Transmitted " \rightarrow " "

2. Circularly polarized :-

$$|E_{i\parallel}| = |E_{i\perp}|$$

$$\phi = \pm \pi/2$$

Reflected $\rightarrow \phi = \pm \pi/2$, $E_{r\parallel} \neq E_{r\perp}$, Elliptical
 Transmitted $\rightarrow \phi = \pm \pi/2$, $E_{t\parallel} \neq E_{t\perp}$, "

Perpendicular polarization (Simulation setup):-

1) H_x, E_y, H_z xz plane \rightarrow propagation
 k_x, k_z

2) $\nabla \times \underline{H} = \epsilon \frac{\partial \underline{E}}{\partial t}$

LHS $\nabla \times \underline{H} =$

$$\begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & 0 & \frac{\partial}{\partial z} \\ H_x & 0 & H_z \end{vmatrix}$$
$$= \hat{i} (0) - \hat{j} \left(\frac{\partial H_z}{\partial x} - \frac{\partial H_x}{\partial z} \right) + \hat{k} (0)$$
$$= \hat{j} \left(\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} \right)$$

RHS

$$\epsilon \frac{\partial \underline{E}}{\partial t} = \epsilon \frac{\partial E_y}{\partial t} \hat{j}$$

$$\epsilon \frac{\partial E_y}{\partial t} \cong \epsilon \frac{E_y(x, z, t + \Delta t) - E_y(x, z, t)}{\Delta t}$$

LHS in difference form,

$$\text{i), } \frac{\partial H_x}{\partial z} \cong \frac{H_x(x, z, t) - H_x(x, z - \Delta z, t)}{\Delta z}$$

$$\text{ii), } \frac{\partial H_z}{\partial x} \cong \frac{H_z(x, z, t) - H_z(x - \Delta x, z, t)}{\Delta x}$$

LHS = RHS & Bringing unknown quantity to the left,

$$\underline{\underline{E_y(x, z, t + \Delta t) = E_y(x, z, t) + \frac{\Delta t}{\epsilon \Delta} \left[H_x(x, z, t) - H_x(x, z - \Delta z, t) - H_z(x, z, t) + H_z(x - \Delta x, z, t) \right]}}$$

$$\begin{aligned} 2) \quad \nabla \times \underline{E} &= - \frac{\partial \underline{B}}{\partial t} \\ &= -\mu \frac{\partial \underline{H}}{\partial t} \end{aligned}$$

$$\begin{aligned} \underline{\underline{LHS}} \quad \nabla \times \underline{E} &= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & 0 & \frac{\partial}{\partial z} \\ 0 & E_y & 0 \end{vmatrix} \\ &= \hat{i} \left(-\frac{\partial E_y}{\partial z} \right) - \hat{j} (0) + \hat{k} \left(\frac{\partial E_y}{\partial x} \right) \end{aligned}$$

$$\underline{\text{RHS}} - \mu \frac{\partial \underline{H}}{\partial t} = -\mu \frac{\partial H_x}{\partial t} \hat{i} - \mu \frac{\partial H_z}{\partial t} \hat{k}$$

LHS = RHS & Equating \hat{i} components,

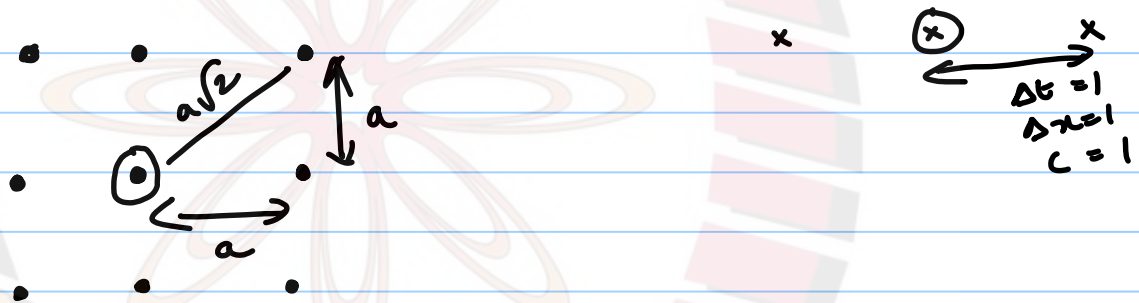
$$-\frac{\partial E_y}{\partial z} = -\mu \frac{\partial H_x}{\partial t}$$

$$\Rightarrow \frac{H_x(x, z, t + \Delta t) - H_x(x, z, t)}{\Delta t} = \frac{1}{\mu \Delta} \left[E_y(x, z + \Delta z, t) - E_y(x, z, t) \right]$$

