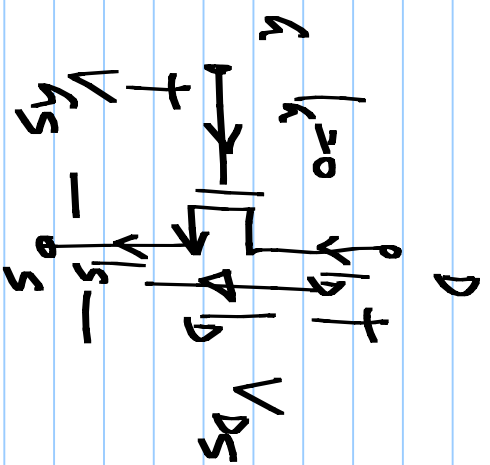
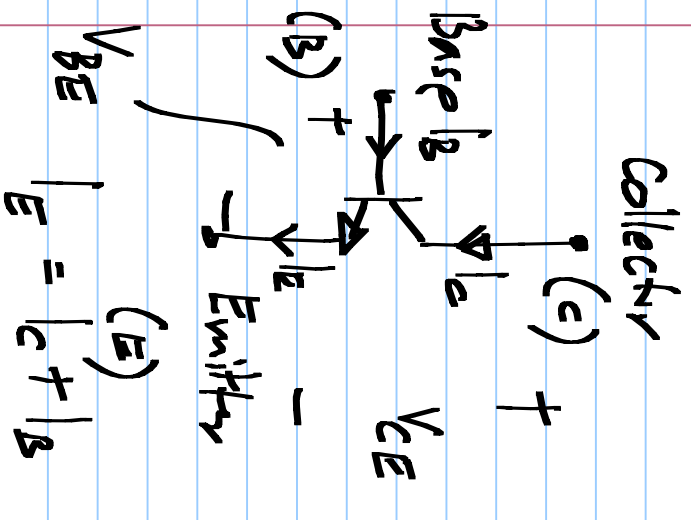


Bipolar junction transistor (BJT)

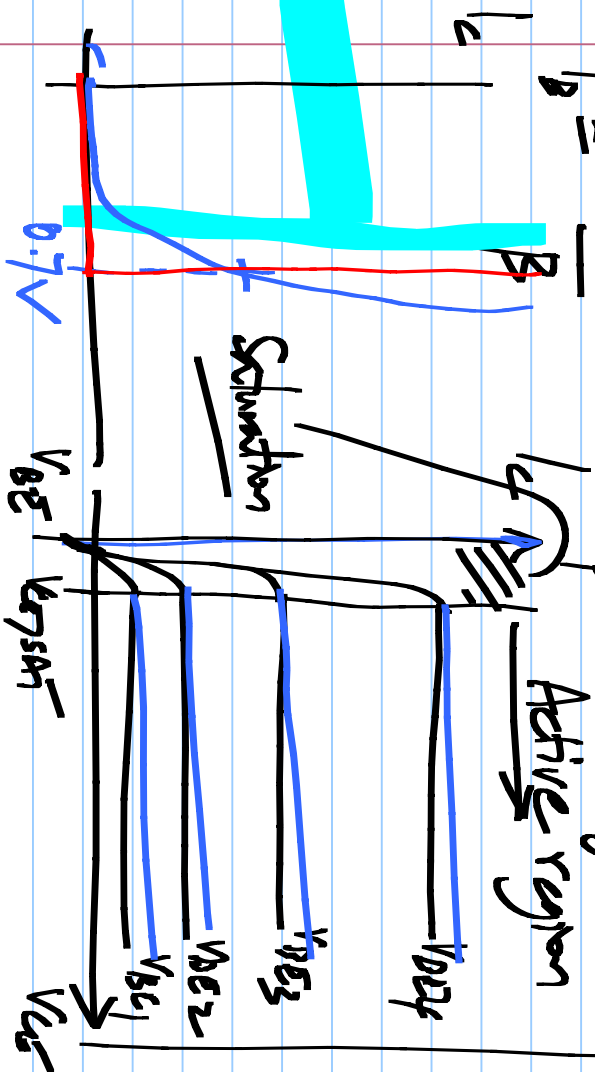


nMOS transistor

$$I_c \approx I_s \exp\left(\frac{V_{BE}}{V_T}\right) \left(1 + \frac{V_{CE}}{V_A}\right)$$

$V_{CE} > V_{CE,sat}$

$$I_B = \frac{I_c}{\beta}$$



$$I_D = \frac{\mu_n C_{ox}}{2} (V_{GS} - V_T)^2 (1 + \lambda_n V_{DS})$$

$V_{GS} > V_T$
 $V_{DS} > (V_{GS} - V_T)$

$$V_{BC} < 0 \quad I_C = I_S \exp\left(\frac{V_{BE}}{V_T}\right) \left(1 + \frac{V_{CE}}{V_A}\right) \quad \left| \quad V_{CE} > V_{CE,sat} \right.$$

