Module 4: Chemistry of combustion
Lecture 21: Chain Branching Explosion

The Lecture Contains:
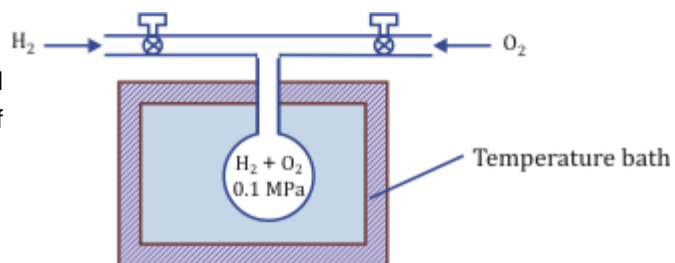
- Chain Branching Explosion
- Multistep Reaction Mechanism
- Quasi-Steady State Approximation
- Partial Equilibrium Approximation (PEA)
- Global Kinetics

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Chain Branching Explosion

Explosion:

Very rapid combustion of fuel and oxidizer, leading to violent release of energy.
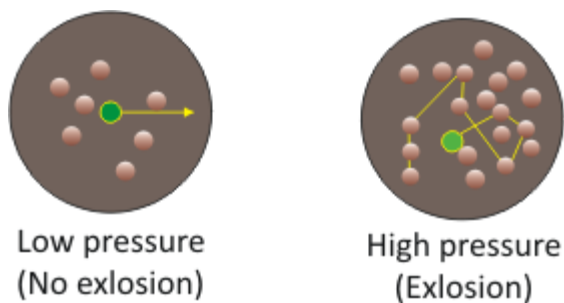

(Figure 20.2)

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Chain Branching Explosion

- To begin with, stoichiometric mixture of H_2 and O_2 is kept in a container.
- Temperature is increased beyond 773 K.
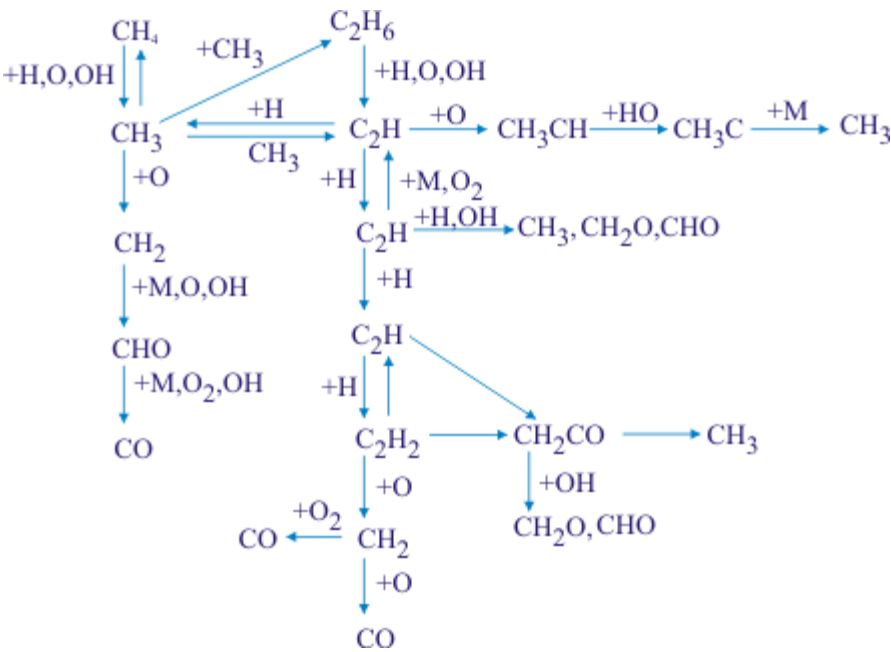- **Result:** Very rapid chemical reaction with explosion.