LHS = RHS & Equating \hat{k} components,

$$\frac{\partial E_y}{\partial x} = -\mu \frac{\partial H_z}{\partial t}$$

$$H_z(x, z, t + \Delta t) = H_z(x, z, t) - \frac{1}{\mu \Delta} \left\{ \dots \right\}$$



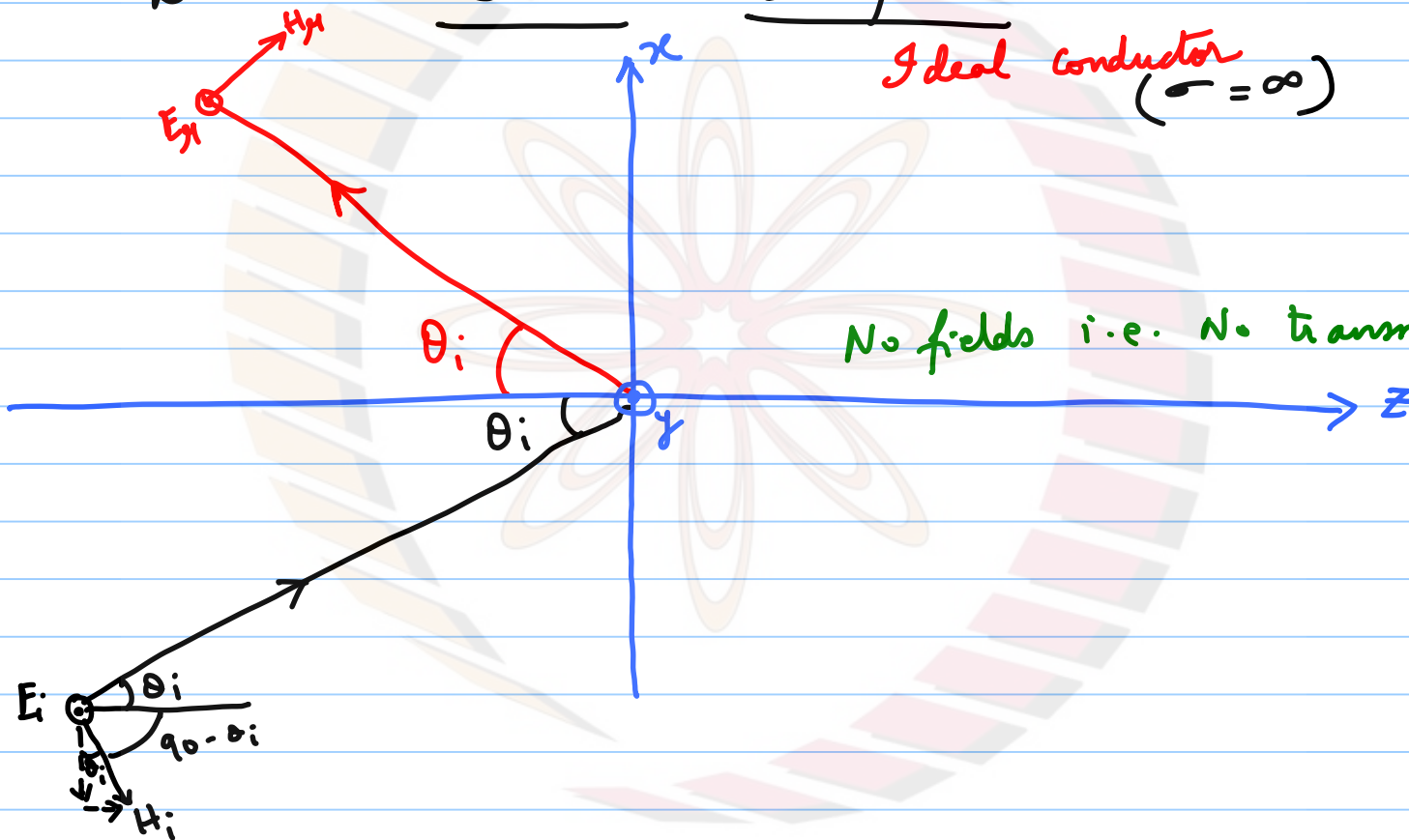
NPTTEL

Dielectric - Ideal Conductor Interface

Ideal Conductor ($\sigma = \infty$)