$$V_{CE,sat} = V_{BE} = 0.7V$$

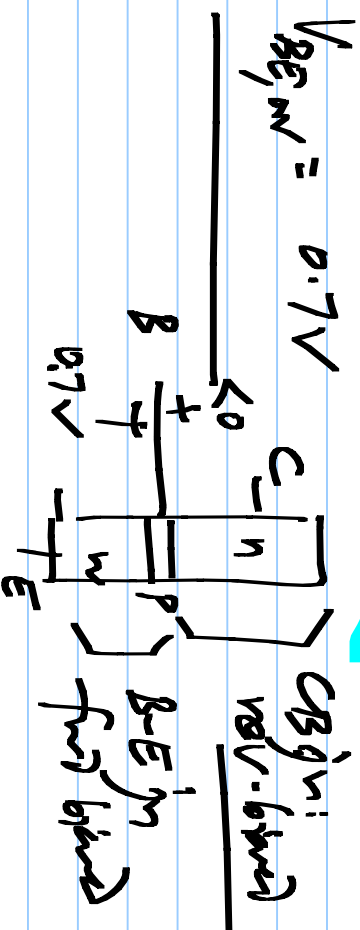
$$I_B = \frac{I_C}{\beta}$$

$$V_{CE} > 0.7V$$

$$V_{BE} = 0.7V$$

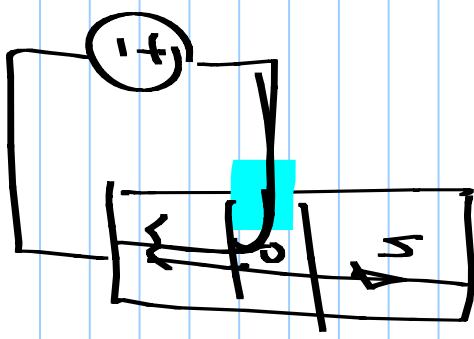
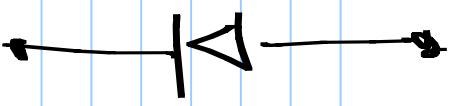
$$V_{CE} = V_{CE} + I_B$$

of Point calculation:

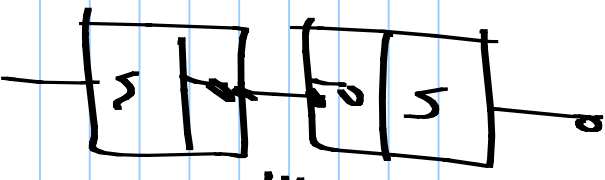




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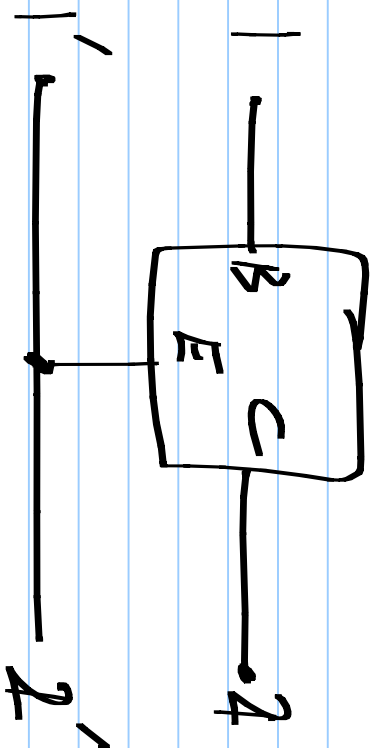
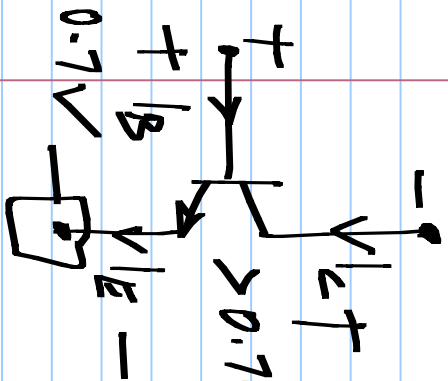
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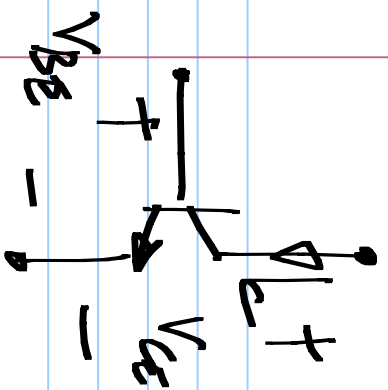


$$I_C = I_S \exp\left(\frac{V_{BE}}{V_T}\right) \left(1 + \frac{V_{CE}}{V_A}\right)$$

$$I_B = \frac{I_C}{\beta}$$

$$y_{11}, y_{12}, y_{21}, y_{22}$$





$$I_C = I_S \exp\left(\frac{V_{BE}}{V_T}\right) \left(1 + \frac{V_{CE}}{V_A}\right)$$

$$\frac{\partial I_C}{\partial V_{BE}} = \frac{I_S \exp\left(\frac{V_{BE}}{V_T}\right)}{V_T} \cdot \underbrace{\frac{kT}{q}}_{\text{Thermal voltage}} \cdot \underbrace{\left(1 + \frac{V_{CE}}{V_A}\right)}_{\text{Early voltage}}$$

