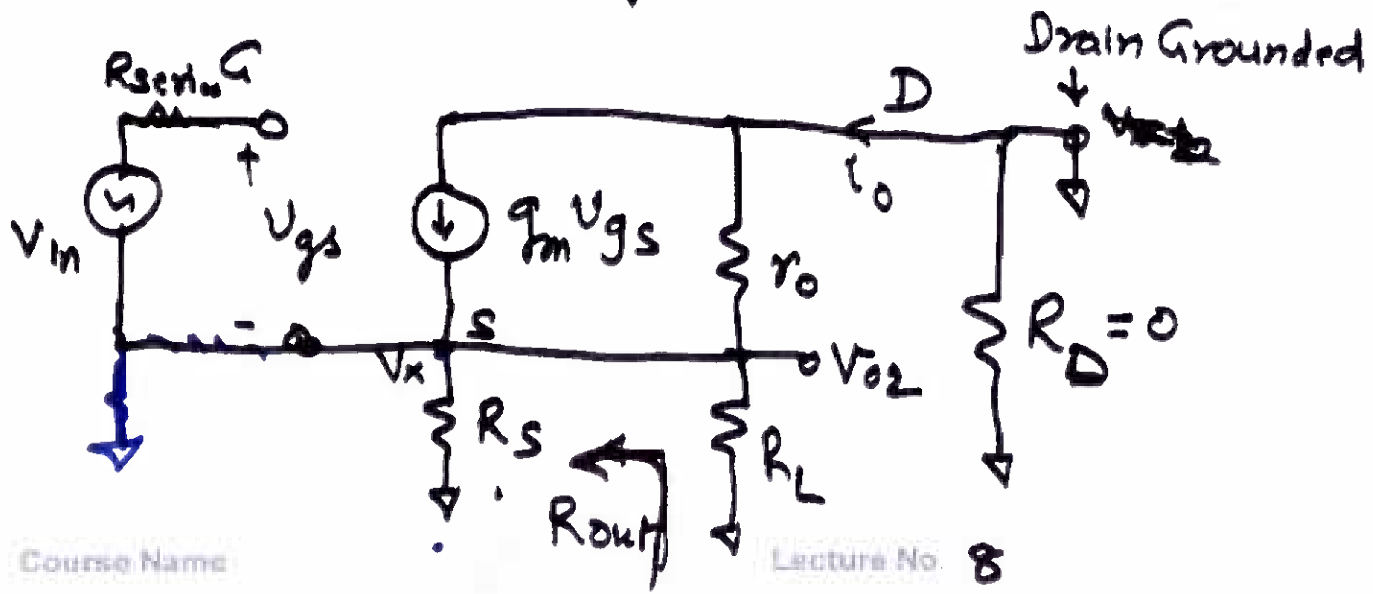
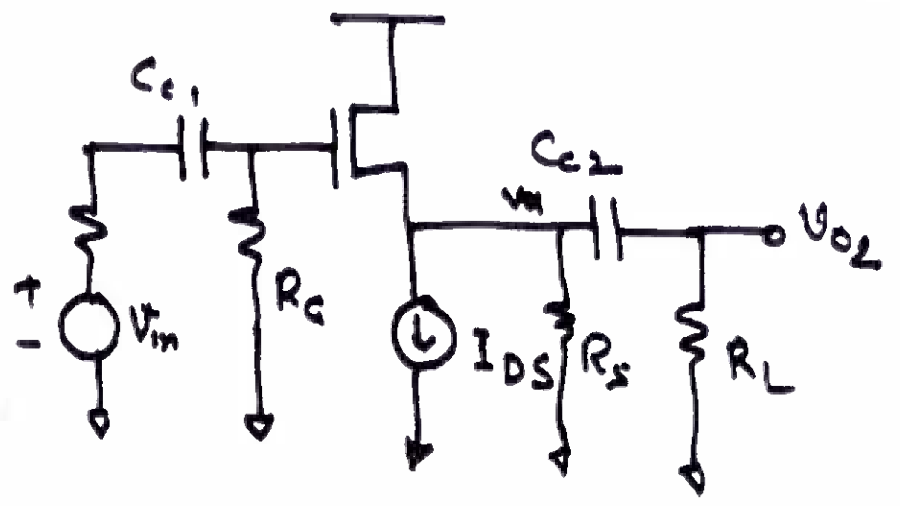