Low pressure
(No exlosion)

High pressure
(Exlosion)
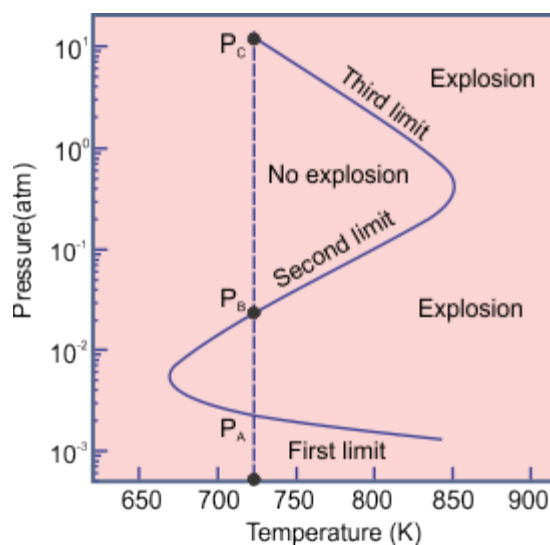
(Figure 21.1)

Regimes in the explosion chart

1. First limit
2. Second limit
3. Third limit

(Figure 21.2)

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Multistep Reaction Mechanism

$$CH_4 \xrightarrow{+CH_3} C_2H_6$$
$$+H,O,OH \quad \quad +H,O,OH$$
$$CH_3 \xrightarrow[CH_3]{+H} C_2H \xrightarrow{+O} CH_3CH \xrightarrow{+HO} CH_3C \xrightarrow{+M} CH_3$$
$$+O \quad \quad +H \Big\updownarrow +M,O_2$$
$$CH_2 \quad \quad C_2H \xrightarrow{+H,OH} CH_3, CH_2O, CHO$$
$$+M,O,OH \quad \quad +H$$
$$CHO \quad \quad C_2H$$
$$+M,O_2,OH \quad +H$$
$$CO \quad \quad C_2H_2 \xrightarrow{\quad} CH_2CO \xrightarrow{\quad} CH_3$$
$$+O \quad \quad +OH$$
$$CO \xleftarrow{+O_2} CH_2 \quad CH_2O, CHO$$
$$+O$$
$$CO$$

Quasi-Steady State Approximation

- Radicals are formed during combustion
- Half life period of radicals - Very small
- Rate of formation = Rate of destruction

Relate radical concentration with
measurable concentration of other species

Consider the two step chain reaction,

$$A_1 \overset{k_1}{\rightarrow} A_2 \; ; \qquad\qquad A_2 \overset{k_2}{\rightarrow} A_3 \; ;$$

Reaction rate of the three species,

$$\frac{dC_{A_1}}{dt} = -k_1 C_{A_1} \qquad\qquad \frac{dC_{A_2}}{dt} = k_1 C_{A_1} - k_2 C_{A_2} \qquad\qquad \frac{dC_{A_3}}{dt} = k_2 C_{A_2}$$

Initial condition, $at\; t = 0; \; C_{A_1} = C_{A_1,in}; \; C_{A_2} = 0; \; C_{A_3} = 0$

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Applying initial condition,

$$C_{A_1} = C_{A_1,in} e^{(-k_2 t)}$$

$$C_{A_2} = C_{A_1,in} \frac{k_1}{k_1 - k_2} \left[e^{(-k_2 t)} - e^{(-k_1 t)} \right]$$