No fields i.e. No transmission

Ir polarization



$$\underline{E}_i = E_{i0} e^{-j\beta_1 (x \sin \theta_i + z \cos \theta_i)} \hat{y}$$

$$\underline{H}_i = \frac{E_{i0}}{\eta_1} e^{-j\beta_1 (x \sin \theta_i + z \cos \theta_i)} \left(-\cos \theta_i \hat{x} + \sin \theta_i \hat{z} \right)$$

$$\underline{E}_r = E_{r0} e^{-j\beta_1 (x \sin \theta_i - z \cos \theta_i)} \hat{y}$$

$$\underline{H}_r = \frac{E_{r0}}{\eta_1} e^{-j\beta_1 (x \sin \theta_i - z \cos \theta_i)} \left(\cos \theta_i \hat{x} + \sin \theta_i \hat{z} \right)$$

Apply boundary conditions at $z=0$;

$$\underline{E}_{tan} = (\underline{E}_i + \underline{E}_r)_{tan} = 0$$

$$\underline{H}_{norm} = (\underline{H}_i + \underline{H}_r)_{norm} = 0$$

At $z=0$,

$$E_{i0} e^{-j\beta_1(x \sin \theta_i)} + E_{r0} e^{-j\beta_1(x \sin \theta_i)} = 0$$

$$\Rightarrow E_{r0} e^{-j\beta_1 x \sin \theta_i} = -E_{i0} e^{-j\beta_1 x \sin \theta_i}$$

$$\Rightarrow \boxed{E_{r0} = -E_{i0}}$$

$$\Gamma = 1 \angle 180^\circ \quad \underline{\underline{(-1)}}$$

At $z=0$,

$$\frac{E_{i0}}{\eta_1} \sin \theta_i e^{-j\beta_1 x \sin \theta_i} + \frac{E_{r0}}{\eta_1} \sin \theta_i e^{-j\beta_1 x \sin \theta_i} = 0$$

$$\Rightarrow \frac{E_{r0}}{\eta_1} \sin \theta_i e^{-j\beta_1 x \sin \theta_i} = - \frac{E_{i0}}{\eta_1} \sin \theta_i e^{-j\beta_1 x \sin \theta_i}$$

$$\Rightarrow \boxed{E_{r0} = -E_{i0}}$$

Total fields in Medium ① :-

$$\begin{aligned}\underline{E} &= \underline{E}_i + \underline{E}_r \\ &= E_{i0} e^{-j\beta_1 x \sin \theta_i} \left(e^{-j\beta_1 z \cos \theta_i} - e^{j\beta_1 z \cos \theta_i} \right) \hat{y} \\ &= -2j E_{i0} \sin(\beta_1 z \cos \theta_i) e^{-j\beta_1 x \sin \theta_i} \hat{y}\end{aligned}$$

||| \hat{y}

$$\begin{aligned}\underline{H} &= \underline{H}_i + \underline{H}_r \\ &= -2 \frac{E_{i0}}{\eta_1} \cos^{\theta_i}(\cos(\beta_1 z \cos \theta_i)) e^{-j\beta_1 x \sin \theta_i} \hat{x} \\ &\quad - 2j \frac{E_{i0}}{\eta_1} \sin \theta_i \left(\sin(\beta_1 z \cos \theta_i) \right) e^{-j\beta_1 x \sin \theta_i} \hat{z}\end{aligned}$$

1)

$$\underline{E_y} = -2j E_{i0} \sin(\beta_1 z \cos \theta_i) e^{-j\beta_1 x \sin \theta_i} \hat{y}$$