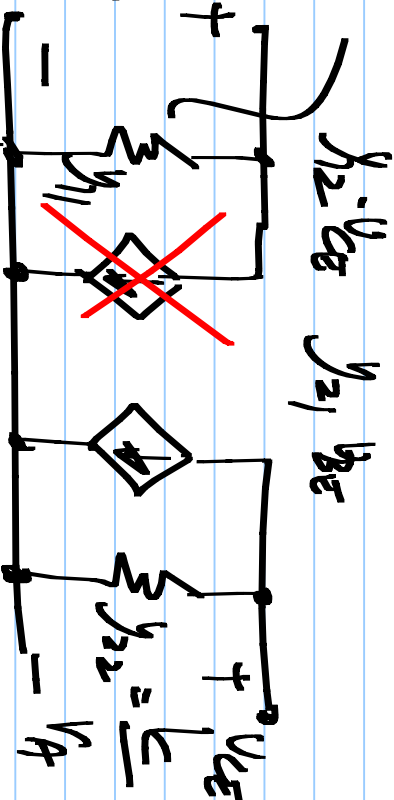
$$\frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{V_T} \cdot \underbrace{\frac{\partial I_C}{\partial V_{CE}} = I_S \exp\left(\frac{V_{BE}}{V_T}\right) \cdot \frac{1}{V_A}}_{\frac{I_C}{V_A}}$$

$$\frac{\partial I_B}{\partial V_{BE}} = \frac{1}{\beta} \frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{\beta V_T} \quad ; \quad \frac{\partial I_B}{\partial V_{CE}} = \frac{\partial I_C}{\partial V_{CE}} = \frac{I_C}{\beta V_A}$$

