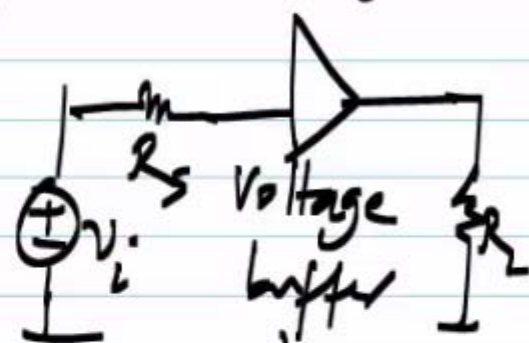
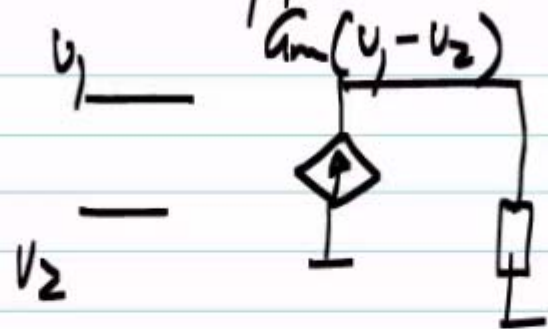
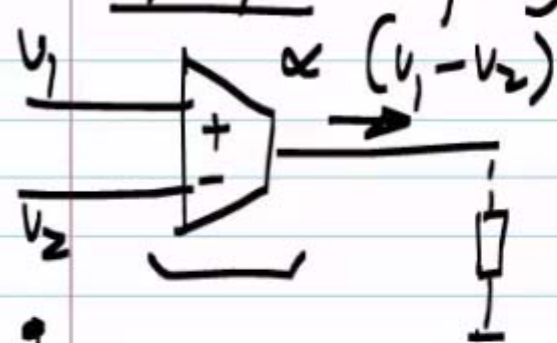
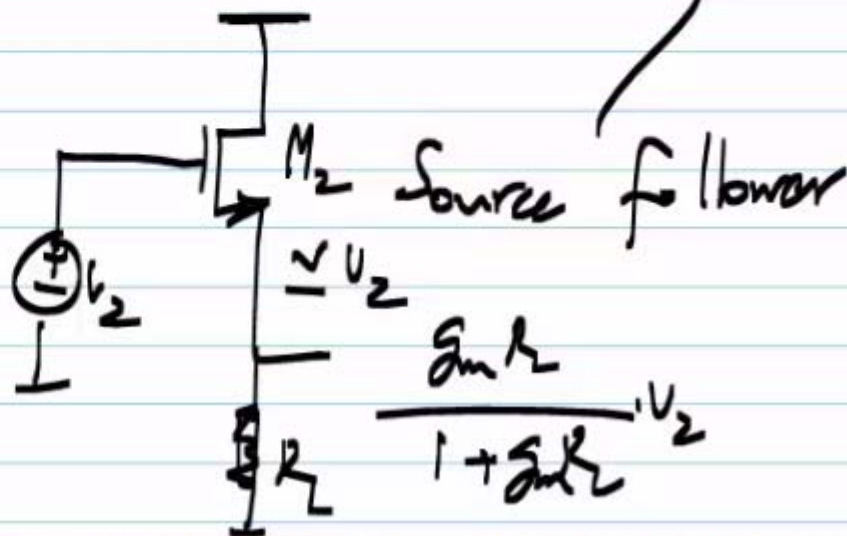
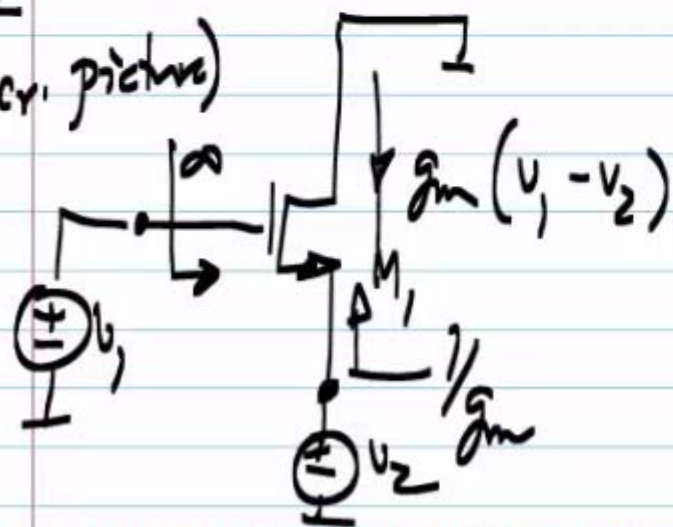


Source follower

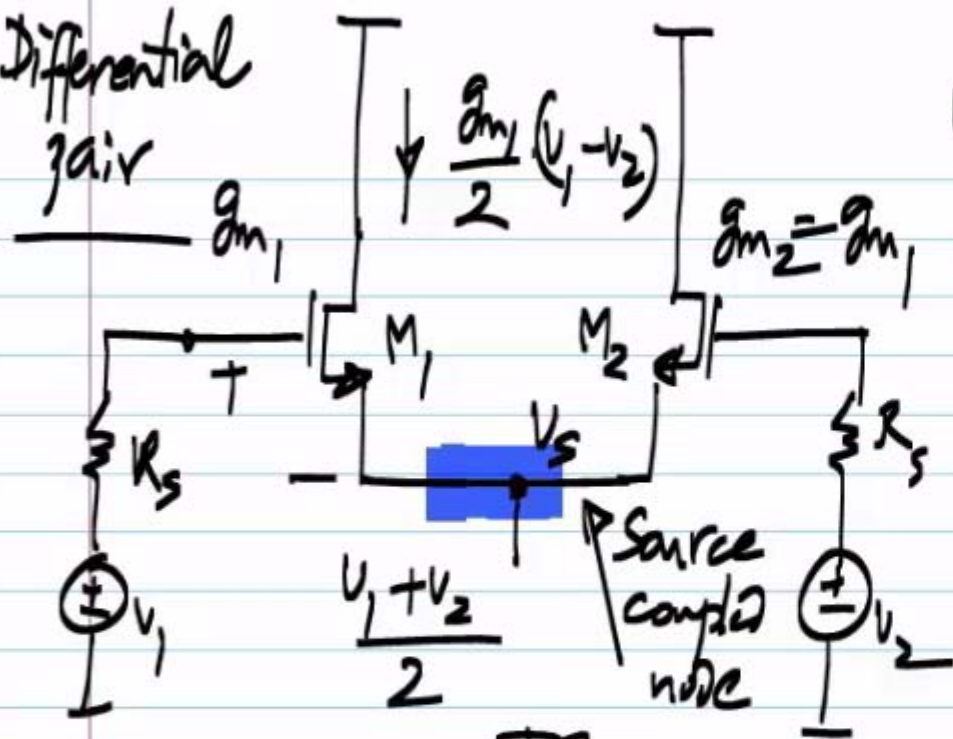
opamp: Amplify the difference of two voltages



(incr. picture)

