

## Module 3 : Equilibrium of rods and plates

### Lecture 14 : Bending of a rod under concentrated load

The Lecture Contains:

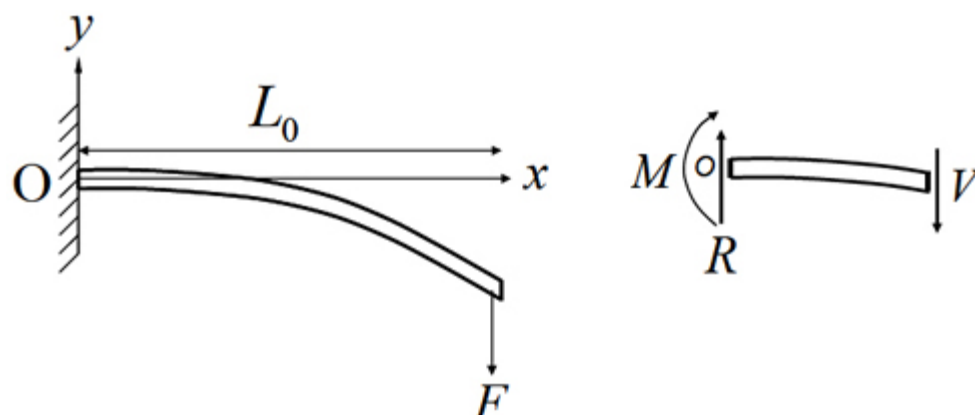
- ☰ Bending of a rod under concentrated load
- ☰ Bending of a rod under concentrated vertical load
- ☰ Euler buckling instability

This lecture is adopted from the following book

1. "Theory of Elasticity, 3 rd edition" by Landau and Lifshitz. Course of Theoretical Physics, vol-7

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## Bending of a rod under concentrated load



At the free end of the rod it is not acted upon by any reaction force. Say at any cross-section at a length  $L$  from wall, the reaction force is  $V$ , then from force balance,

$$V = R = F \Rightarrow \frac{dV}{dL} = 0 \quad (14.1)$$

$$\bar{V} = -F\bar{e}_y \text{ and } -\bar{K} = -F\bar{e}_y$$

From equation 13.1,  $K_y = F$ . Then from,  $\bar{M} = EI\bar{t} \times \frac{d\bar{t}}{dL} + \bar{t}C\Omega_\zeta$  we have the following:

$$\text{For a circular rod } \Omega_\zeta = 0, \text{ so that } \frac{d\bar{M}}{dL} = EI\bar{t} \times \frac{d^2\bar{t}}{dL^2} = EI \frac{d\bar{r}}{dL} \times \frac{d^3\bar{r}}{dL^3}.$$

But from equation 13.3,  $\frac{d\bar{M}}{dL} = \bar{V} \times \bar{t}$ , so that

$$EI \frac{d\bar{r}}{dL} \times \frac{d^3\bar{r}}{dL^3} = \bar{V} \times \bar{t} = \bar{V} \times \frac{d\bar{r}}{dL} \quad (14.2)$$

Now from the following expression of the tangent to any point on the rod and its derivatives,

$$\begin{aligned} \bar{t} &= \frac{d\bar{r}}{dL} = \sin \theta \bar{e}_x - \cos \theta \bar{e}_y \\ \frac{d^3\bar{r}}{dL^3} &= \left( \cos \theta \bar{e}_x + \sin \theta \bar{e}_y \right) \frac{d^2\theta}{dL^2} + \left( \sin \theta \bar{e}_x - \cos \theta \bar{e}_y \right) \left( \frac{d\theta}{dL} \right)^2 \\ \frac{d\bar{r}}{dL} \times \frac{d^3\bar{r}}{dL^3} &= \left( \sin \theta \bar{e}_x - \cos \theta \bar{e}_y \right) \times \left( \left( \cos \theta \bar{e}_x + \sin \theta \bar{e}_y \right) \frac{d^2\theta}{dL^2} + \left( \sin \theta \bar{e}_x - \cos \theta \bar{e}_y \right) \left( \frac{d\theta}{dL} \right)^2 \right) \\ &= \frac{d^2\theta}{dL^2} \bar{e}_x \times \bar{e}_y \end{aligned} \quad (14.3a)$$

$$\bar{V} \times \frac{d\bar{r}}{dL} = -F \bar{e}_y \times (\sin \theta \bar{e}_x - \cos \theta \bar{e}_y) = F \sin \theta \bar{e}_x \times \bar{e}_y \quad (14.3b)$$