$$r_\pi = \frac{\beta V_T}{I_C}$$

$$g_m = y_{21} = \frac{I_C}{V_T}$$

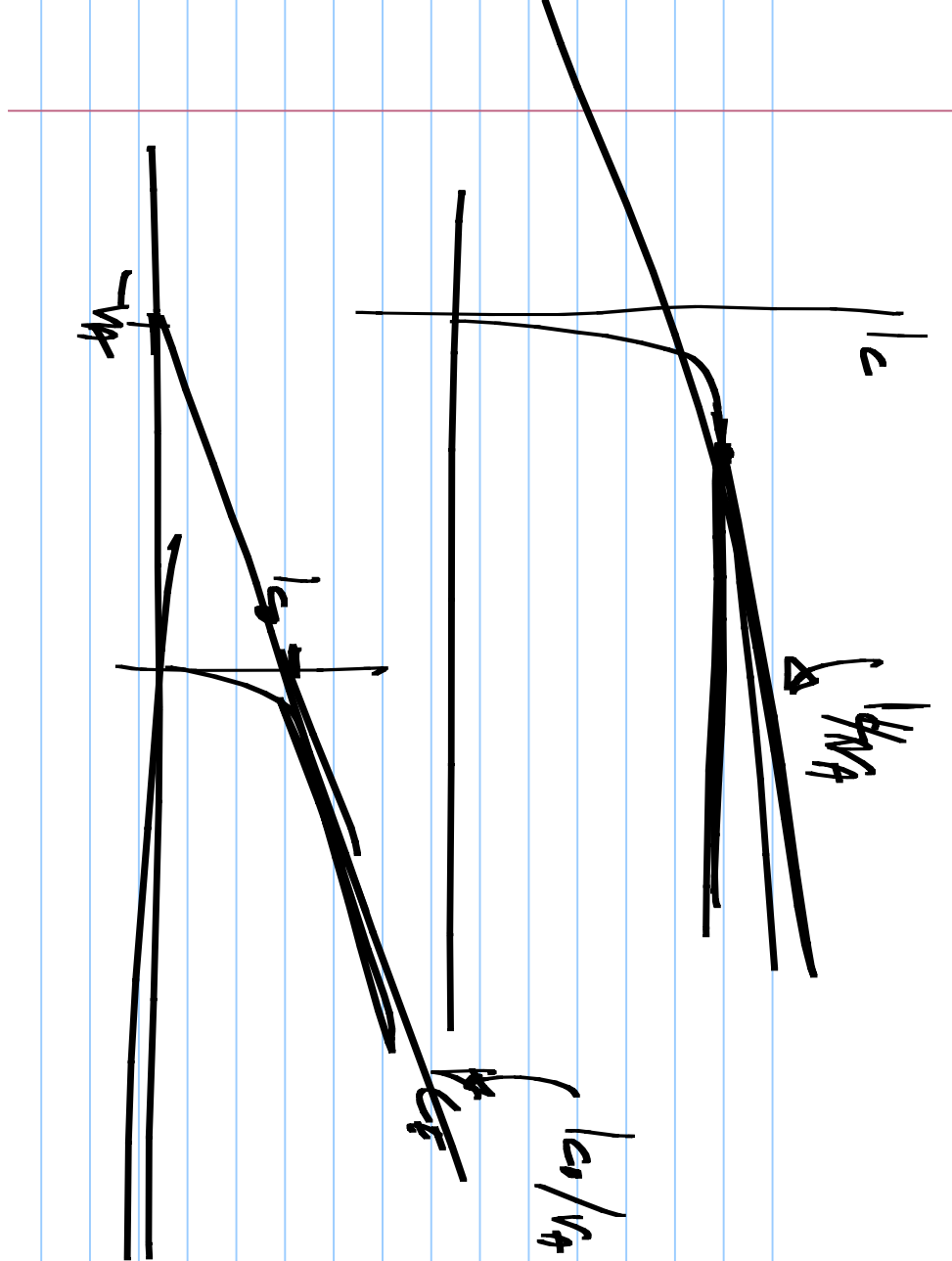
$$= 1/y_1 \quad V_{BE}$$

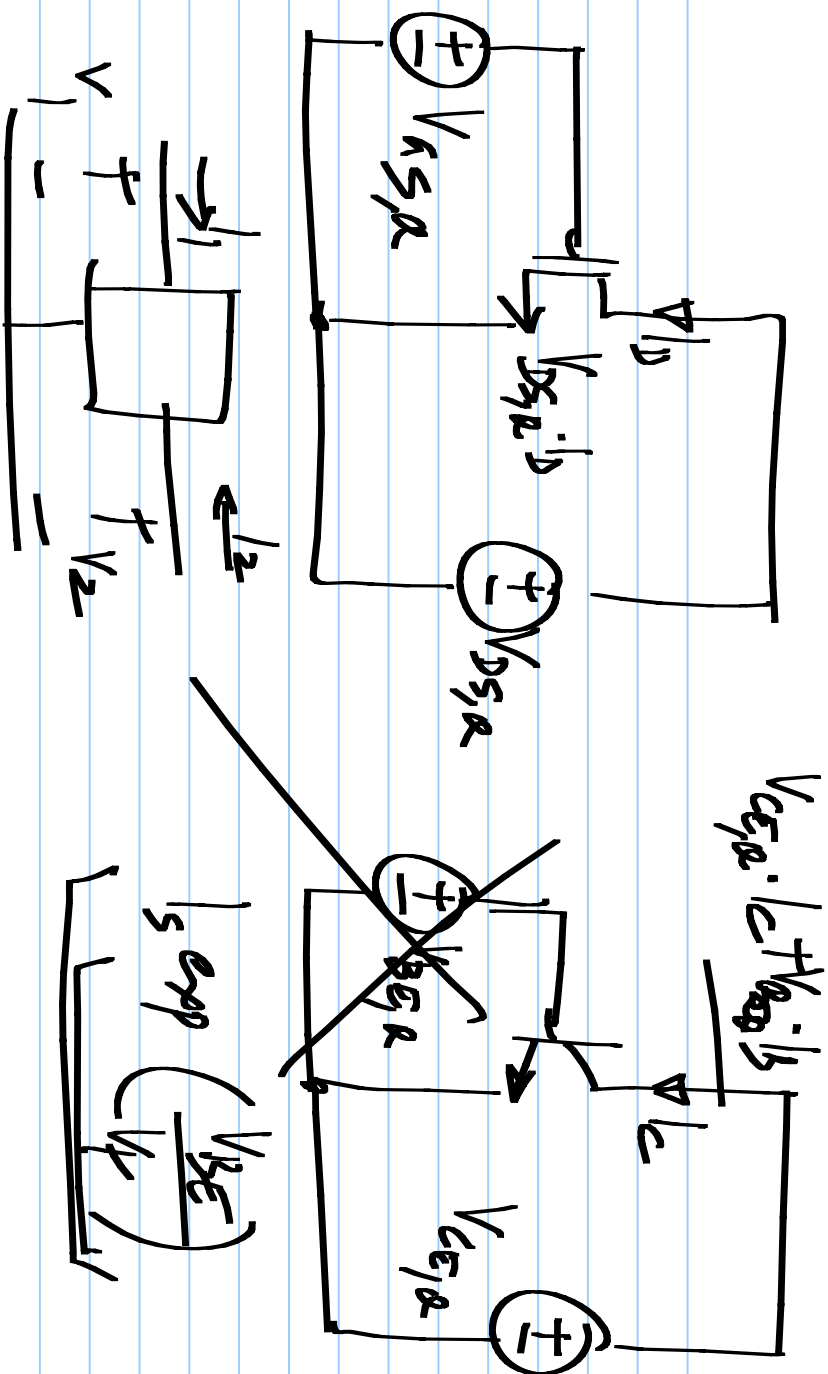


$$r_o = \frac{1}{y_{22}} = \frac{V_A}{I_C}$$

$$y_2 = \frac{I_C}{\beta V_A}$$

$$y_1 = \frac{I_C}{\beta V_T} \quad y_2 = \frac{I_C}{\beta V_T}$$





Const. current biasing:

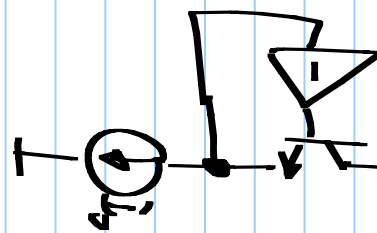
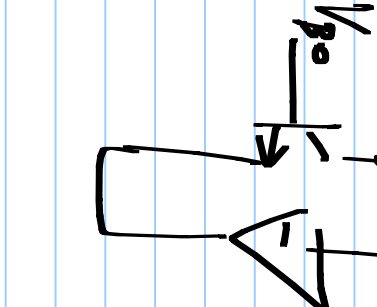
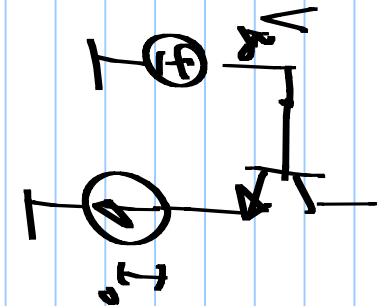
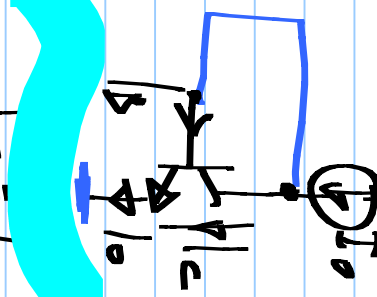
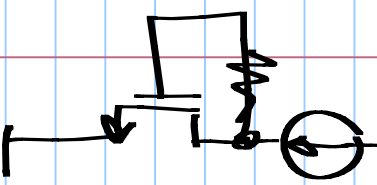
Sense collector emitter

collector emitter
emitter base

fb.