2) The zeros of the electric field, are located at,

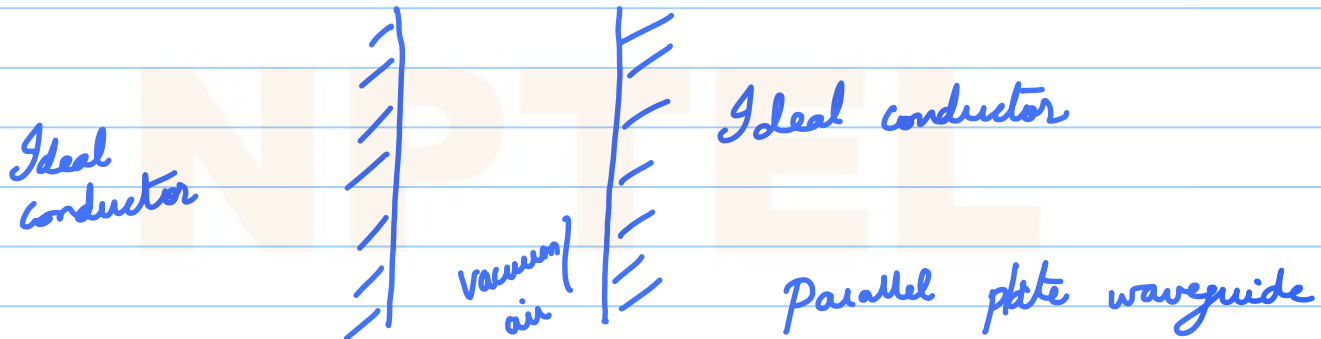
$$\beta_1 z \cos \theta_i = m\pi$$

$$\Rightarrow z = \frac{m\pi}{\beta_1 \cos \theta_i}$$

$$\beta_1 = \frac{2\pi}{\lambda_1}$$

$$z = \frac{m\lambda_1}{2 \cos \theta_i}$$

3)



4) Construct a parallel plate waveguide with distance b/w the plates being "d"

$$\cos \theta_i = \frac{m\lambda_1}{2d}$$

Integer

$|\cos \theta_i| \leq 1$

There are a finite number of angles for a given "d".

5)

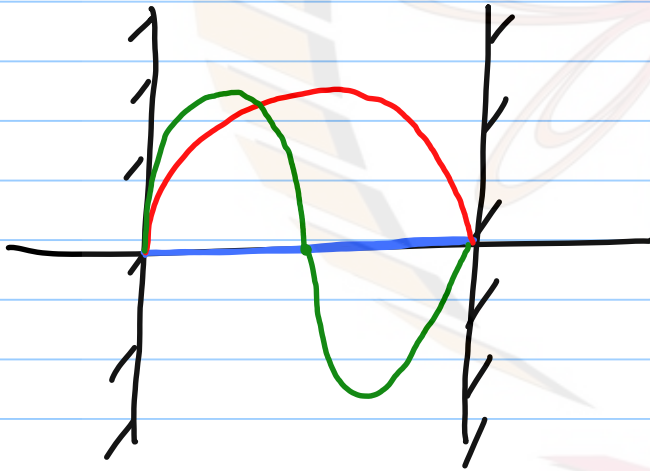
$$-2j E_{i0} \sin(\beta_1 z \cos \theta_i) e^{-j\beta_1 x \sin \theta_i}$$

$$= -2j E_{i0} \sin\left(\beta_1 z \frac{m\lambda_1}{2d}\right) e^{-j\beta_1 x \sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}}$$

6) Let $\beta_w = \beta_1 \sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}$

7) Propagation constant in the waveguide is different from the homogeneous bulk medium:

8)



$m = 0$

$m = 1$ (Max. e-field at center of waveguide)

$m = 2$ (Center has no e-field)

Modes of the 1st plate waveguide

9)

$$\beta_w = \beta_1 \sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}$$

$$\rightarrow \frac{2\pi}{\lambda_1} = \frac{2\pi f_1}{v_1}$$

$$\Rightarrow \beta_1 \geq \frac{m\pi}{d}$$

$$\Rightarrow \frac{2\pi}{\lambda_1} \geq \frac{m\pi}{d} \quad \text{or} \quad \boxed{\lambda_1 \leq \frac{2d}{m}} \quad \text{Cut-off wavelength}$$