$$C_{A_3} = C_{A_{1,0}} \left[1 - \frac{k_1}{k_1 - k_2} e^{(-k_2 t)} + \frac{k_2}{k_1 - k_2} e^{(-k_1 t)} \right]$$
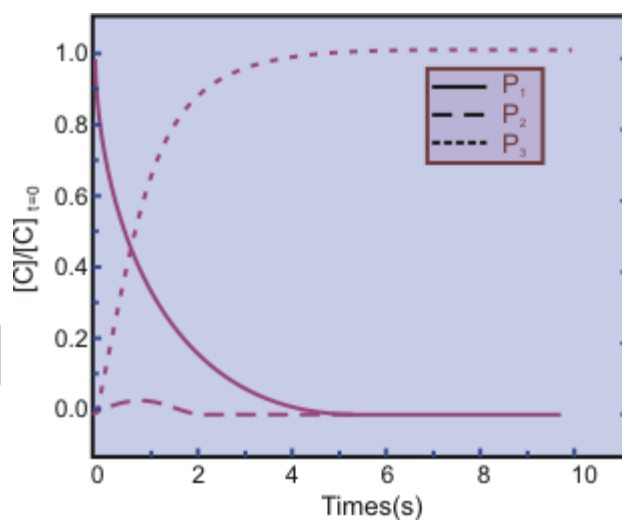
(Figure 21.3)

Applying QSSA method to A_2,

$$\frac{dC_{A_2}}{dt} = k_1 C_{A_1} - k_2 C_{A_2} \approx 0$$

$$k_1 C_{A_1} = k_2 C_{A_2} ; \qquad \frac{dC_{A_3}}{dt} = k_1 C_{A_1,in} e^{(-k_2 t)} ;$$

$$\frac{dC_{A_3}}{dt} = k_1 C_{A_1} ; \qquad C_{A_3} = C_{A_1,in} \left[1 - e^{(-k_2 t)} \right] ;$$

QSSA method predicts the concentration of species especially when $k_2 \gg k_1$

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Partial Equilibrium Approximation (PEA)

PEA expresses concentration of unknown species in terms of known concentrations.

Consider NO formation mechanism,

$$O + N_2 \Leftrightarrow NO + N \qquad k_f = 2 \times 10^{14}\, e^{(-315/RT)}$$

Reaction Rate (RR) for NO species:

$$\frac{dC_{NO}}{dt} = k_f C_O C_{N_2}$$

Note 1: O and N_2 concentration are required to determine RR

Note 2: Rate of formation and destruction of O is very high

Difficult to measure the concentration of O!!!

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Step 1:

Assume partial equilibrium for O_2 molecule

Step 2:

PEA	QSSA
Reaction attains steady state	Species attains steady state

Relate O_2 molecule to O by

$$O_2 \Leftrightarrow 2O$$

Equilibrium constant

$$K_C = \frac{C_O^2}{C_{O_2}}$$

Note !

➤ Thermal NO – Less dependent on CO_2
➤ Thermal NO – Temperature dependent
➤ NO reduction – By reducing combustion temperature

Reaction Rate (RR) for NO species:

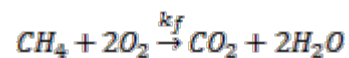$$\frac{dC_{NO}}{dt} = k_f \left(K_C\, C_{O_2} \right)^{0.5} C_{N_2}$$

Caution !

❑ In real situation, particular reaction may not attained equilibrium
❑ PEA provides satisfactory results only at high temperature !
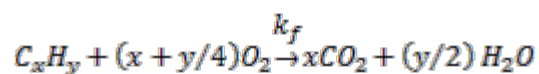
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Global Kinetics

Single step methane combustion:

$$CH_4 + 2O_2 \xrightarrow{k_f} CO_2 + 2H_2O$$

Overall reaction rate (CH_4)

$$\frac{dC_{CH_4}}{dt} = Ae^{(-E/R_uT)}C_{CH_4}^m C_{O_2}^n$$

Global kinetic scheme for an arbitrary hydrocarbon (C_xH_y):

$$C_xH_y + (x + y/4)O_2 \xrightarrow{k_f} xCO_2 + (y/2)H_2O$$

Overall reaction rate (C_xH_y)

$$\frac{dC_xH_y}{dt} = -A_f e^{(-E/R_uT)}C_{C_xH_y}^m C_{O_2}^n$$

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