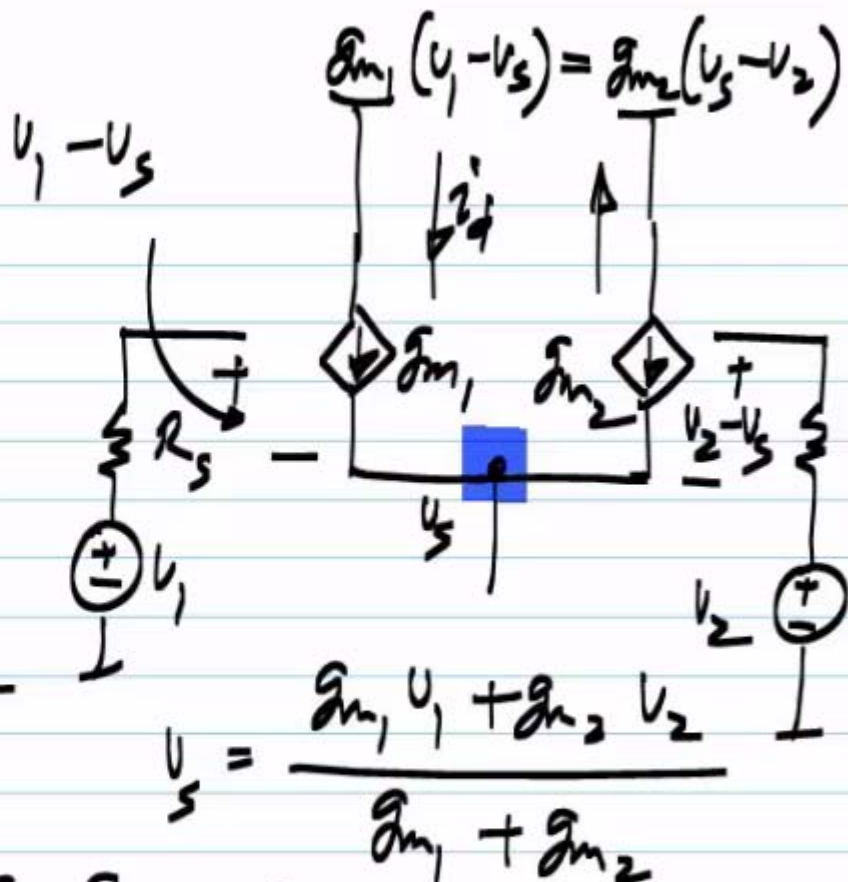


Differential pair



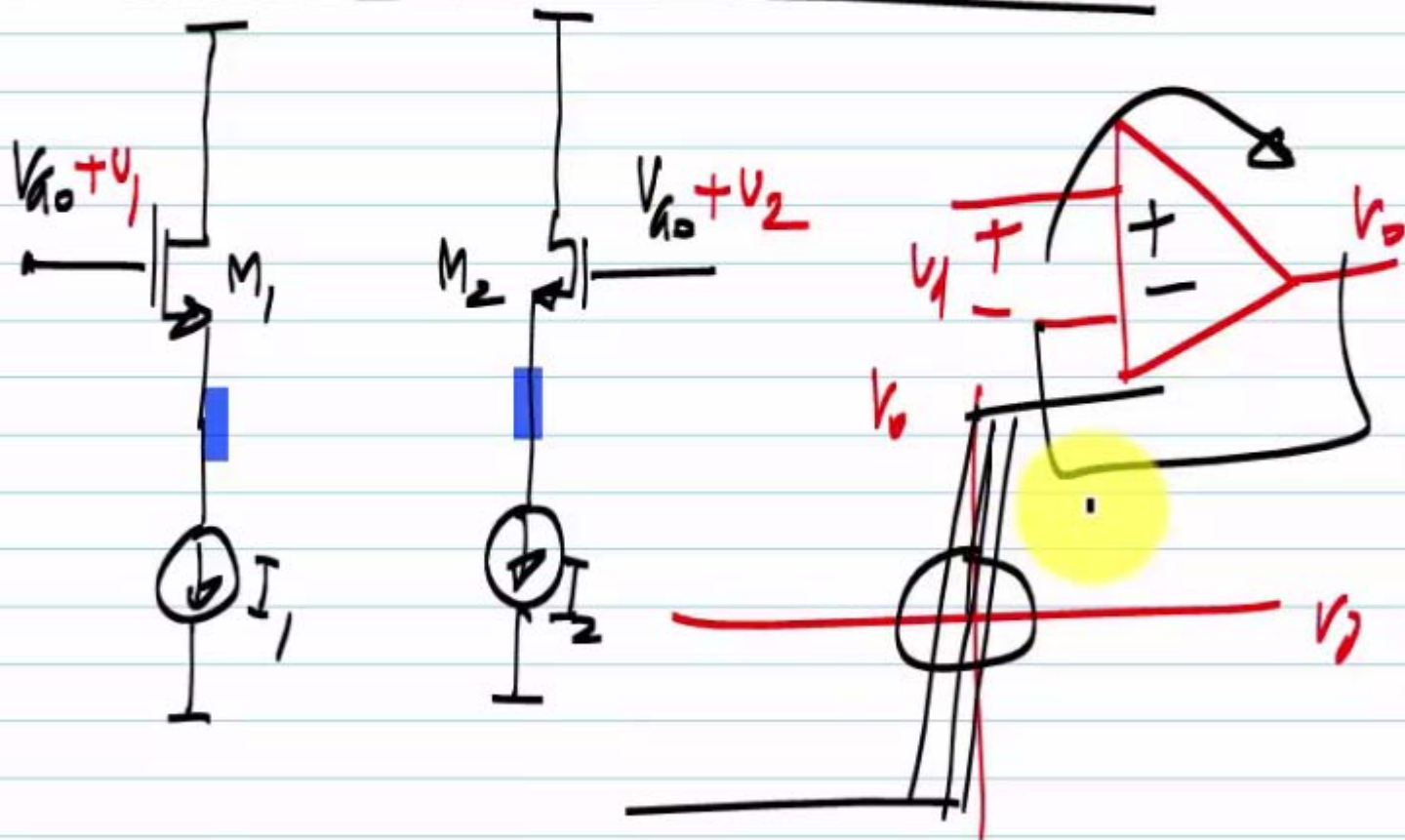
Thévenin node

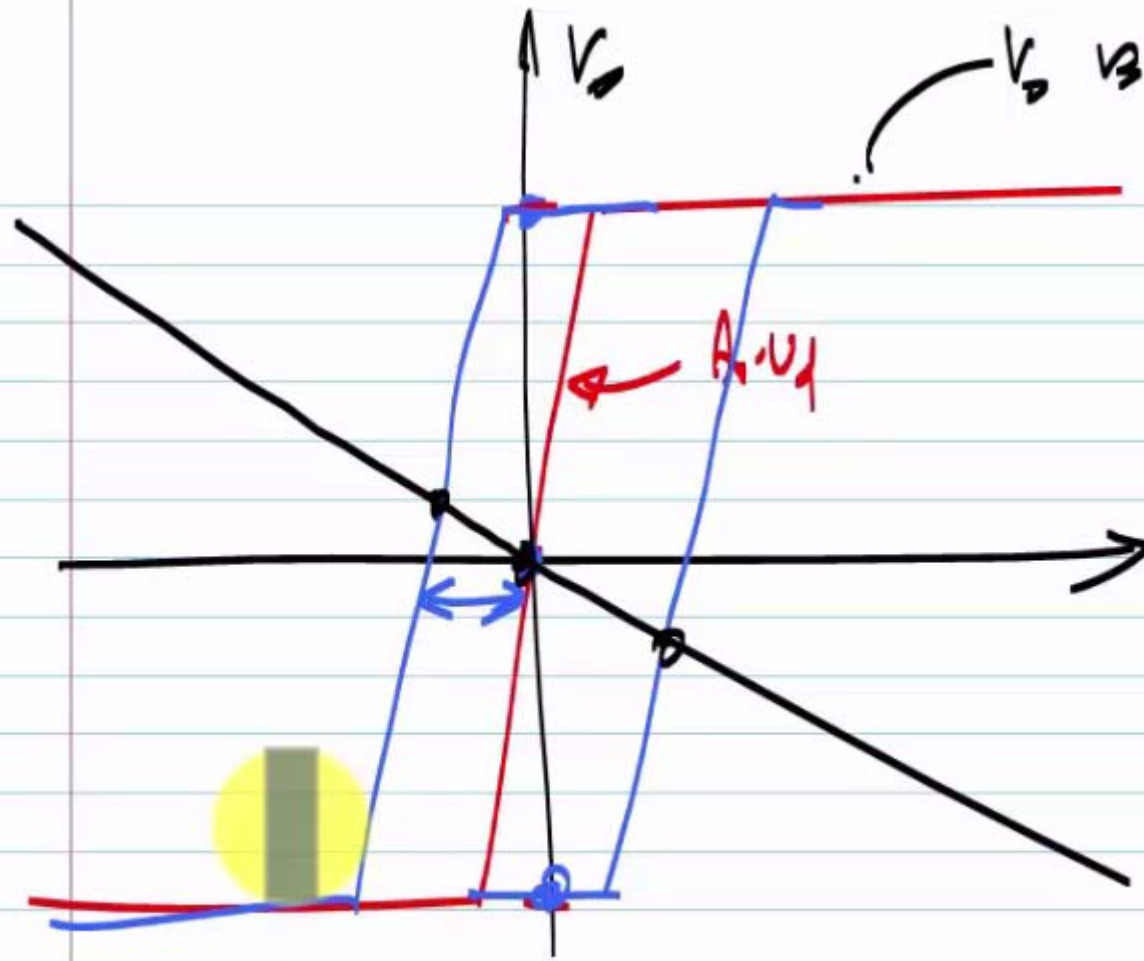
$$i_d = \left(\frac{g_{m1} g_{m2}}{g_{m1} + g_{m2}} \right) (v_1 - v_2)$$



$$v_s = \frac{g_{m1} v_1 + g_{m2} v_2}{g_{m1} + g_{m2}}$$

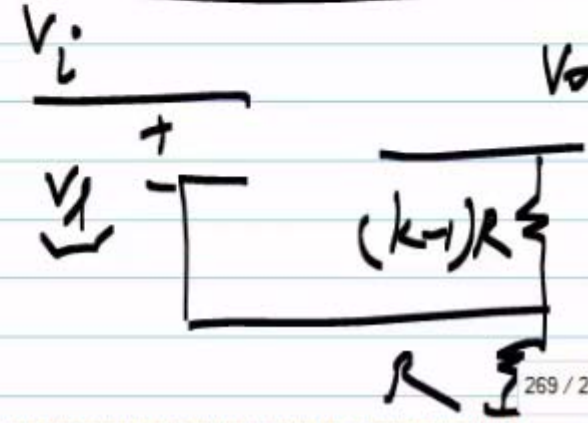
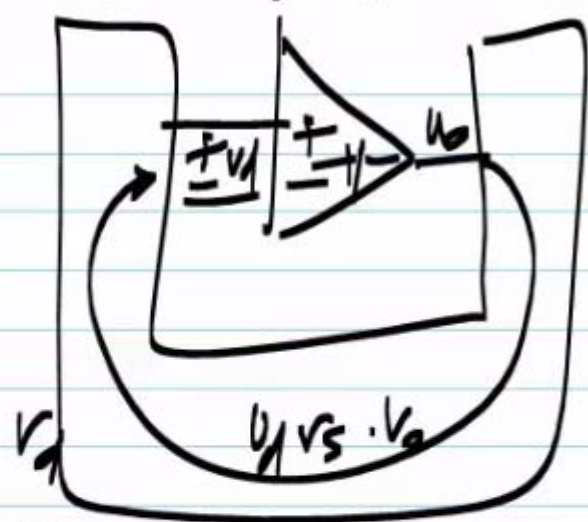
Source feedback biam : most suitable