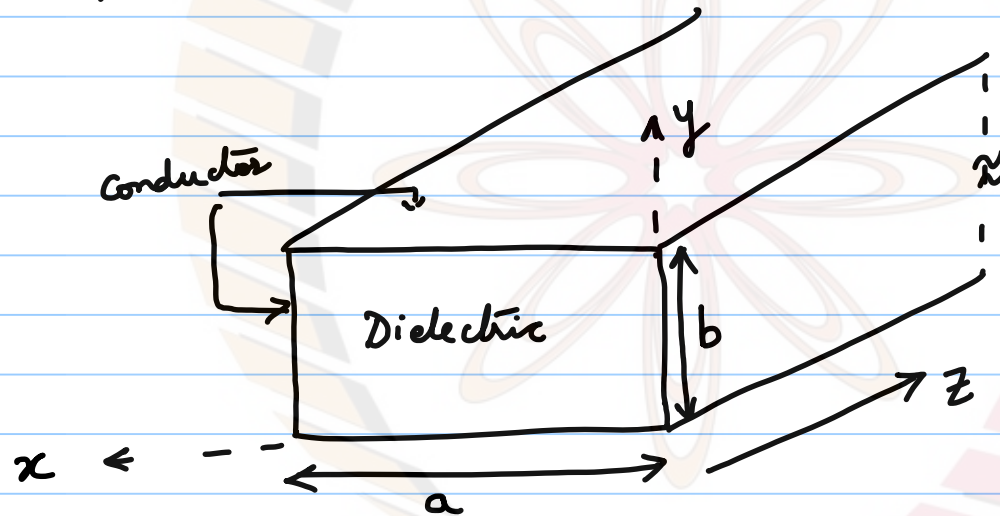
$$\text{or} \quad \boxed{f \geq \frac{\|v_1\|}{2d}} \quad \text{Cut-off frequency.}$$

NPTTEL

Rectangular waveguides

1) Key ideas/results are important.

2)



3) If $H_z = 0$; $E_z \neq 0$

TM polarization (Transverse Magnetic)

4) $E_z(x, y, z)$

$$\frac{\partial^2 E_z}{\partial x^2} + \frac{\partial^2 E_z}{\partial y^2} + \frac{\partial^2 E_z}{\partial z^2} + \omega^2 \mu \epsilon E_z = 0$$

Method of separation of variables :-

$$E_z(x, y, z) = X(x) Y(y) Z(z)$$

$$YZ \frac{d^2 X}{dx^2} + XZ \frac{d^2 Y}{dy^2} + XY \frac{d^2 Z}{dz^2} + \omega^2 \mu \epsilon XYZ = 0$$

Dividing both sides by XYZ ,

$$\Rightarrow \frac{1}{X} \frac{d^2 X}{dx^2} + \frac{1}{Y} \frac{d^2 Y}{dy^2} + \frac{1}{Z} \frac{d^2 Z}{dz^2} + \omega^2 \mu \epsilon = 0$$

$$\Rightarrow \frac{1}{X} \frac{d^2 X}{dx^2} + A^2 = 0$$

or $\boxed{\frac{1}{X} \frac{d^2 X}{dx^2} = -A^2}$ ————— ①

$\boxed{\frac{1}{Y} \frac{d^2 Y}{dy^2} = -B^2}$ ————— ②

$\boxed{\frac{1}{Z} \frac{d^2 Z}{dz^2} = -\beta^2}$ ————— ③

Assume general solutions of the form,

$$\begin{aligned} X &= C_1 \cos Ax + C_2 \sin Ax \\ Y &= C_3 \cos By + C_4 \sin By \\ Z &= C_5 e^{-j\beta z} + C_6 e^{+j\beta z} \end{aligned} \left. \begin{array}{l} \\ \\ \end{array} \right\} \begin{array}{l} \text{Standing wave patterns} \\ \\ \text{Traveling wave} \end{array}$$