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# Common Drain or Source Follower Amplifier



$$\text{Load} = R_s \parallel R_L$$

$$= R_{sL}$$

Assuming  $r_o \rightarrow \infty$

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$$v_{o2} = \frac{g_m v_{gs} R_{SL}}{1 + g_m R_{SL}}$$

x  $v_{gs} = v_{in}$  as  $i_G = 0$

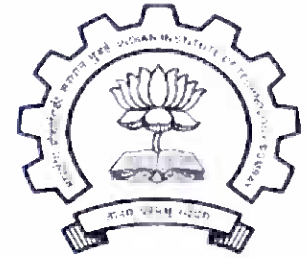
$$A_v = \frac{v_{o2}}{v_{in}} = \frac{g_m R_{SL}}{1 + g_m R_{SL}}$$

$$A_v \approx 1$$

$\therefore$  Output follows Input as it is

$\therefore$  The name Source Follower

$$v_{gs} = f(v_m)$$



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If  $r_o$  is finite

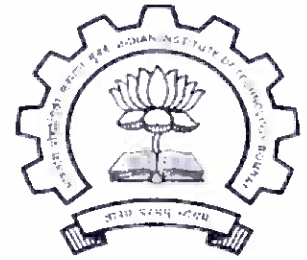
$$R_{SL} = R_S \parallel R_L \parallel r_o$$

If we consider Bias Network & source  
Input signal Generator Resistance

$$\text{Then } V_{gs} = \frac{R_G}{R_G + R_{source}} V_{in}$$

Clearly Input-resistance  $R_{in} = R_G$

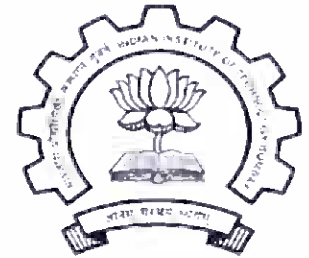
We need to evaluate Output resistance  $R_o$