base

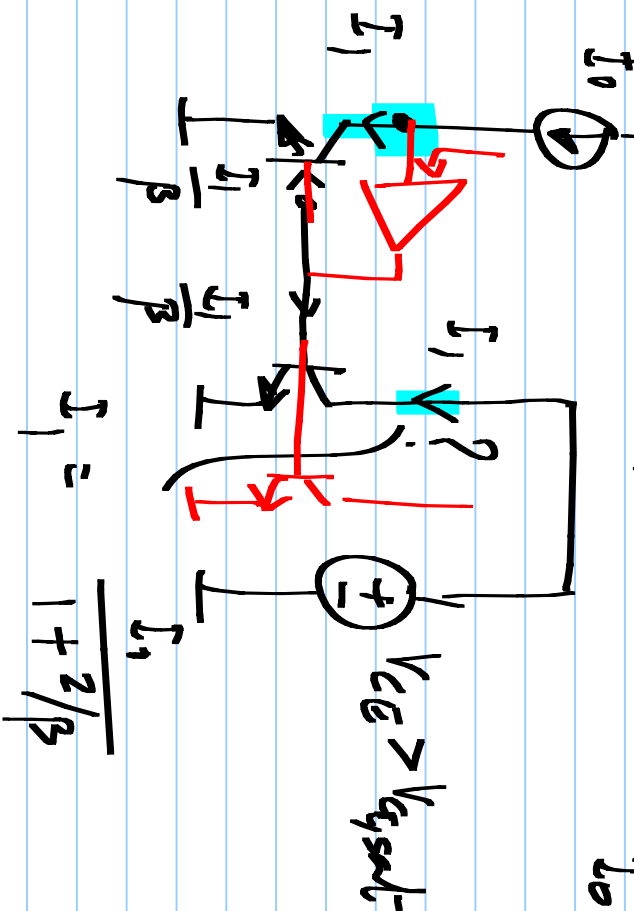
emitter



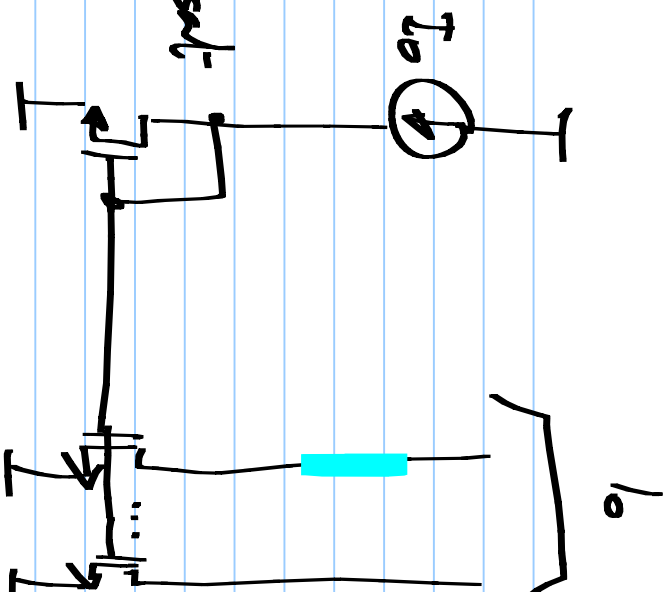
$$I_c = \left(\frac{\beta}{1+\beta} \right) I_o = \alpha I_o$$

Collector feedback bjt :

