

Module 6: Navier-Stokes Equation

Lecture 16: Couette and Poiseuille flows

☰ NS equation and example

☰ Ex.1 Couette-flow:

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Module 6: Navier-Stokes Equation

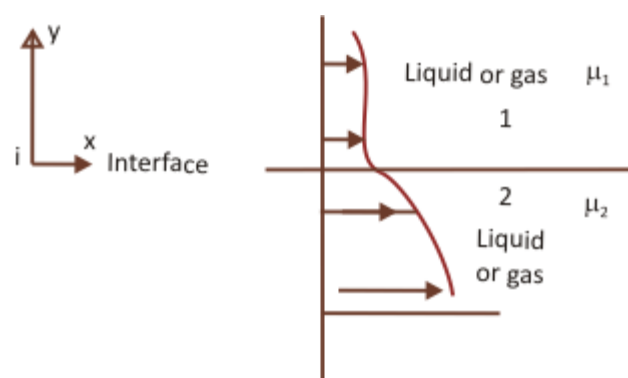
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NS equation and examples

$$\rho \left[\frac{\partial \vec{V}}{\partial t} + (\vec{V} \cdot \nabla) \vec{V} \right] = -\nabla p + \rho \vec{g} + \mu \nabla^2 \vec{V}$$

Before we apply the NS equation, let us make a note that the NS equation is a 2nd order PDE. Therefore, 2 BCs are required for \vec{V} along each direction to solve for the velocity-field. We should note the common boundary conditions:

1. No slip condition at the solid surface: it is an experimental observation that the relative velocity at the surface is zero. So, $\mathbf{V}_x = \mathbf{V}_y = \mathbf{V}_z = \mathbf{0}$ at a stationary solid surface
2. At the interface of liquid-gas or liquid-liquid (immiscible fluids), there is no jump in the velocity, shear stress and pressure



(Fig. 16a)

(gradients maybe different) $\mu_1 \left. \frac{\partial V_x}{\partial y} \right|_{i^-} = \mu_2 \left. \frac{\partial V_x}{\partial y} \right|_{i^+}$

3. Symmetric BC: $\left(\tau_{yx}|_{i^-} = \tau_{yx}|_{i^+} \right)$

At the center- line of tube or rectangular channel, velocity- gradient is zero.



(Fig. 16b)

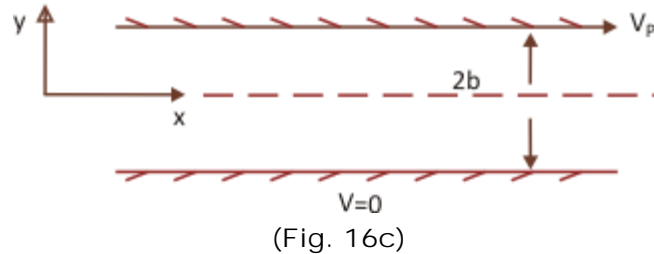
$$\frac{\partial V_z}{\partial r} = 0$$

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Ex.1 Couette-flow

Consider the steady-state 2D-flow of an incompressible Newtonian fluid in a long horizontal rectangular channel. The bottom surface is stationary, whereas the top surface is moved horizontally at the constant velocity, V_p . Determine the velocity field in the channel. Assume fully developed flow.



Assumption: $\rho = c$, and Newtonian fluid \Rightarrow NS is applicable

$$\text{2D flow} \Rightarrow V_z = 0 \text{ and } \frac{\partial}{\partial z} = 0$$

$$\text{Fully developed flow: } \frac{\partial v_x}{\partial x} = 0$$

(Note: this statement is equivalent to saying, neglect the end effects)

$$\text{Apply continuity: } \nabla \cdot \vec{V} = 0$$

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

For fully developed flow, first term is zero.

$$\text{Therefore, } \frac{\partial v_y}{\partial y} = 0 \Rightarrow v_y \text{ is constant along } y \text{ direction.}$$

But, $v_y = 0$ at $y = \pm b$ (no-slip condition)

So, $v_y = 0$ everywhere. $v_x(y) \neq 0$

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Apply NS in x-direction:

$$\rho \left(\frac{\partial V_x}{\partial t} + V_x \frac{\partial V_x}{\partial x} + V_y \frac{\partial V_x}{\partial y} \right) = -\frac{\partial p}{\partial x} + \rho g_x + \mu \left(\frac{\partial^2 V_x}{\partial x^2} + \frac{\partial^2 V_x}{\partial y^2} \right)$$

1st term is zero for SS; $\frac{\partial V_x}{\partial x} = 0$ for fully developed flow; $V_y = 0$. Horizontal $\Rightarrow g_x = 0$. Therefore, the equation is simplified as

$$0 = -\frac{\partial p}{\partial x} + \mu \frac{\partial^2 V_x}{\partial y^2}$$

No external pressure was applied and in addition, it is a long plate $\Rightarrow \frac{\partial p}{\partial x} = 0$

$$\mu \frac{\partial^2 V_x}{\partial y^2} = 0$$

Integrate twice, $\mu V_x = C_1 y + C_2$

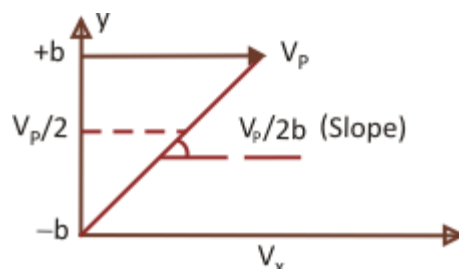
Apply BC (1) $y = -b, V_x = 0$ (no slip condition)

BC (2) $y = b, V_x = V_p$

Solve for c_1 and c_2 to obtain

$$V_x = \frac{V_p}{2} \left(1 + \frac{y}{b} \right) \Rightarrow \text{This is the expression for velocity profiles in a Couette flow}$$

(Note: at $y = 0, \frac{\partial V_x}{\partial y} = \frac{V_p}{2b} \neq 0$).



