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The Barrett and Nix model applies to grain boundary sliding and creep data from  $\Upsilon$ -TiAl corresponded to the power law breakdown regime.

No, the answer is incorrect. Score: 0

## **Accepted Answers:**

The Barrett and Nix model required an activation energy of grain boundary diffusion activation energy whereas the creep data from  $\Upsilon$ -TiAl could be explained with grain boundary diffusion activation energy.

| 9) The creep parameters n, p and Q stand for  | 1 point                   |
|---|---------------------------|
| Grain size exponent, stress exponent and activation energy respectively   |                           |
| Stress exponent, grain boundary exponent and activation energy respectively   | 1                         |
| Strain exponent, grain size exponent and temperature exponent respectively  | £                         |
| Stress exponent, grain size exponent and activation energy respectively   |                           |
| No, the answer is incorrect.<br>Score: 0  |                           |
| <b>Accepted Answers:</b><br>Stress exponent, grain size exponent and activation energy respective   | <sup>∍ly</sup> in         |
| 10)The post creep microstructure shown in the figure below indicates deformation controlled by  | 1 point<br>8 <sup>+</sup> |
|   |                           |
| Ref. R. Korla, A. H. Chokshi, Metall. Mater. Trans A, 2014  |                           |
| Viscous glide creep   |                           |
| Power law breakdown   |                           |
| Grain boundary sliding  |                           |
| Harper-Dorn creep   |                           |
| No, the answer is incorrect.<br>Score: 0  |                           |
| Accepted Answers:<br>Grain boundary sliding   |                           |
| 11)In first order kinetic reaction, the rate of the reaction is directly proportional to theof the reactant.  |                           |
|   |                           |
| No, the answer is incorrect.  |                           |
| Accepted Answers:   |                           |
| (Type: String) concentration  |                           |
|   | 1 point                   |
| 12During creep studies, there is always a risk of phase transformation  | 1 point                   |
| or change in microstructural length scales due to exposure to high<br>temperature. What would be the correct approach to ensure that the ma<br>characteristics such as phases, microstructural length scales such as gra<br>size / interparticle spacing etc do not change? | aterial<br>ain            |
|   |                           |

Heat treat the sample at a test temperature lower than the creep test temperature. Plastically deform the material at room temperature and subsequently heat treat the sample at a test temperature higher than the creep test temperature. Heat treat the sample at a temperature higher than the creep test temperature. Plastically deform the material at room temperature and subsequent heat treat the sample at a test temperature lower than the creep test temperature. No, the answer is incorrect. Score: 0 **Accepted Answers:** Heat treat the sample at a temperature higher than the creep test tempe  $\prod$ <sup>13</sup>A material displayed a strain rate of deformation of  $4.5 \times 10^{-7}$  s-1 after a time of 100 h under an applied stress of 45 MPa. What will be the deformation rate after a time of 300 h if the material is displaying a logarithmic creep behavior?  $\varepsilon = \varepsilon_0 + \alpha \ln(1 + \gamma t)$  $\odot$  5.4 x 10<sup>-7</sup> s<sup>-1</sup> 3.37 x 10<sup>-7</sup> s<sup>-1</sup>  $1.8 \times 10^{-8} \text{ s}^{-1}$ 2.72 x 10<sup>-7</sup> s<sup>-1</sup> No, the answer is incorrect. Score: 0 **Accepted Answers:** 2.72 x 10<sup>-7</sup> s<sup>-1</sup>

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