If the waveguide is infinitely long,

$$C_6 = 0$$

$$\left. \begin{array}{l} \text{at } x=0 \\ \text{at } y=0 \\ \text{at } x=a \\ \text{at } y=b \end{array} \right\} E_z = 0$$

$$\text{at } x=0, E_z = 0 \Rightarrow C_1 = 0$$

$$\text{at } y=0, E_z = 0 \Rightarrow C_3 = 0$$

$$\text{at } \begin{array}{l} x=a \\ y=b \end{array}, E_z = 0$$

As of now,

$$E_z(x, y, z) = (C_2 \sin Ax) (C_4 \sin By) (C_5 e^{-j\beta z})$$

$$\text{At } x=a, E_z=0 \Rightarrow A = \frac{m\pi}{a}$$

$$\text{At } y=b, E_z=0 \Rightarrow B = \frac{n\pi}{b}$$

$$E_z(x, y, z) = \left[C_2 \sin \frac{m\pi}{a} x \right] \left[C_4 \sin \frac{n\pi}{b} y \right] \left[C_5 e^{-j\beta z} \right]$$

$$= C \left[\sin \frac{m\pi}{a} x \right] \left[\sin \frac{n\pi}{b} y \right] \left[e^{-j\beta z} \right]$$

$m=0, n=0$ is not possible

$m=0, n=1$ " " "

$m=1, n=0$ " " "

$m=1, n=1$

TM_{mn}

$$1) \quad E_x = \frac{-j\omega\mu}{\omega^2\mu\epsilon - \beta^2} \frac{\partial H_z}{\partial y} - \frac{j\beta}{\omega^2\mu\epsilon - \beta^2} \frac{\partial E_z}{\partial x}$$

$\overset{0.}{\curvearrowright}$

$$E_x = \frac{-j\beta}{\omega^2\mu\epsilon - \beta^2} \left(\frac{m\pi}{a}\right) \left(\cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta z} \right)$$

$$2) \quad E_y = \frac{j\omega\mu}{\omega^2\mu\epsilon - \beta^2} \frac{\partial H_z}{\partial x} - \frac{j\beta}{\omega^2\mu\epsilon - \beta^2} \frac{\partial E_z}{\partial y}$$

$\overset{0.}{\curvearrowright}$

$$E_y = \frac{-j\beta}{\omega^2\mu\epsilon - \beta^2} \left(\frac{n\pi}{b}\right) \left(\sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{-j\beta z} \right)$$

3) (i) Fields \rightarrow Patterns (Depend on m for parallel plate waveguide, m, n for rectangular waveguide)
 \rightarrow Discrete patterns

↳ Sinusoidal variations in transversal directions

$$(ii) \quad \omega_{\mu\epsilon}^2 = \beta^2 + \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2$$

$$\beta^2 = \omega_{\mu\epsilon}^2 - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2$$

$$\Rightarrow \beta = \sqrt{\omega_{\mu\epsilon}^2 - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

$$\omega_{\mu\epsilon}^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 \quad \text{worst case}$$

$$\Rightarrow \omega_c = \frac{1}{\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$\omega_{\text{input}} > \omega_c$
Cut-off frequency

NPTTEL

$$1) \beta_w = \beta_1 \sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}$$

$$2) \text{Phase Velocity} = \frac{\omega}{\beta_w} = \frac{\omega}{\beta_1 \sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}}$$

$$= \frac{v_1}{\sqrt{1 - \left(\frac{m\lambda_1}{2d}\right)^2}}$$

3) From prior lectures,

$$\lambda_{\text{cut-off}} = \frac{2d}{m}$$

&

$$f_{\text{cut-off}} = \frac{mv_1}{2d}$$

$$4) \quad V_p = \frac{V_1}{\sqrt{1 - \left(\frac{\lambda_1}{\lambda_{cut} - \lambda} \right)^2}} = \frac{V_1}{\sqrt{1 - \left(\frac{f_{cut} - f}{f} \right)^2}}$$

5) Phase velocity is a function of frequency.
 \rightarrow Means wave dispersion

6) As $f \uparrow \infty$, $V_p = V_1$
 But at all lower frequencies, $V_p > V_1$

7) Phase velocity does not convey information.