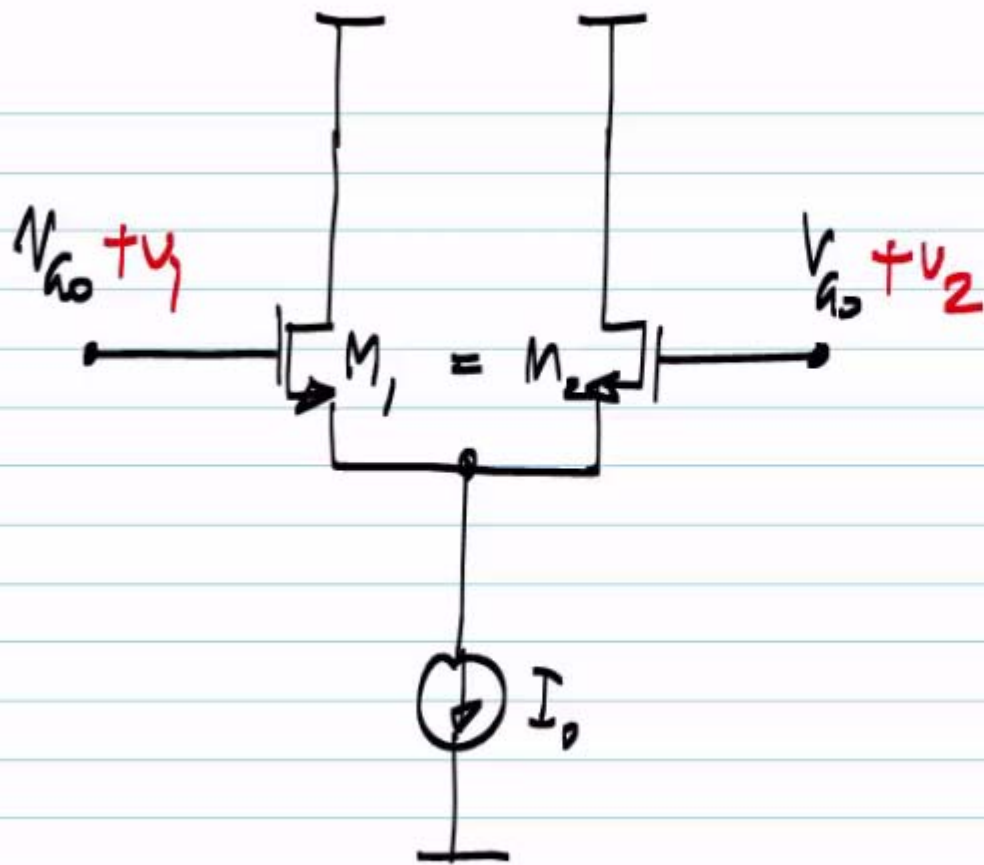


V_o is V_o of the opamp

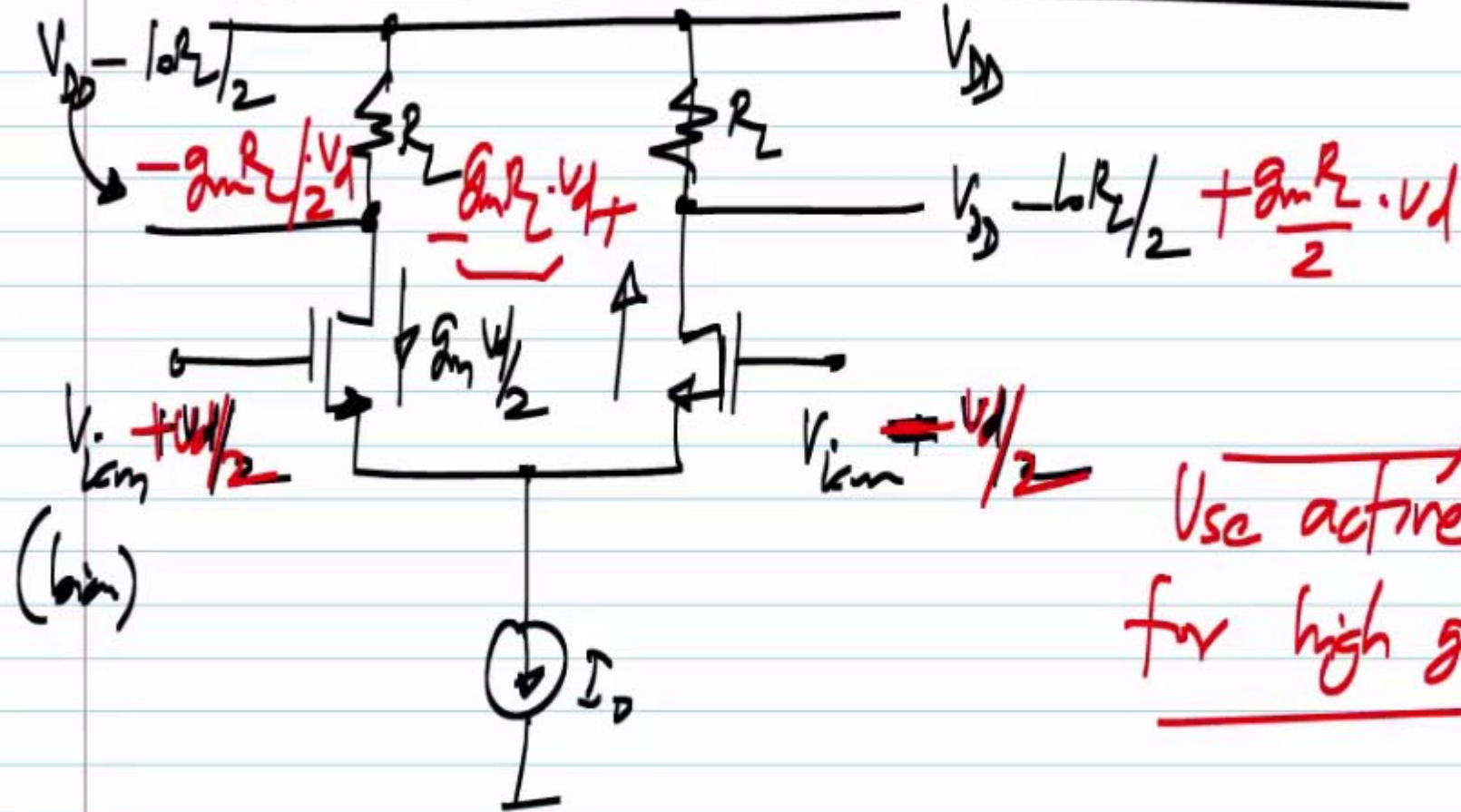
$A_v \cdot V_i$



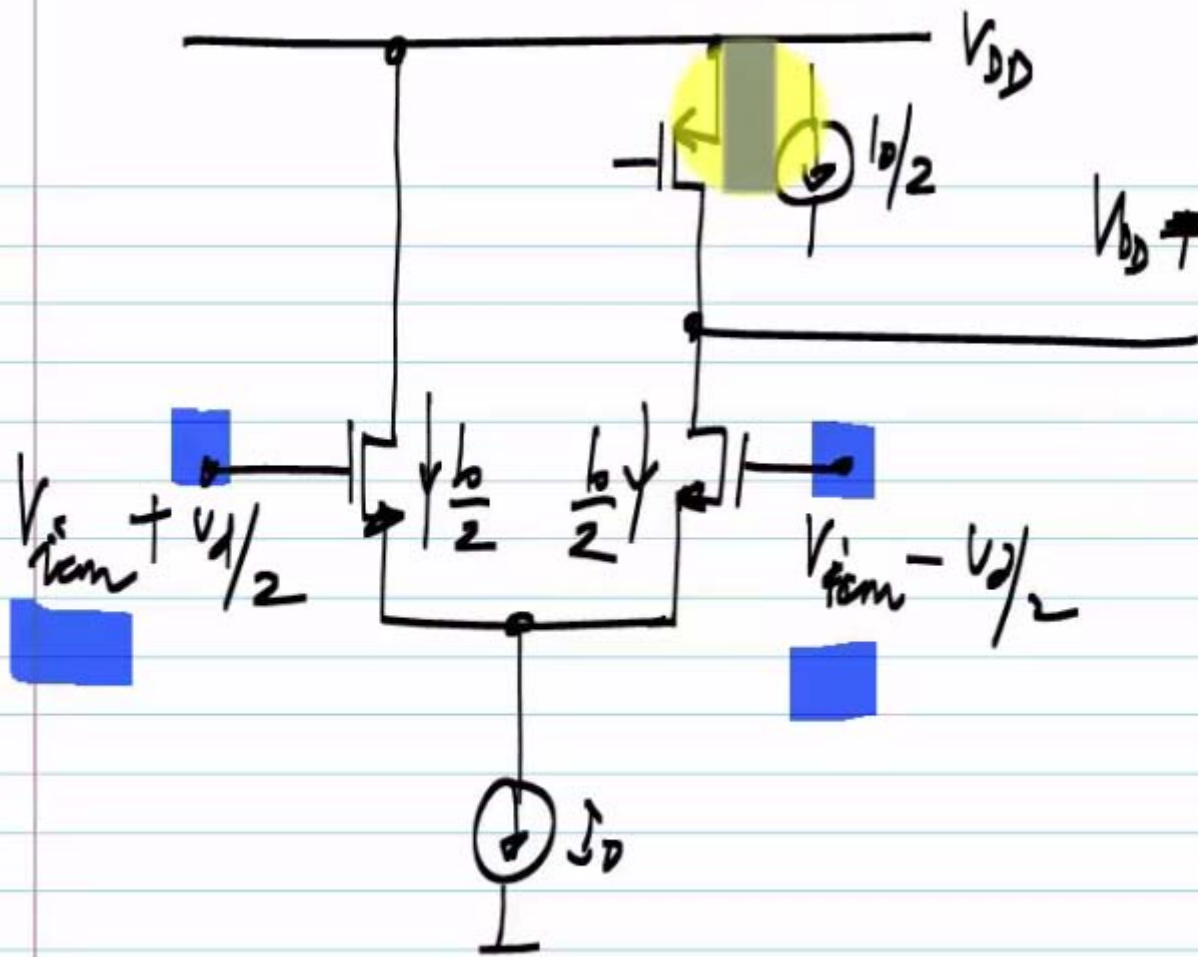
Differential pair
Source couple



Differential pair with differential excitation