From equation 14.3a and b, we derive,

$$EI \frac{d^2 \theta}{dL^2} = F \sin \theta \quad (14.4)$$

Putting  $L = L_0 \eta$  and  $\kappa = \frac{EI}{FL_0^2}$ , we finally obtain,

$$\frac{d^2 \theta}{d\eta^2} = \frac{1}{\kappa} \sin \theta \quad (14.5)$$

Equation 8.36 is solved with the boundary conditions:

$$\text{at } \eta = 0, \theta = \pi/2 \text{ and at } \eta = 1, \theta = \theta_0 \text{ and } d\theta/d\eta = 0 \quad (14.6)$$

Integrating equation 14.5 and using b.c. 14.6,

$$\frac{d\theta}{d\eta} = \pm \sqrt{\frac{2}{\kappa}} \sqrt{\cos \theta_0 - \cos \theta} \quad (14.7)$$

Integrating the above expression we obtain the following integral, known as the elliptic integral

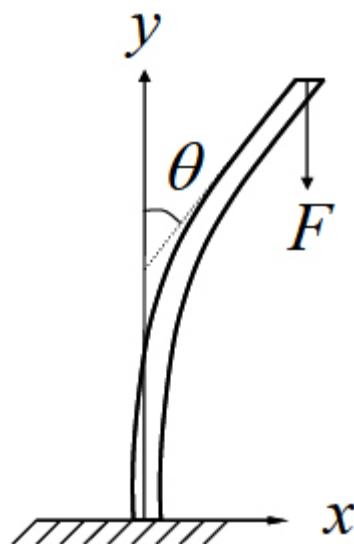
$$\sqrt{\frac{2}{\kappa}} = \int_{\theta_0}^{\pi/2} \frac{d\theta}{\sqrt{\cos \theta_0 - \cos \theta}} \quad (14.8)$$

and,  $\theta(\eta)$  is obtained in terms of elliptic functions.

The shape of the rod is finally obtained in terms of dimensionless lengths as:

$$\eta_x = \int \sin \theta d\eta, \quad \eta_y = \int \cos \theta d\eta$$

## Bending of a rod under concentrated vertical load



At any cross section, the internal stress is constant and is equal to  $\bar{F} = -F\bar{e}_y$ . Similar to earlier examples, the expression of the tangent to the rod at any location and its derivatives can be written in terms of the angle  $\theta$ ,

$$\begin{aligned}\bar{t} &= \frac{d\bar{r}}{dL} = \sin \theta \bar{e}_x + \cos \theta \bar{e}_y \\ \frac{d^3\bar{r}}{dL^3} &= (\cos \theta \bar{e}_x - \sin \theta \bar{e}_y) \frac{d^2\theta}{dL^2} - (\sin \theta \bar{e}_x + \cos \theta \bar{e}_y) \left( \frac{d\theta}{dL} \right)^2 \\ \frac{d\bar{r}}{dL} \times \frac{d^3\bar{r}}{dL^3} &= (\sin \theta \bar{e}_x + \cos \theta \bar{e}_y) \times \left( (\cos \theta \bar{e}_x - \sin \theta \bar{e}_y) \frac{d^2\theta}{dL^2} - (\sin \theta \bar{e}_x + \cos \theta \bar{e}_y) \left( \frac{d\theta}{dL} \right)^2 \right) \quad (14.9a,b) \\ &= -\frac{d^2\theta}{dL^2} \bar{e}_x \times \bar{e}_y \\ \bar{F} \times \frac{d\bar{r}}{dL} &= -F\bar{e}_y \times (\sin \theta \bar{e}_x + \cos \theta \bar{e}_y) = F \sin \theta\end{aligned}$$

From equation (14.9)a and b,

$$-EI \frac{d^2\theta}{dL^2} = F \sin \theta \text{ or } EI \frac{d^2\theta}{dL^2} + F \sin \theta = 0 \quad (14.10)$$