(Fig. 16d)

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Example 2: Suppose that an external pressure-drop along x-direction is applied across the channel, in addition to the conditions mentioned in example 1. Now, calculate the velocity profiles in the channel.

- X- momentum balance is now modified to

$$0 = -\frac{\partial p}{\partial x} + \mu \frac{\partial^2 v_x}{\partial y^2}$$

Y – momentum balance:

$$0 = -\frac{\partial p}{\partial y} \quad (v_y = 0)$$

- $p \neq f(y)$ and $\frac{\partial p}{\partial x} = \frac{dp}{dx}$ ($p = p(x)$ only)

But, v_x is a function of y only. This implies that $\frac{dp}{dx} = \mu \frac{\partial^2 v_x}{\partial y^2} = p'$ (constant)

Integrating twice,
$$v_x = \frac{p'}{\mu} \frac{y^2}{2} + c_1 y + c_2$$

Apply BCs to obtain

$$v_x = -\frac{p' b^2}{2\mu} \left(1 - \frac{y^2}{b^2}\right) + \frac{V_p}{2} \left(1 + \frac{y}{b}\right)$$

You should check the two BCs.

- Special case
1. $p' = 0$ (Same as in example 1)
 2. $V_p = 0$

$$v_x = -\frac{p' b^2}{2\mu} \left(1 - \frac{y^2}{b^2}\right) = \frac{\Delta p}{L} \frac{b^2}{2\mu} \left(1 - \frac{y^2}{b^2}\right)$$

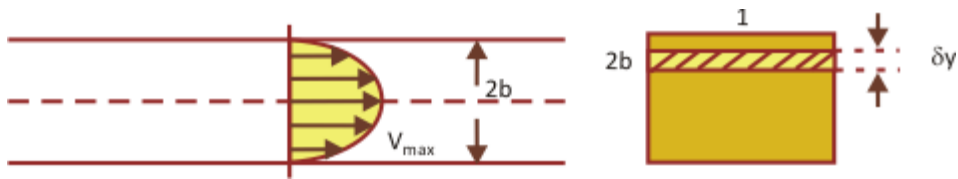
$$V_{\max} = \frac{\Delta p}{L} \frac{b^2}{2\mu} \quad (y = 0), \quad \text{where, } p' = -\frac{p_1 - p_2}{2} = \frac{\Delta p}{L}$$

$$v_x(y) = V_{\max} \left(1 - \frac{y^2}{b^2}\right); \quad V_{\max} = \frac{\Delta p}{L} \frac{b^2}{2\mu}$$

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- This is called Poiseuille-flow (velocity profile is parabolic)



(Fig. 16e)

- Determine the average velocity in the channel

$$\bar{V} = Q/A = Q/2b$$

$$Q = \int_{-b}^{+b} V_x(y) \cdot \underbrace{\delta y \cdot 1}_{\delta A} = \int_{-b}^{+b} V_{\max} \left(1 - \frac{y^2}{b^2}\right) \delta y$$

Simplify to show that $\bar{V} = \frac{2}{3} V_{\max}$

or, $V_{\max} = 1.5 \bar{V}$

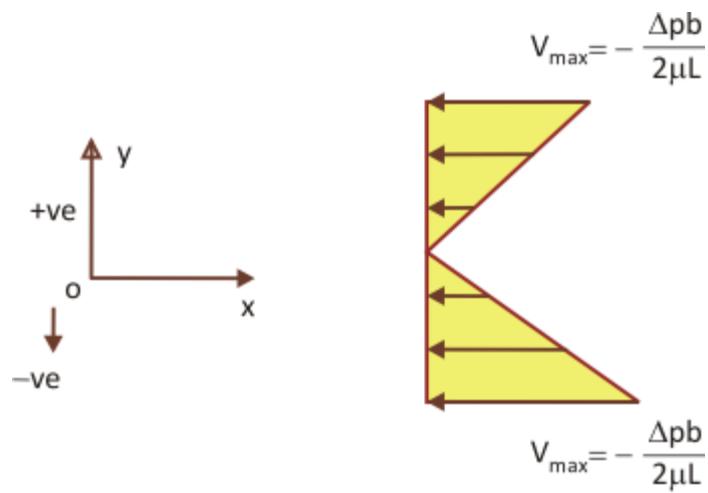
Next, plot τ_{yx} for Poiseuille and Couette flow

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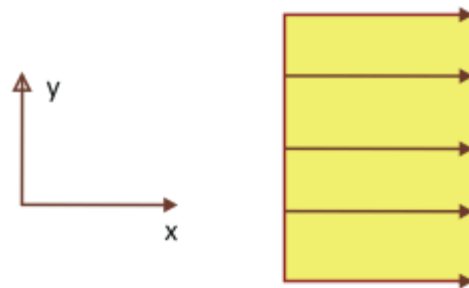
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1. $\tau_{yx} = \mu \frac{dV_x}{dy} = -2 V_{\max} \mu \frac{y}{b^2} = -\frac{\Delta p}{L} y$: Poiseuille flow



(Fig. 16f)

2. $\tau_{yx} = \frac{V_P}{2b}$



(Fig. 16g)

$$\tau_{yx} = \text{constant} = \frac{V_P}{2b}$$