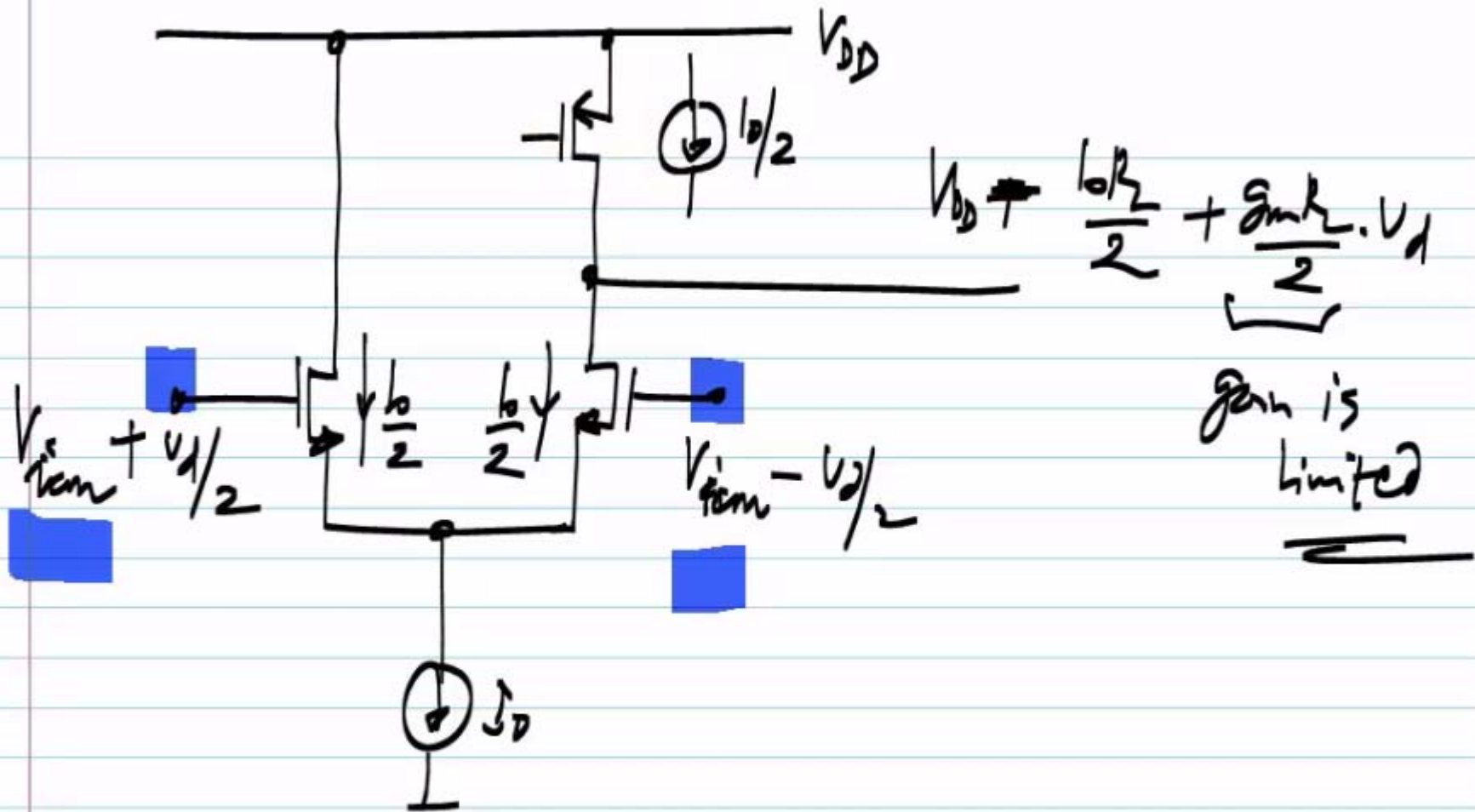


Use active load for high gain

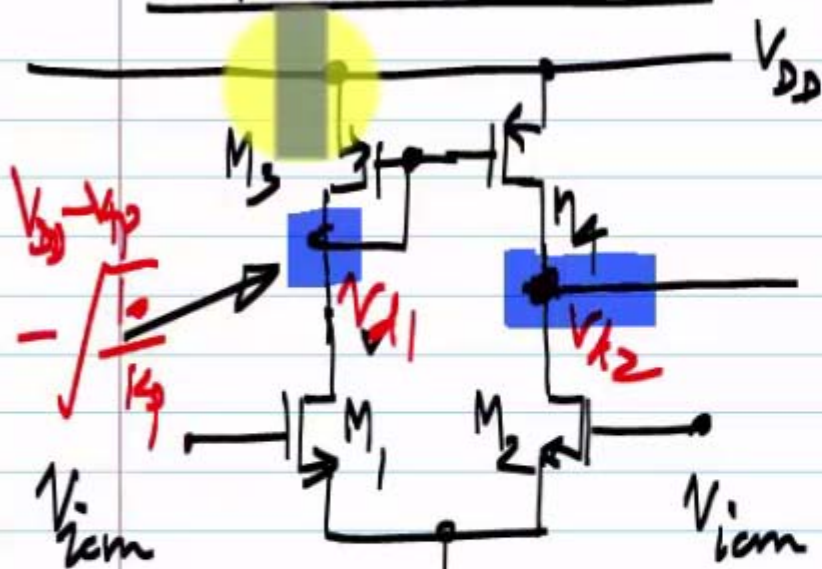


$$V_{od} = \frac{I_D R_L}{2} + \underbrace{g_{mL} \cdot v_d}_{\text{gain is limited}}$$