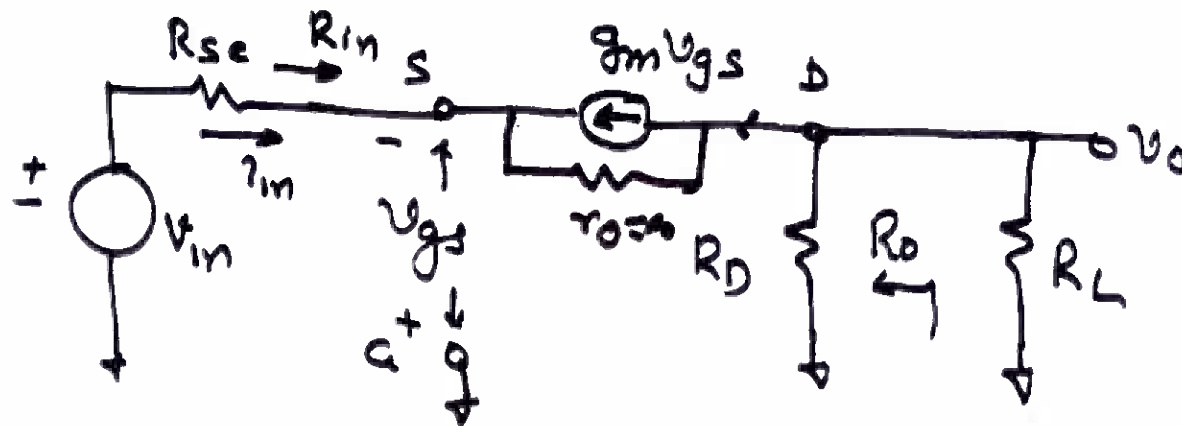
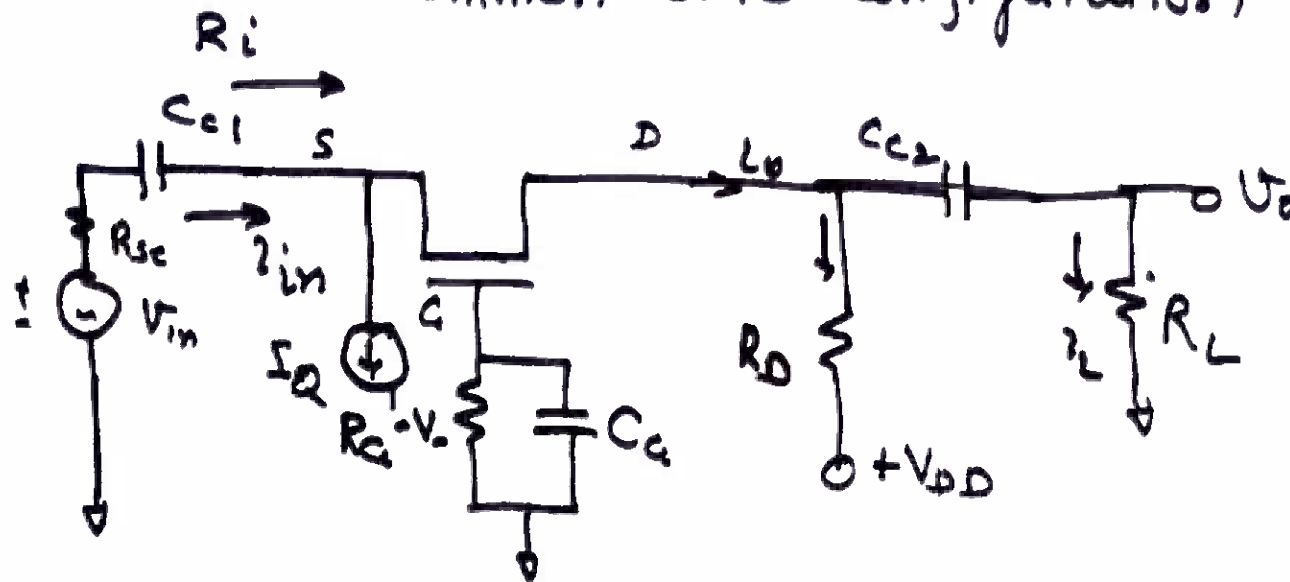
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# Common Gate Configuration



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Input Side

$$v_{in} = i_{in} R_{se} - v_{gs} \quad \text{from Input Loop} \quad - \textcircled{1}$$

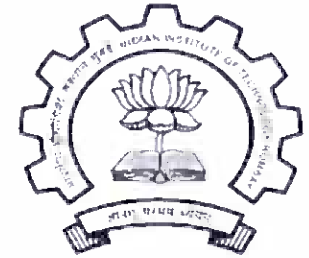
$$\text{However } i_{in} = -g_m v_{gs} \quad - \textcircled{2}$$