8) In the simplest case, a single tone amplitude modulation, can be achieved by 2 sinusoids. (of different frequencies & of different wavelengths)

$$9) \cos((\omega + \Delta\omega)t - (\beta + \Delta\beta)z) + \cos((\omega - \Delta\omega)t - (\beta - \Delta\beta)z)$$

$$10) 2 \cos(\omega t - \beta z) \cos(\Delta\omega t - \Delta\beta z)$$

$$11) V_p = \frac{\omega}{\beta} \quad V_g = \frac{\Delta\omega}{\Delta\beta}$$

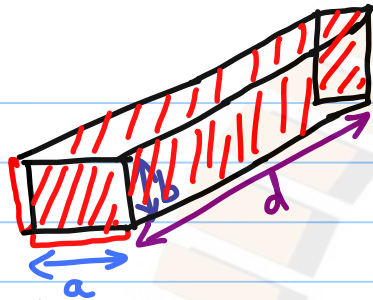
$$\text{As } \begin{matrix} \Delta\omega \rightarrow 0 \\ \Delta\beta \rightarrow 0 \end{matrix}, \quad V_g = \frac{d\omega}{d\beta}$$

$$12) V_g = \frac{d\omega}{d\beta} = v_1 \sqrt{1 - \left(\frac{f_{cut} - f}{f} \right)^2}$$

$$\text{As } f \uparrow \infty, \quad V_g = v_1$$

$$\text{For All other lower } f, \quad V_g < v_1$$

$$\therefore V_g \leq v_1$$



CAVITY

For TM_{mn} modes in rectangular waveguides that we have already seen,

$$E_{z\text{forward}} = C \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{-j\beta z}$$

$$E_{z\text{backward}} = D \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) e^{+j\beta z}$$

Total E-field,

$$E_{z\text{total}} = E_{z\text{forward}} + E_{z\text{backward}}$$

$$\text{At } z=0, E_{z\text{total}} = 0, \text{ \& at } z=d, E_{z\text{total}} = 0$$

$$\Rightarrow C = -D$$

$$\begin{aligned}
 E_{z_{total}} &= C \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) \left[e^{-j\beta z} - e^{+j\beta z} \right] \\
 &= -2j C \sin\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right) \underline{\underline{\sin(\beta z)}}
 \end{aligned}$$

At $z=d$,

$$\sin(\beta z) = \sin(\beta d) = 0$$

$$\Rightarrow \beta d = l\pi, \quad l = 1, 2, 3, \dots$$

$$\Rightarrow \beta = \frac{l\pi}{d}$$

As before,

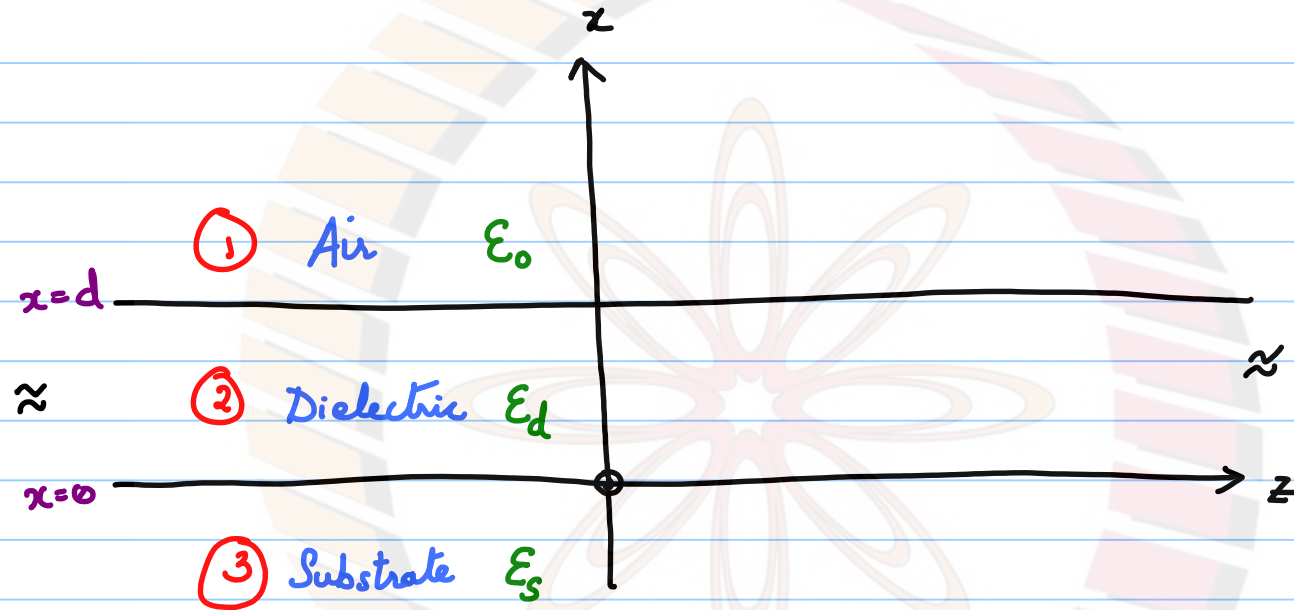
$$\omega_{HE}^2 = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{l\pi}{d}\right)^2$$

$$\Rightarrow \omega = \frac{1}{\sqrt{\mu\epsilon}} \left[\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{l\pi}{d}\right)^2 \right]^{1/2}$$

→ Cavity Resonance Frequencies.