Boundary conditions are:

$$\text{At } L = 0: \theta = 0, \quad L = L_0: \theta = \theta_0 \text{ and } \frac{d\theta}{dL} = 0 \quad (14.11)$$

Solution of equation 14.10:

Multiplying both left and right hand side of equation 14.10

$$2 \frac{d^2 \theta}{dL^2} \frac{d\theta}{dL} + \frac{2F}{EI} \frac{d\theta}{dL} \sin \theta = 0 \Rightarrow \frac{d}{dL} \left[ \frac{d\theta}{dL} \right]^2 - \frac{2F}{EI} \frac{d}{dL} (\cos \theta) = 0$$

Integrating,

$$\left[ \frac{d\theta}{dL} \right]^2 - \frac{2F}{EI} \cos \theta + c = 0 \quad (14.12)$$

Using boundary condition  $L = L_0 : \theta = \theta_0$  and  $\frac{d\theta}{dL} = 0$ , we have,

$$-\frac{2F}{EI} \cos \theta_0 + c = 0 \Rightarrow c = \frac{2F}{EI} \cos \theta_0$$

From equation 14.12 we have,

$$\begin{aligned} \left[ \frac{d\theta}{dL} \right]^2 &= \frac{2F}{EI} (\cos \theta - \cos \theta_0) \\ \Rightarrow L &= \sqrt{\frac{EI}{2F}} \int_0^{\theta_0} \frac{d\theta}{\sqrt{(\cos \theta - \cos \theta_0)}} \end{aligned} \quad (14.13)$$

Then, for small  $\theta$ , we have

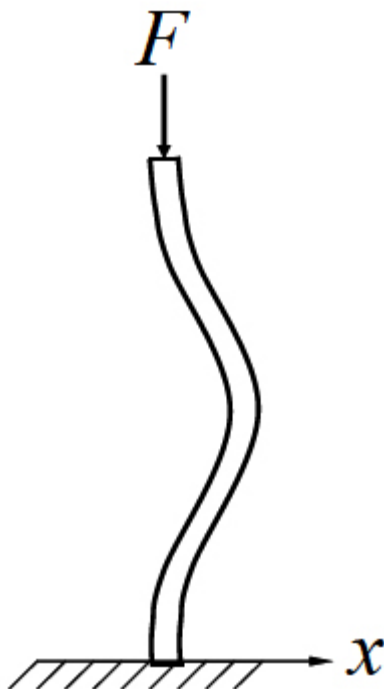
$$\begin{aligned} L &= \sqrt{\frac{EI}{2F}} \int_0^{\theta_0} \frac{d\theta}{\sqrt{2 \sin^2 \frac{\theta_0}{2} - 2 \sin^2 \frac{\theta}{2}}} \Rightarrow L = \sqrt{\frac{EI}{F}} \int_0^{\theta_0} \frac{d\theta}{\sqrt{\theta_0^2 - \theta^2}} \\ \Rightarrow L &= \sqrt{\frac{EI}{F}} \sin^{-1} \left( \frac{\theta}{\theta_0} \right) \Bigg|_0^{\theta_0} = \sqrt{\frac{EI}{F}} \frac{\pi}{2} \end{aligned} \quad (14.14)$$

The above expression yields a critical force for buckling of the rod under vertical load

$$F_{cr} > \frac{\pi^2 EI}{4L^2} \quad (14.15)$$

## Euler buckling instability

Bending of a rod with both ends constrained to be in the same straight line:



The force balance equation for the above situation can be written as,

$$\left[ \frac{d\theta}{dL} \right]^2 - \frac{2F}{EI} \cos \theta + c = 0 \quad (14.16)$$

We can integrate this equation using boundary condition that at  $L = \frac{L_0}{2}$  :  $\theta = \frac{\pi}{2}$  and  $\frac{d\theta}{dL} = 0$ , which yields  $c = 0$ , leading to

$$\left[ \frac{d\theta}{dL} \right]^2 = \frac{2F}{EI} \cos \theta \quad (14.17)$$

Notice that equation 14.16 is the analog of oscillation of a suspended pendulum for which the equation of motion can be written as

$$m \frac{d^2 x}{dt^2} + (mg) \sin \theta = 0$$

The critical load for buckling for the above problem can be obtained as,

$$F_{cr} > \frac{4\pi^2 EI}{L^2} \quad (14.18)$$