$$\text{or } v_{in} = -(g_m R_{se} + 1) v_{gs}$$

$$\text{or } v_{gs} = \frac{-v_{in}}{1 + g_m R_{se}} \quad - \textcircled{3}$$

Output Side

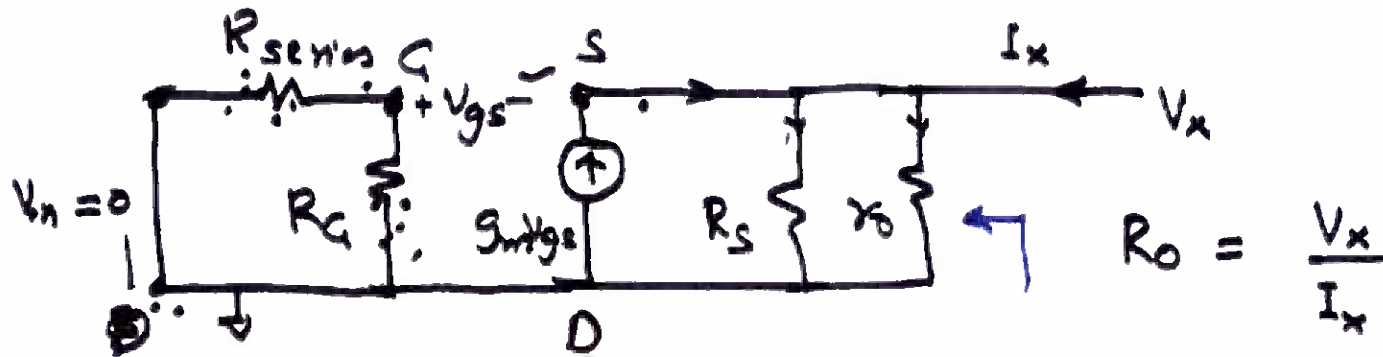
$$v_o = -g_m v_{gs} (R_D \parallel R_L) \quad - \textcircled{4}$$



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## Output Resistance evaluation



$$R_o = \frac{V_x}{I_x}$$

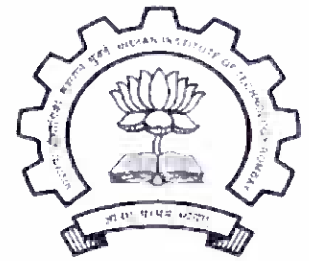
KCL  $\rightarrow I_x + g_m v_{gs} = \frac{V_x}{R_S} + \frac{V_x}{r_o}$

However  $v_x = -v_{gs}$  As no current in Input Side

$$\therefore I_x = g_m v_x + v_x \left( \frac{1}{R_S} + \frac{1}{r_o} \right) = \left( g_m + \frac{1}{R_S} + \frac{1}{r_o} \right) v_x$$

$$\text{or } R_o = \frac{v_x}{I_x} = \frac{1}{g_m + \left( \frac{1}{R_S} + \frac{1}{r_o} \right)}$$

$$= \frac{1}{\left( \frac{1}{g_m} + \frac{1}{R_S} + \frac{1}{r_o} \right)} = \frac{1}{\frac{1}{g_m} \parallel R_S \parallel r_o}$$



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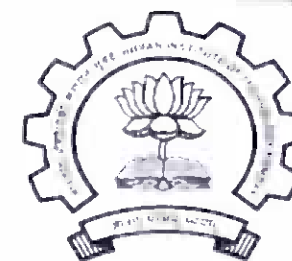
$$\therefore V_o = -g_m(R_D \parallel R_L) \left[ -\frac{V_{in}}{1 + g_m R_{se}} \right]$$

$$\therefore \frac{V_o}{V_{in}} = A_v = + \frac{g_m(R_D \parallel R_L)}{1 + g_m R_{se}}$$

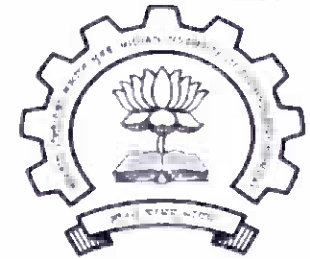
Here  $V_o$  and  $V_{in}$  are "In-Phase"

Exercise :-

$$\text{find } A_v = \frac{I_o}{I_{in}}$$



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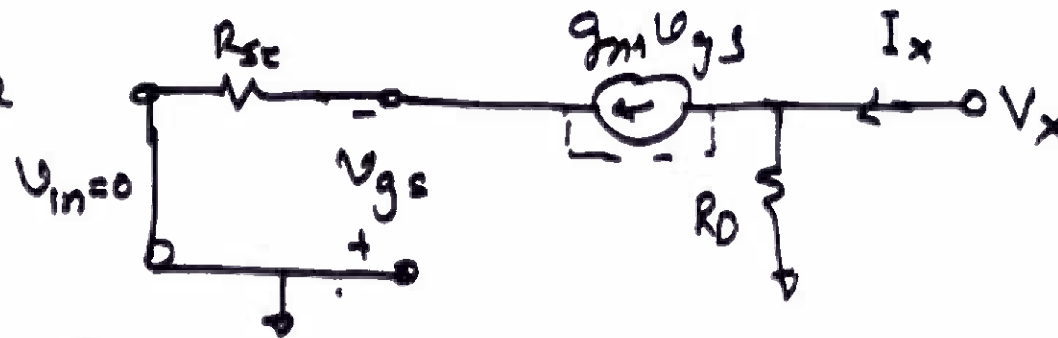
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Input Resistance:  $R_{in} = \frac{-v_{gs}}{i_{in}}$