TM_{mnl}

NPTTEL



TE polarization.

$$E_z = 0$$

$$H_z \neq 0$$

$$H_z = X(x) e^{-j\beta z}$$

$$\underbrace{\frac{1}{X} \frac{d^2 X}{dx^2}} - \beta^2 + \omega^2 \mu \epsilon = 0$$

$$\text{Let } \frac{1}{X} \frac{d^2 X}{dx^2} = \text{constant} = \pm k^2$$

$$\Rightarrow \frac{d^2 X}{dx^2} = \pm k^2 X$$

Region 1

$$\frac{d^2 X_1}{dx^2} = k_1^2 X_1$$

$$k_1^2 - \beta^2 + \omega^2 \mu \epsilon_0 = 0 \quad \text{--- (1)}$$

Region 2

$$\frac{d^2 X_2}{dx^2} = -k_2^2 X_2$$

$$-k_2^2 - \beta^2 + \omega^2 \mu \epsilon_d = 0 \quad \text{--- (2)}$$

Region 3

$$\frac{d^2 X_3}{dx^2} = k_3^2 X_3$$

$$k_3^2 - \beta^2 + \omega^2 \mu \epsilon_s = 0 \quad \text{--- (3)}$$

$$X_1 = A_1 e^{-k_1 x} + A_2 e^{k_1 x}$$

$\hookrightarrow A_2 \equiv 0$

$$X_2 = A_3 \cos k_2 x + A_4 \sin k_2 x$$

$$X_3 = A_5 e^{-k_3 x} + A_6 e^{k_3 x}$$

$\hookrightarrow \equiv 0$

$$H_{z1} = A_1 e^{-k_1 x} e^{-j\beta z}$$

$$H_{z2} = [A_3 \cos k_2 x + A_4 \sin k_2 x] e^{-j\beta z}$$

$$H_{z3} = A_6 e^{k_3 x} e^{-j\beta z}$$

At $x=0$,

$$H_{z2} = H_{z3} \Rightarrow \boxed{A_3 = A_6}$$

and

$$E_{y2} = E_{y3}$$

$$E_{y2} = \frac{j\omega\mu}{k_2} \left[A_3 \sin k_2 x - A_4 \cos k_2 x \right] e^{-j\beta z}$$

$$E_{y3} = \frac{j\omega\mu}{k_3} A_6 e^{k_3 x} e^{-j\beta z}$$

$$\Rightarrow \frac{-A_4}{k_2} = \frac{A_6}{k_3}$$

At $x=d$,

$$H_{z1} = H_{z2}$$

$$A_1 e^{-k_1 d} = A_3 \cosh k_2 d + A_4 \sinh k_2 d$$

$$\& \quad E_{y1} = E_{y2}$$

① - ②,

$$k_1^2 + k_2^2 + \omega^2 \mu \epsilon_0 - \omega^2 \mu \epsilon_d = 0$$

$$\Rightarrow k_1 = \sqrt{\omega^2 \mu (\epsilon_d - \epsilon_0) - k_2^2}$$

k_1 is real,

$$\Rightarrow \omega^2 \mu (\epsilon_d - \epsilon_0) > k_2^2 \quad \text{—————} \textcircled{4}$$

From ② & ⑤,

$$k_3^2 + k_2^2 + \omega^2 \mu \epsilon_s - \omega^2 \mu \epsilon_d = 0$$

k_2 is real,

$$\Rightarrow \omega^2 \mu (\epsilon_d - \epsilon_s) > k_2^2 \quad \text{—————} \quad (5)$$

From (4),

$$\epsilon_d > \epsilon_0$$

From (5),

$$\epsilon_d > \epsilon_s$$

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