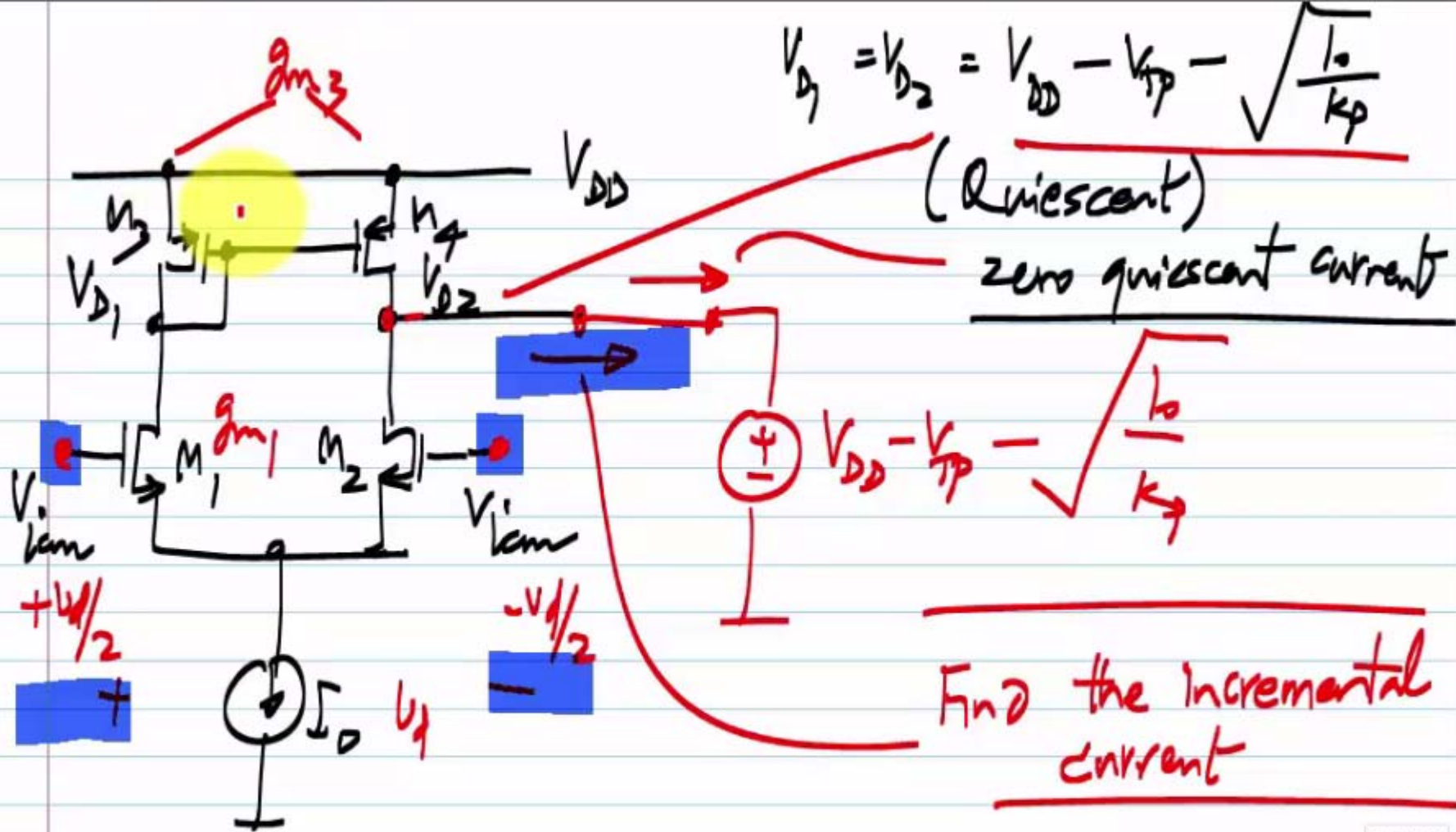
gain is limited

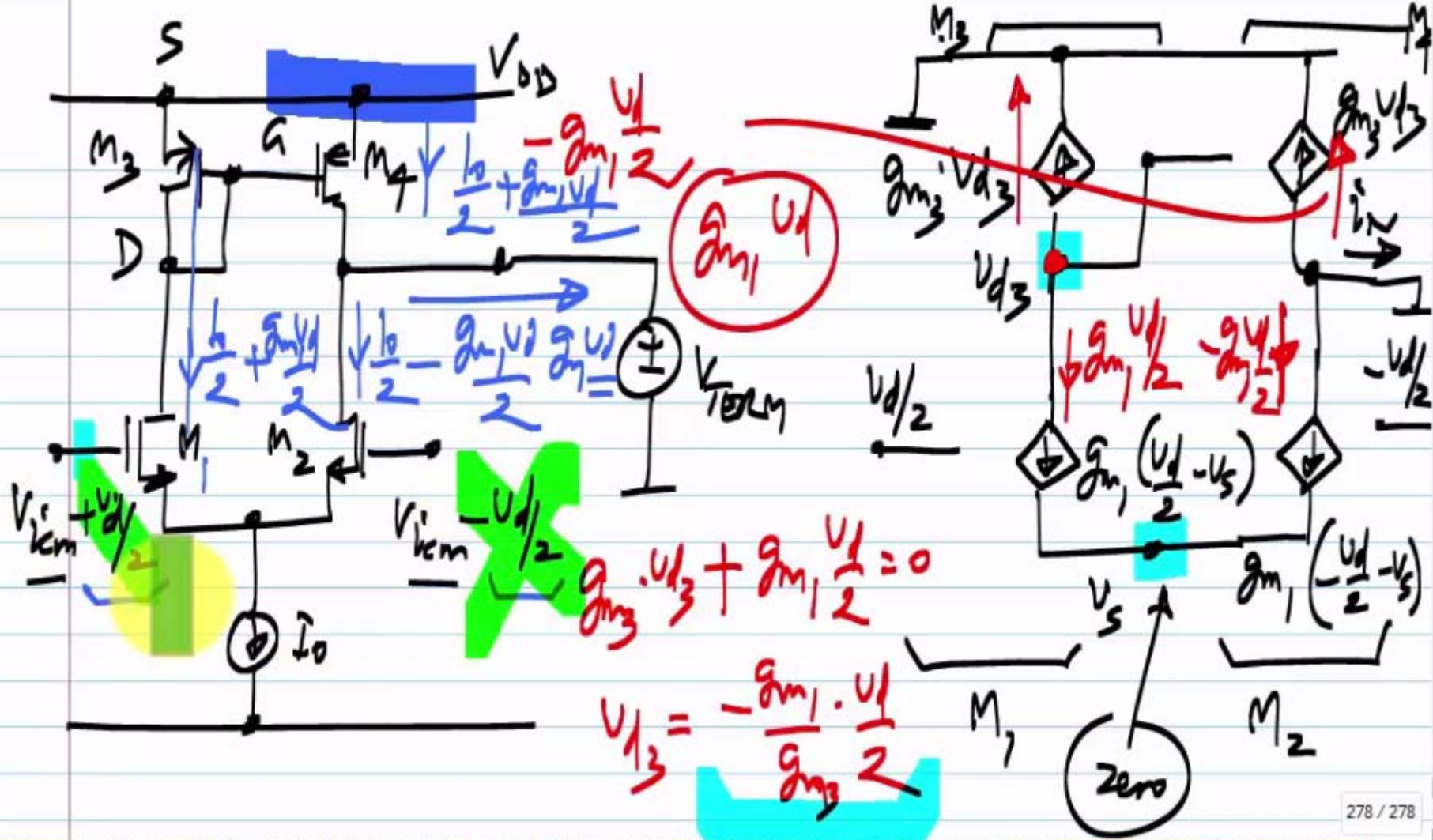


Differential pair with a current mirror load

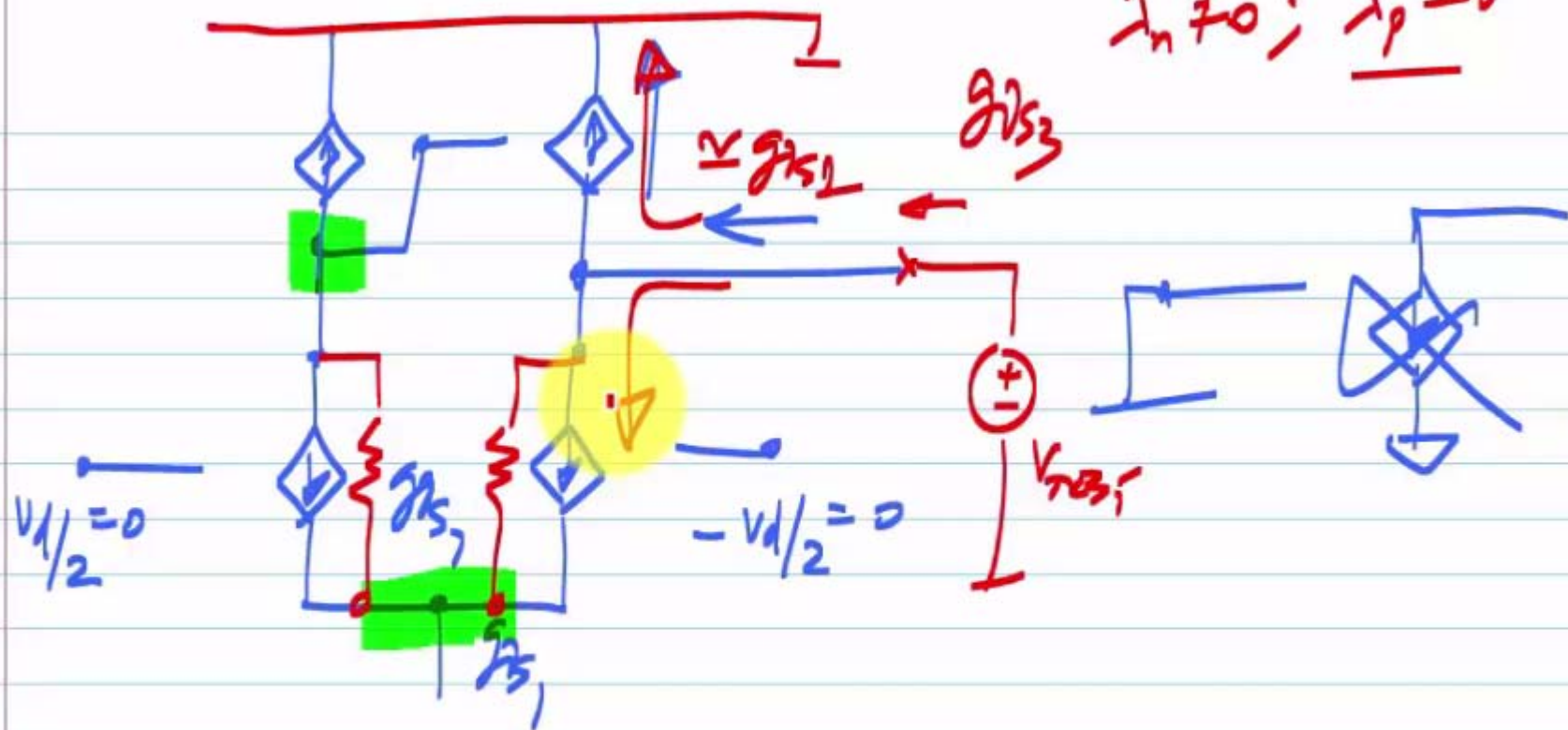


$$\begin{aligned}
 &V_{d1} > V_{d2} \\
 &V_{DS1} > V_{DS2} \Rightarrow I_{D1} > I_{D2} \\
 &V_{SD3} < V_{SD4} \Rightarrow I_{D3} < I_{D4}
 \end{aligned}$$