However  $i_{in} = -g_m v_{gs}$

$\therefore R_{in} = \frac{1}{g_m}$

Output Resistance

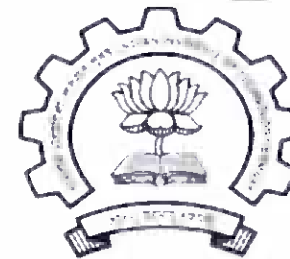


$\therefore R_o = \frac{v_x}{i_x} = R_D$

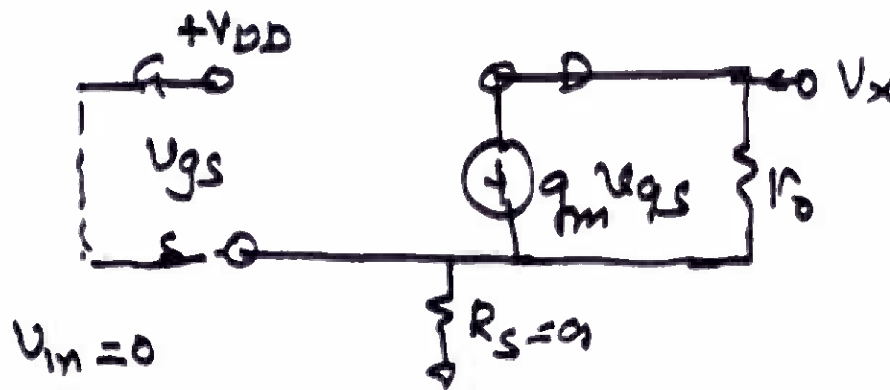
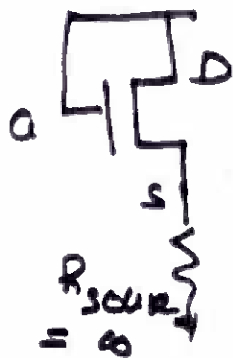
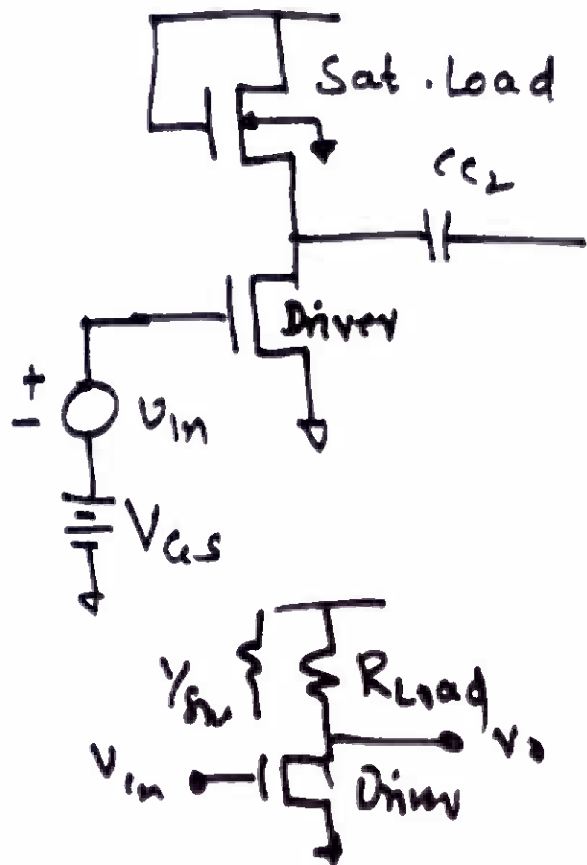