$$I_o = I_1 + \frac{2I_1}{\beta}$$

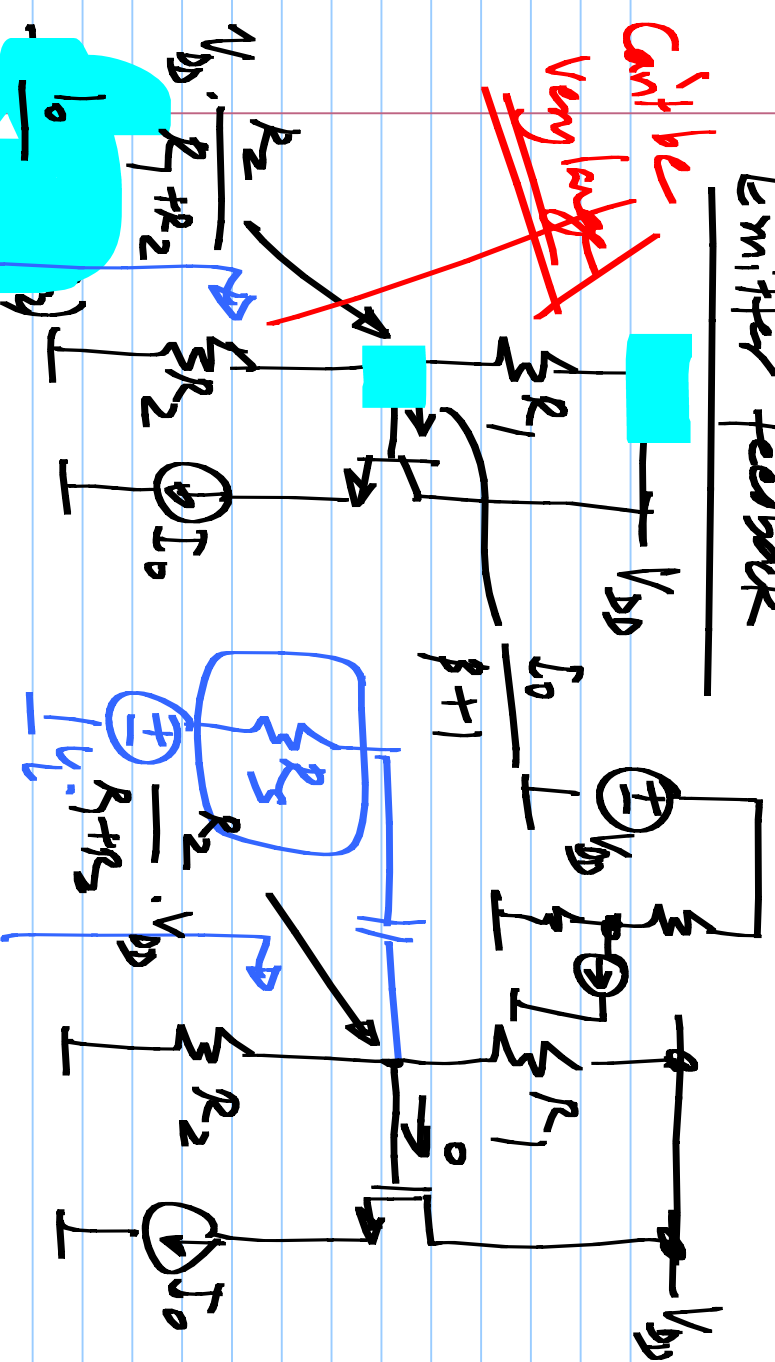


$$I_1 = \frac{I_o}{1 + 2/\beta}$$



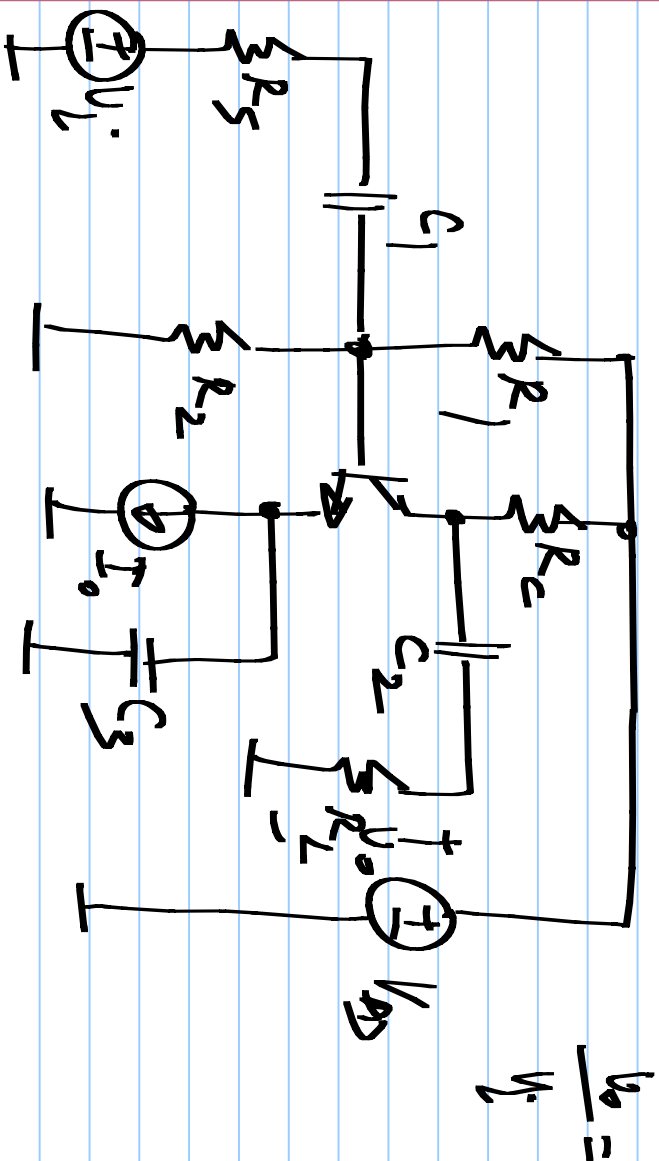
Emitter feedback

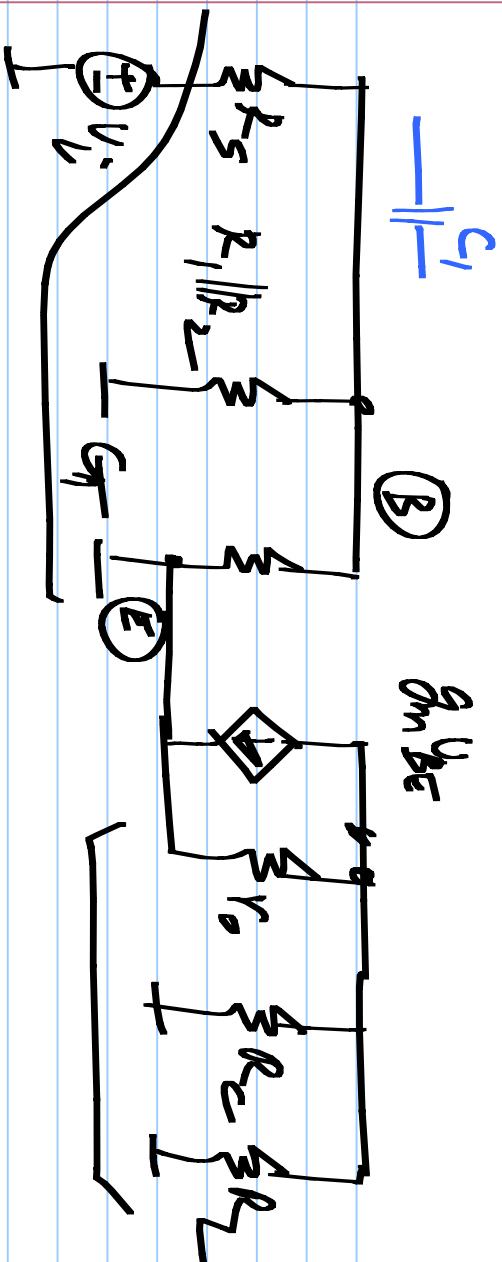
~~Can't be
very large~~



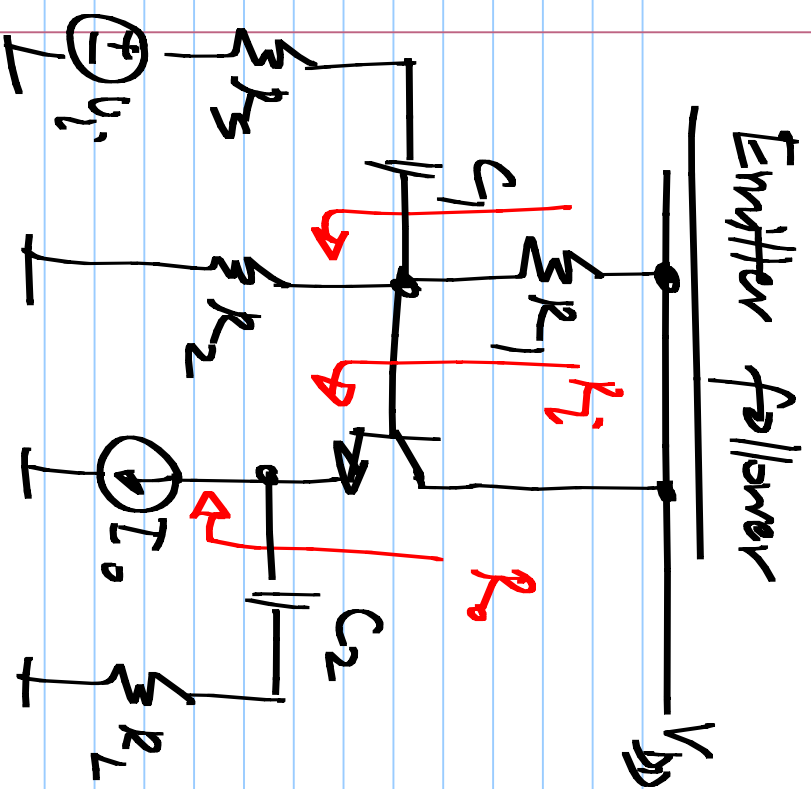
$$\frac{I_O}{\beta + 1}$$

Bipolar Common Emitter Amplifier





$$\frac{v_o}{v_i} = -g_m \left(R_L \parallel R_2 \parallel r_o \right) \cdot \frac{R_1 \parallel R_2 \parallel r_f}{R_1 \parallel R_2 \parallel r_f + R_S}$$



Find R_i & R_o [neglect r_o]