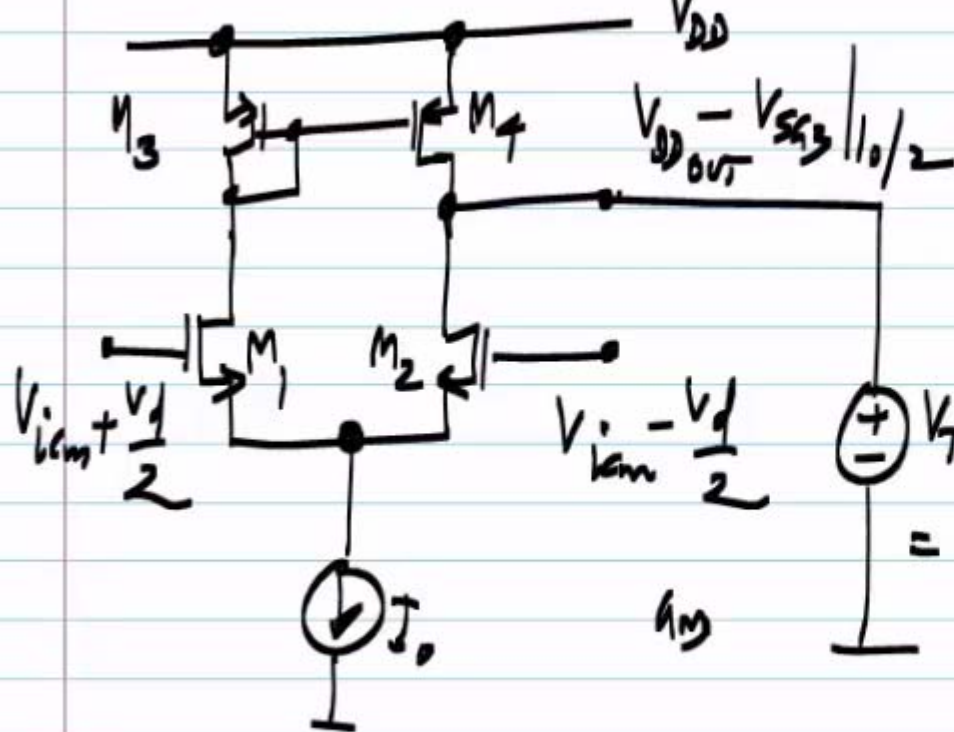




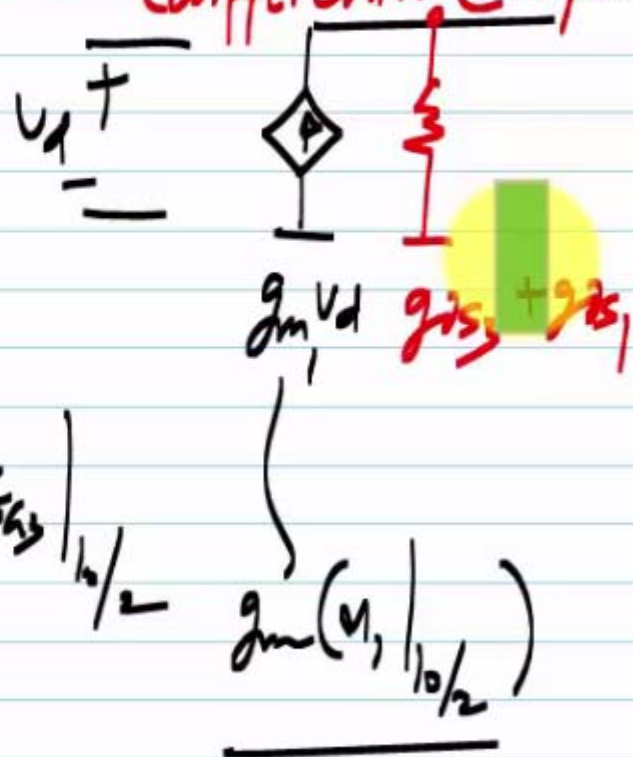
$$\lambda_n \neq 0; \lambda_p = 0$$

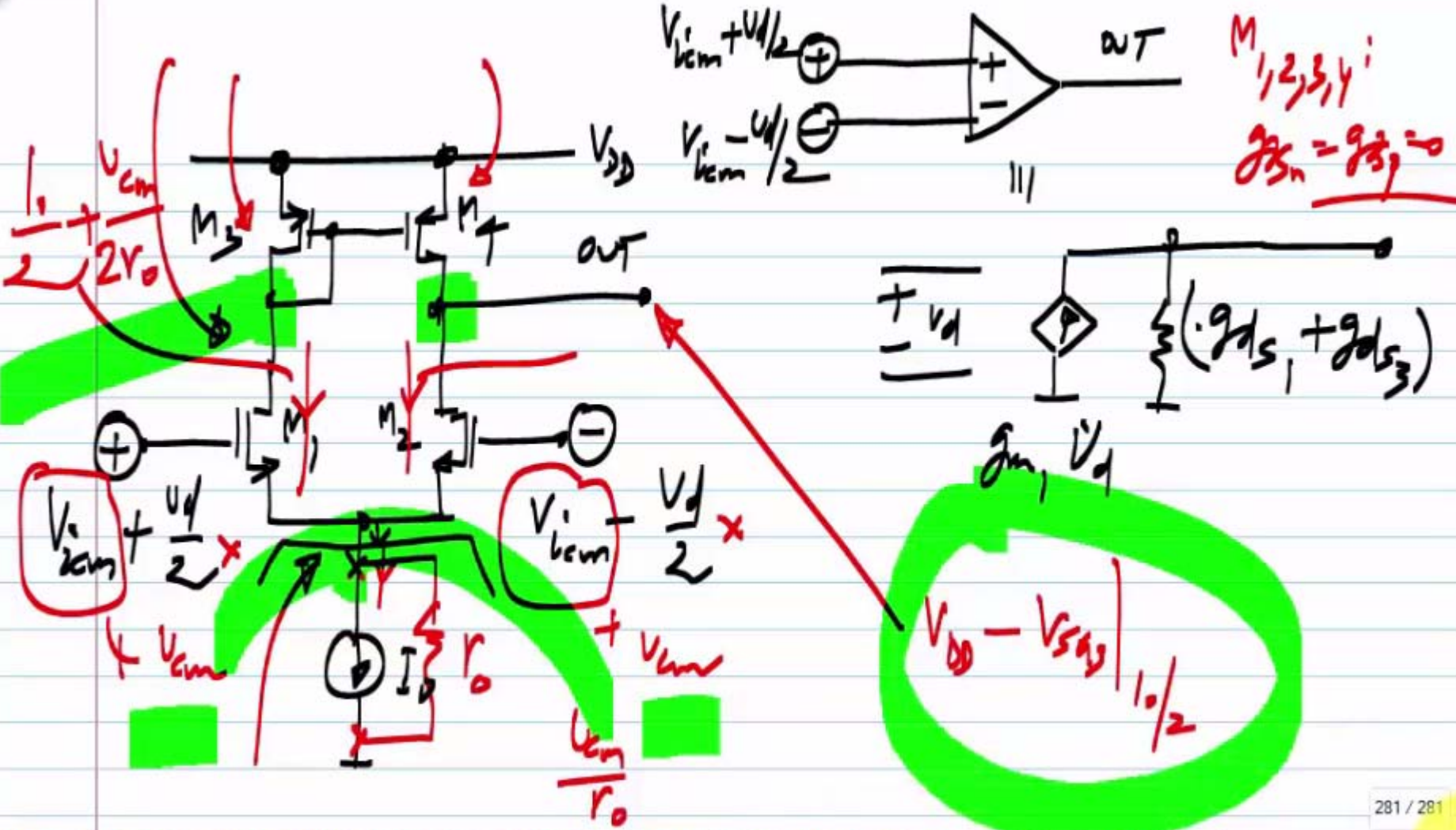


$$\lambda_n = 0; \lambda_p \neq 0$$

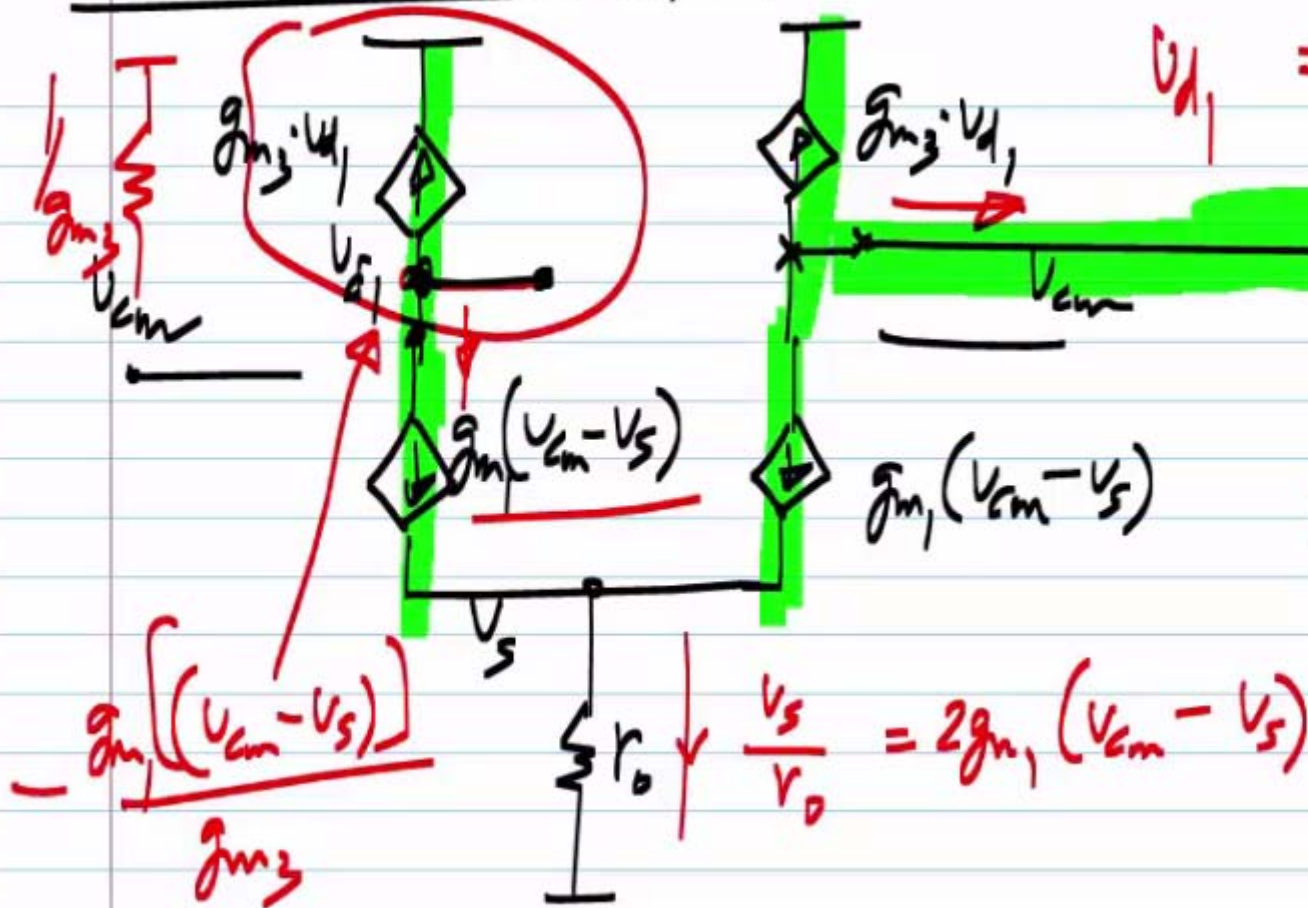


Small signal model of
a differential pair
(differential inputs)