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# NMOS Amplifier with Sat. Load



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$$R_o = \frac{V_x}{I_x} = \left( \frac{1}{g_m} \parallel r_o \right) \approx \frac{1}{g_m}$$

$$\left( \frac{R_s}{1 + g_m R_s} \right) \approx \frac{1}{g_m}$$

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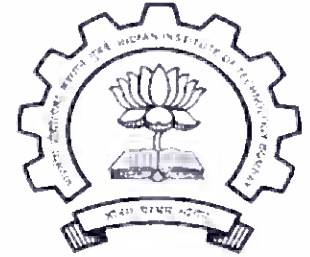
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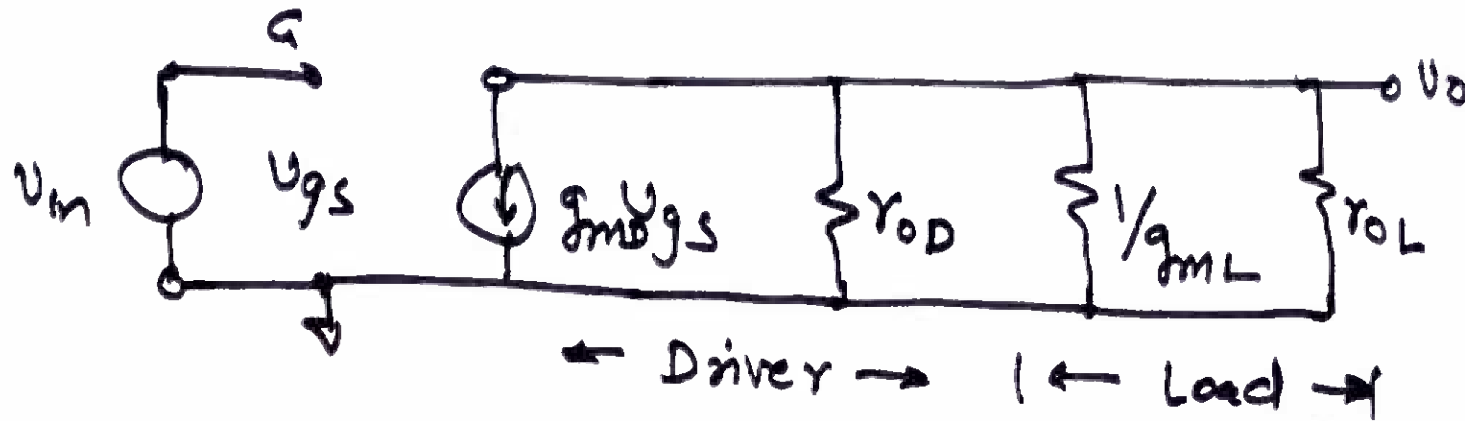
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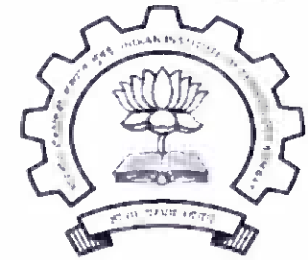
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$$A_v = \frac{v_o}{v_{in}} = - \frac{g_{mD}}{g_{mL}} = - \frac{\sqrt{2\beta_n'(W/L)_D I_{DQ}}}{\sqrt{2\beta_n'(W/L)_L I_{DQ}}}$$