MOS

$$R_i = \infty$$

$$R_o = 1/g_m$$

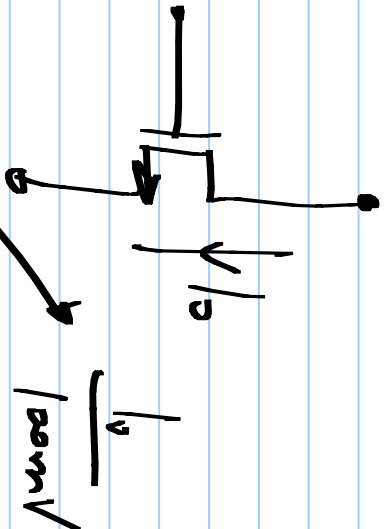
Higher g_m for a given

Current

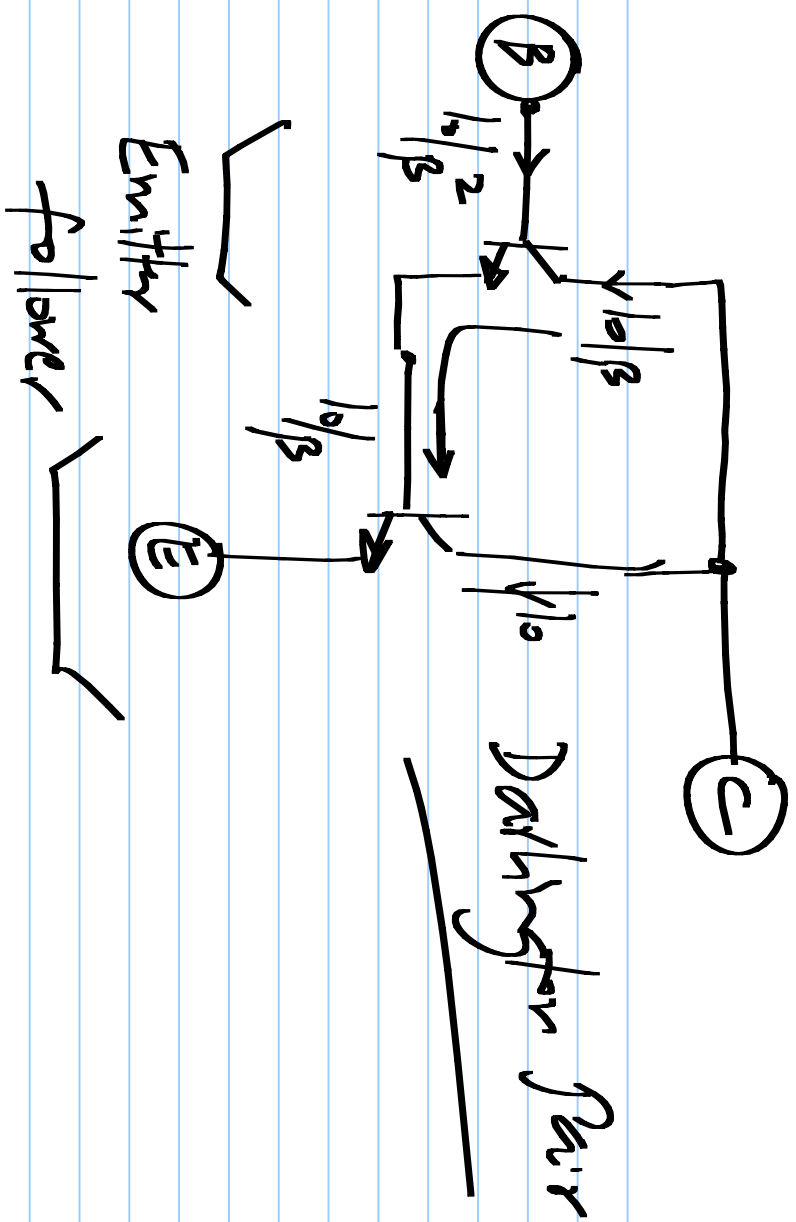
↑ high freq. currents
↑ low power analogs

$$V_t = kT/q$$

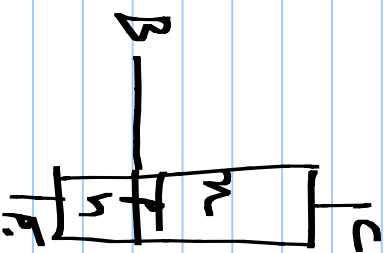
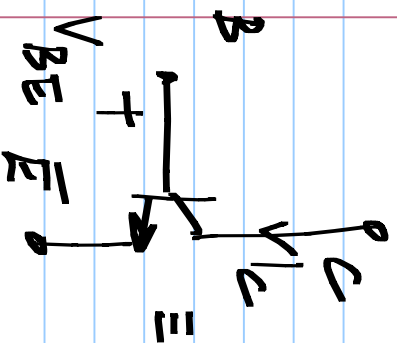
$$g_m = \frac{I_0}{V_t} = \frac{I_0}{25mV}$$



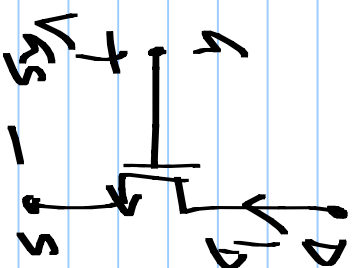
$$g_m = \frac{I_D}{(V_{GS} - V_t)/2}$$



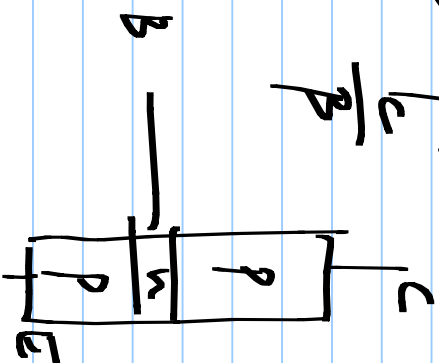
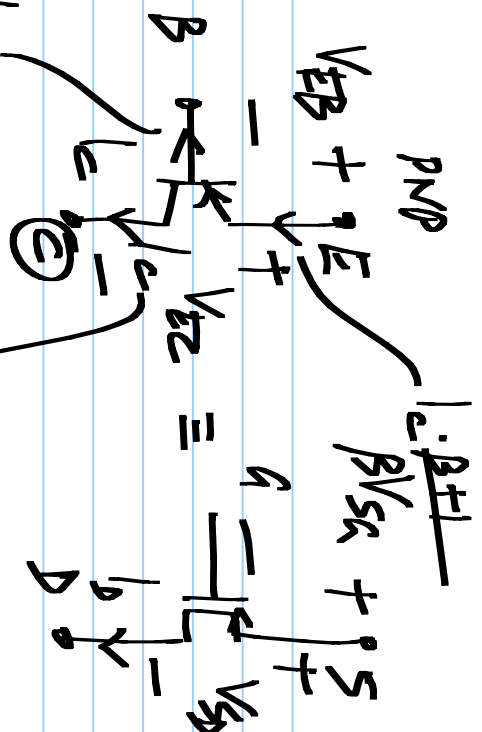
NPN



nMOS



PNP



$$I_C \approx I_S \exp\left(\frac{V_{BE}}{V_T}\right) \left(1 + \frac{V_{CE}}{V_A}\right)$$