Common mode input-



$$V_{d1} = - \frac{g_{m1}}{g_{m3} (2g_{m1} r_0 + 1)} \cdot V_{cm}$$

$$V_s = \frac{2g_{m1} r_0}{2g_{m1} r_0 + 1} \cdot V_{cm}$$

$$\frac{V_s}{r_0} = 2g_{m1} (V_{cm} - V_s)$$

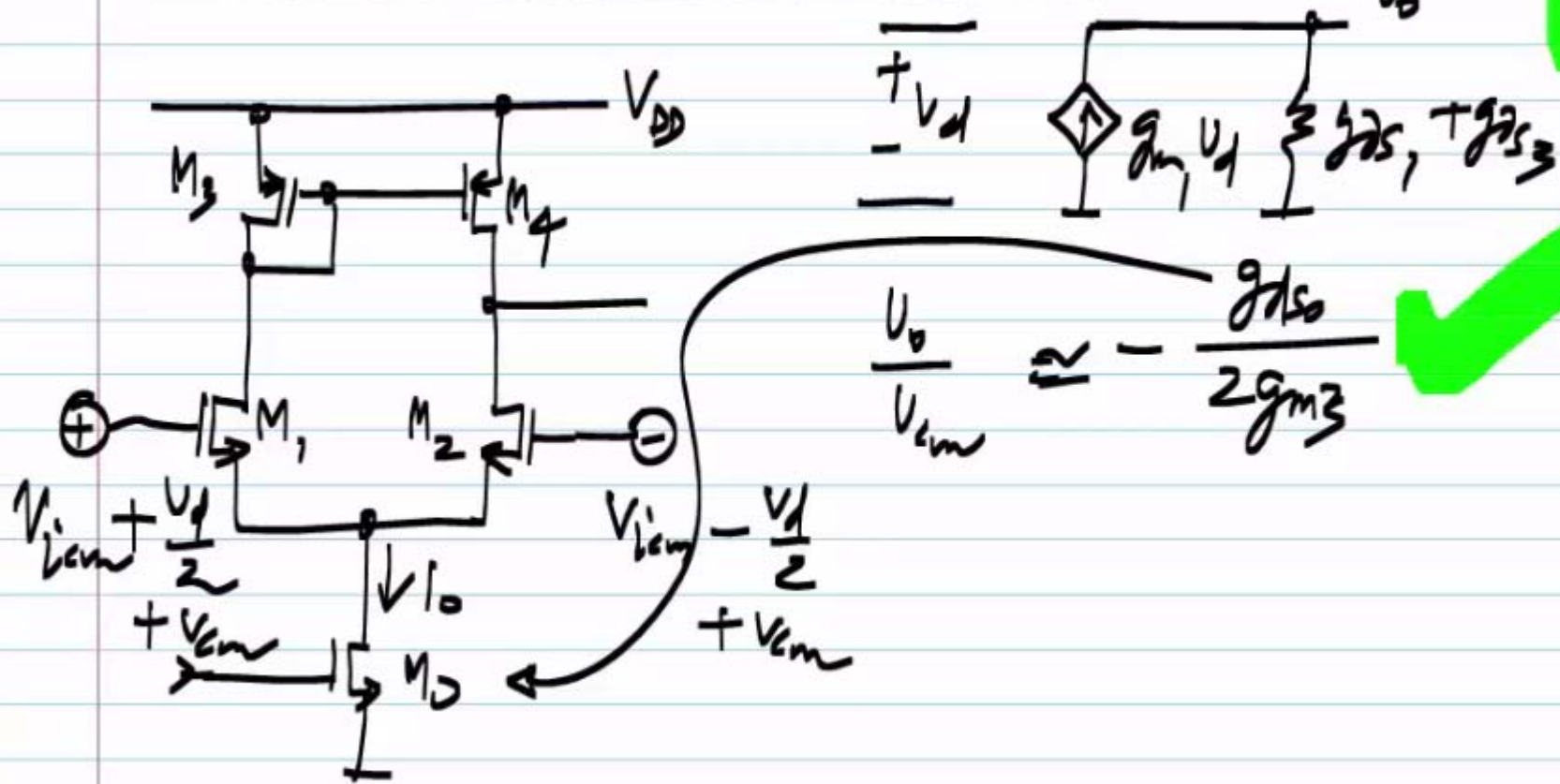
Voltage gain of a diff pair

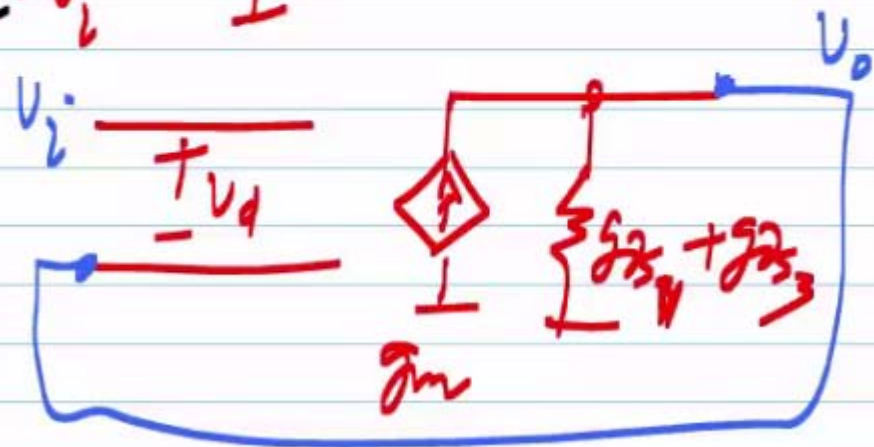
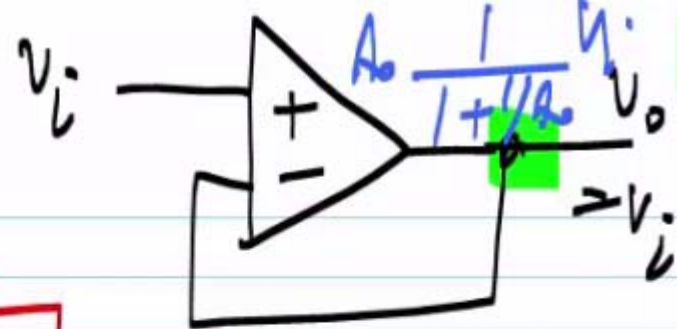
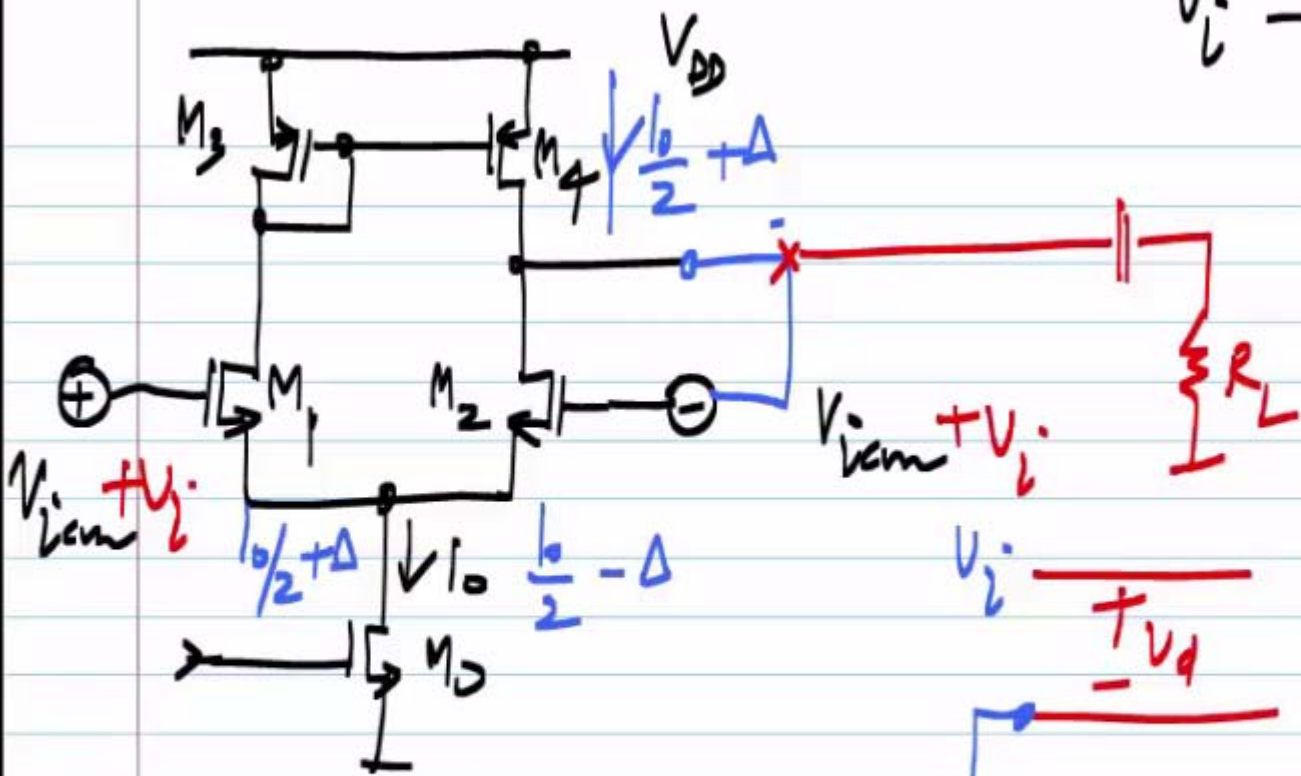
for differential signals $A_d = \frac{v_o}{v_d} = \left[\frac{g_{m1}}{g_{ds1} + g_{ds3}} \right]$

for CM signals $A_{cm} = \frac{v_o}{v_{cm}} = \left[\frac{g_{m1}}{g_{m3} (2g_{m1}r_o + 1)} \right]$

Common mode rejection ratio $CMRR = \left| \frac{A_d}{A_{cm}} \right| = \frac{2g_{m1}r_o + 1 \cdot (g_{m3})}{(g_{ds1} + g_{ds3})} = \frac{2g_{m3}r_o}{\gg 1}$