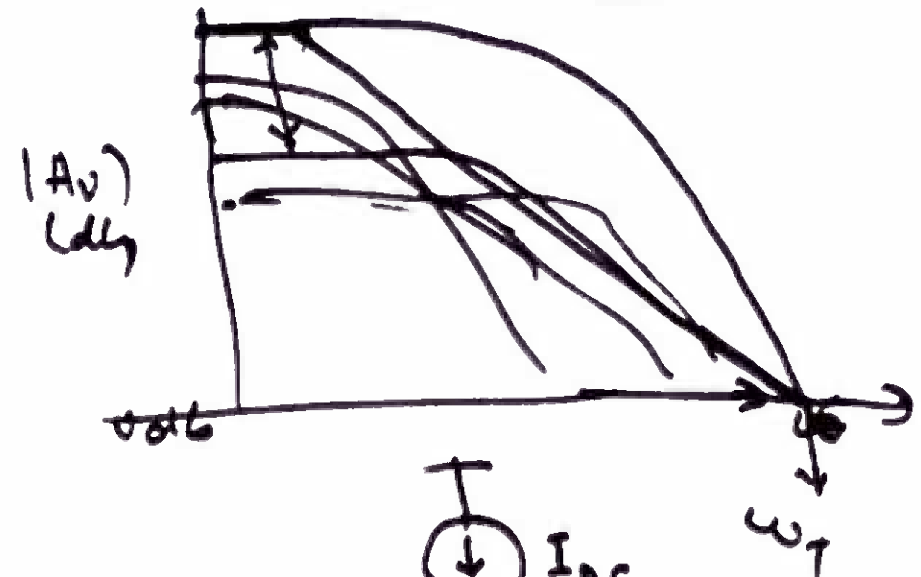
$$r_{OD} \gg \frac{1}{g_{mD}} \quad r_{OL} \gg \frac{1}{g_{mL}}$$

$$\therefore A_v = - \sqrt{\frac{(W/L)_D}{(W/L)_L}}$$



# Cascode Amplifier

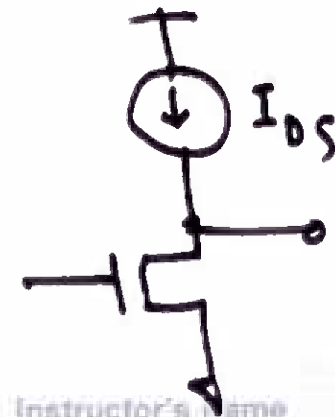
$$\omega_T = C_{BW} = \frac{g_m}{C_{in}}$$

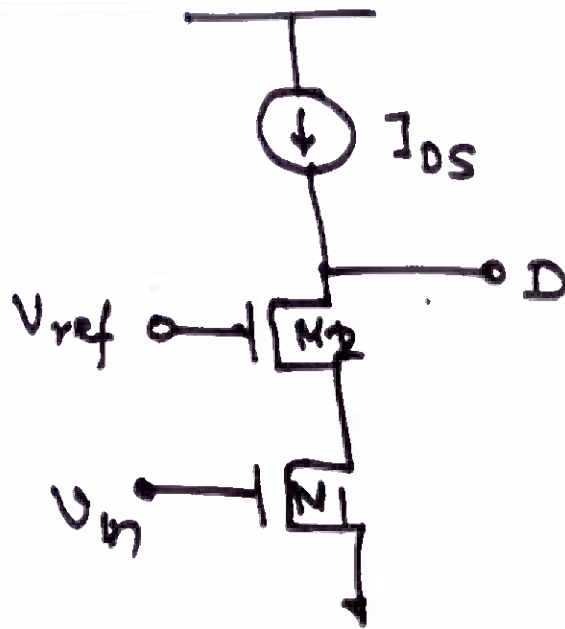


→ Cascode



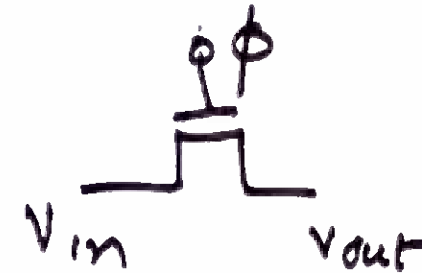
$$A = A_1 A_2 A_3$$





$$S_m = \frac{\partial I_{OS}}{\partial V_{CS}}$$

M<sub>1</sub> - CE  
M<sub>2</sub> - CE



$$|A| = g_m r_o$$

$\downarrow$   $\uparrow$   
 $g_m r_o$   
 $S_{m\text{ new}} = I_{\text{old}}$