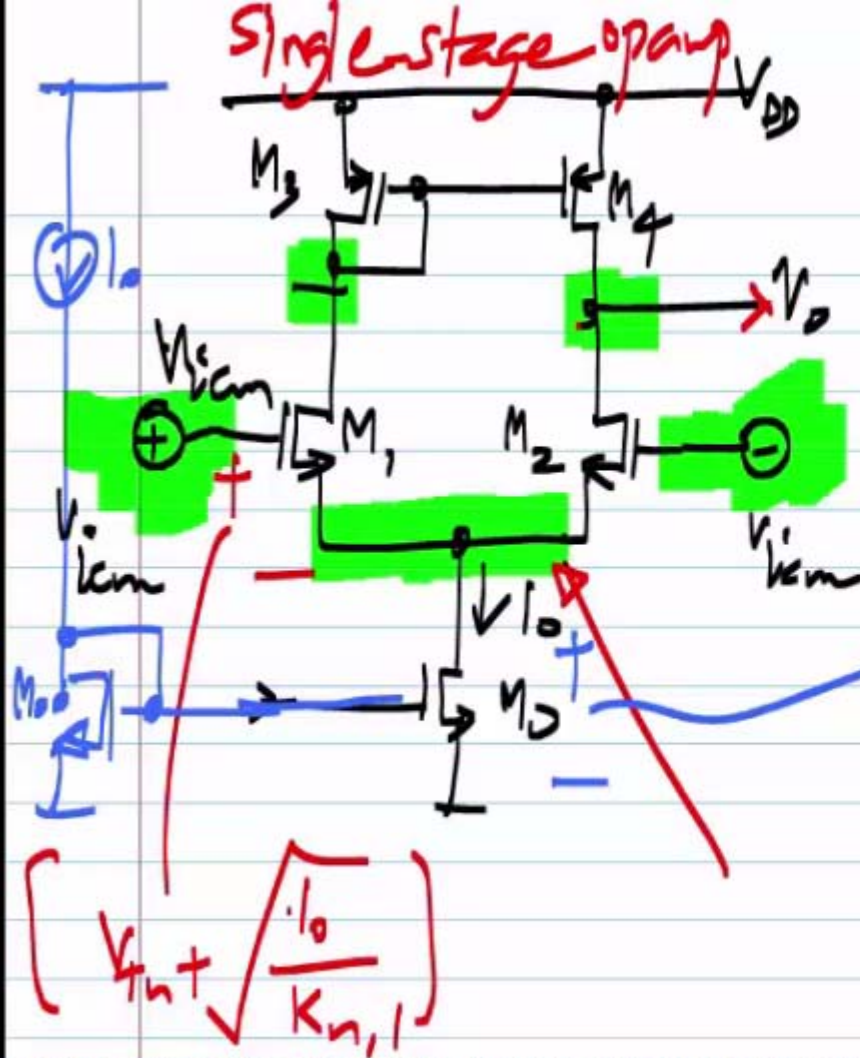
Diff. pair with current mirror load





Single stage opamp

$$K_{n,0} = \mu_n C_{ox} \frac{W_2}{L_0}$$



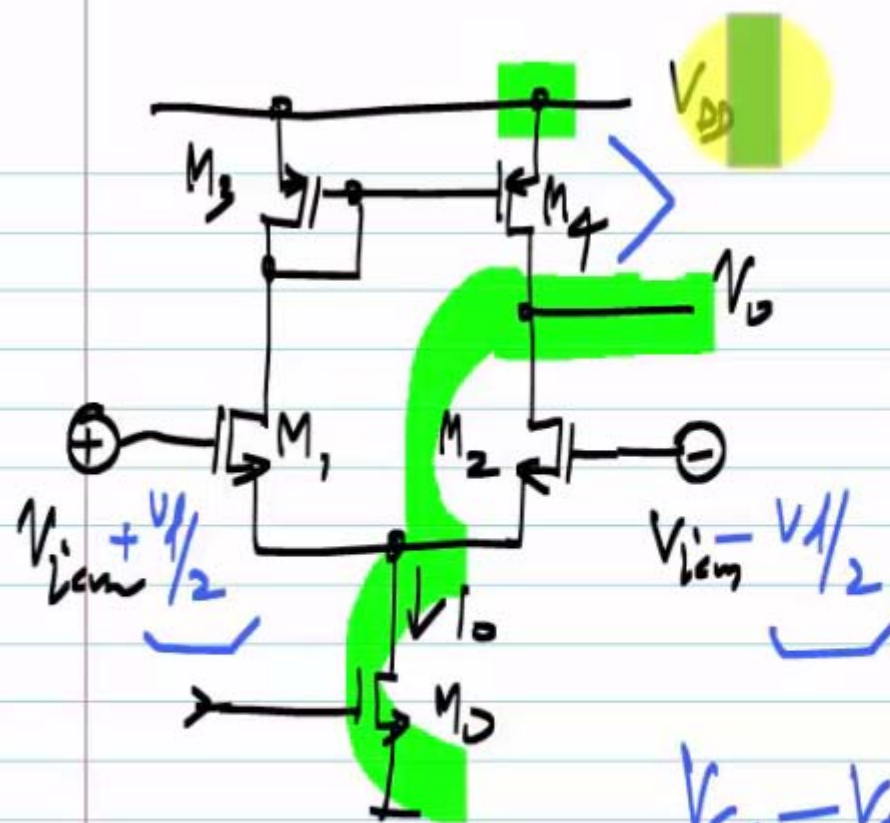
$$V_{DSAT0} + V_{GS1} < V_{icm} < V_{DD} - V_{SG3} + V_{TN}$$

$$V_{TN} + \sqrt{\frac{I_0}{K_{n,1}}}$$

$$V_{DD} - V_{TP} - \sqrt{\frac{I_0}{K_{p,3}}}$$

$$+ \sqrt{\frac{2I_0}{K_{n,0}}}$$

$$V_{icm} < V_{DD} - V_{SG3} + V_{TN}$$

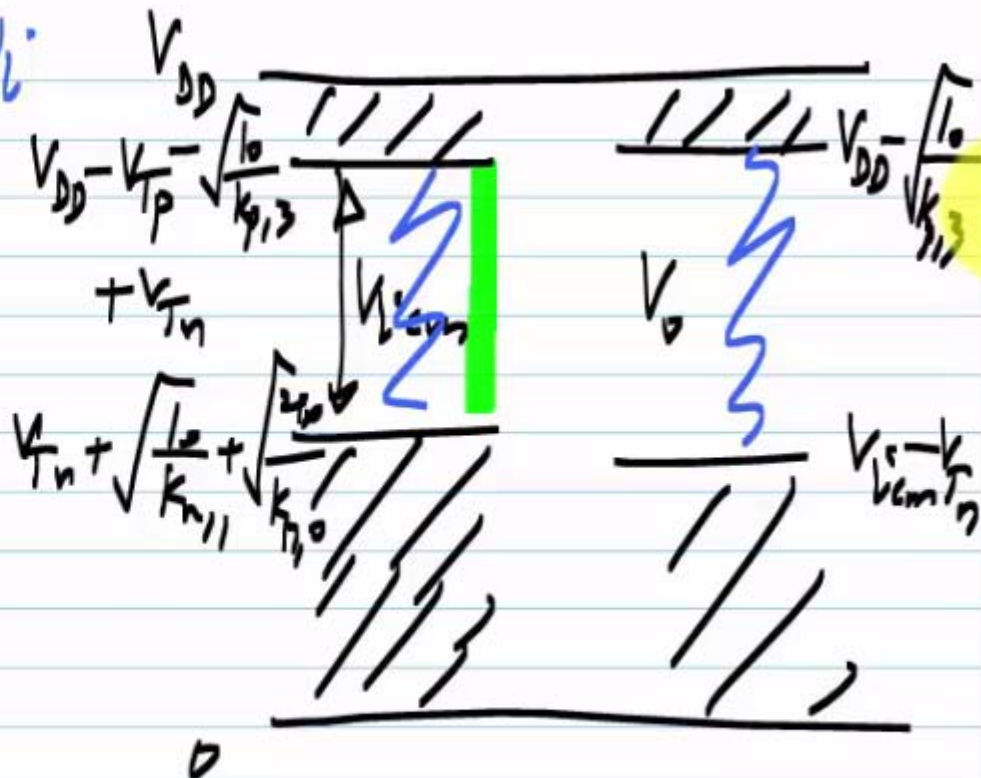
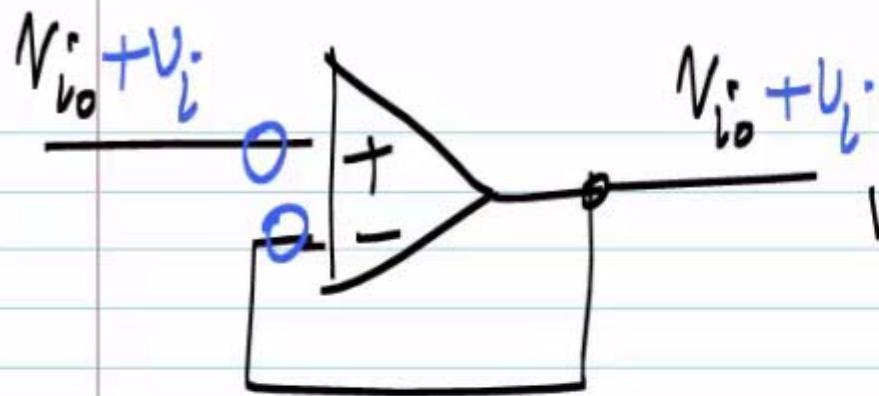


$$V_{DS} > V_{GS} - V_T$$

$$V_D > V_a - V_T$$

$$V_{bias} - V_{Tn} < v_D < V_{DD} - \sqrt{\frac{I_0}{k_{p,3}}}$$

$$V_{SG3} - V_{TP} = \sqrt{\frac{I_0}{k_{p,3}}}$$



$$V_{icm} = V_{io} + v_i$$

$$V_o = V_{io} + v_i$$