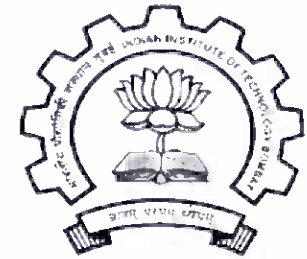


Slide No: ✖



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3/2/2011 Thursday

1st Quiz Cum Test

Venue GG1 / GG-2 EE Dept.

Time :— 9.30 PM to 10.30 PM

You Will Sit on your Left on every Desk

Course Name

Analog Circuits

Lecture No. 7

Instructor's Name

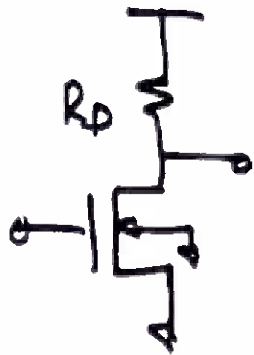
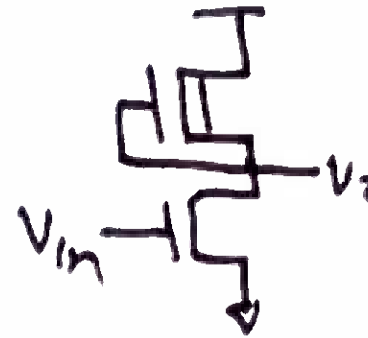
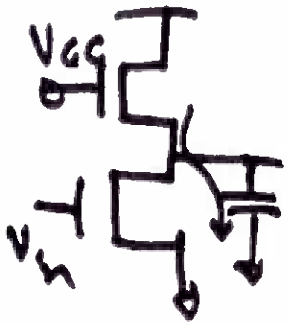
Prof. A. N. Chandorkar

Types of Amplifiers

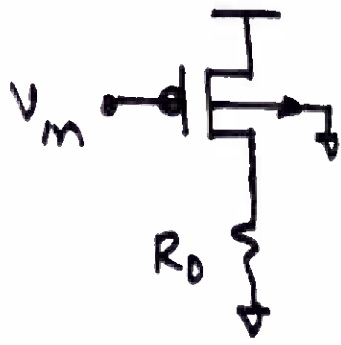


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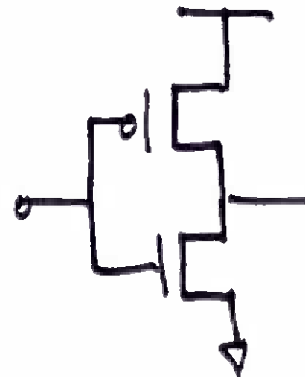
1. NMOS Amplifier
2. PMOS Amplifier
3. CMOS Amplifier



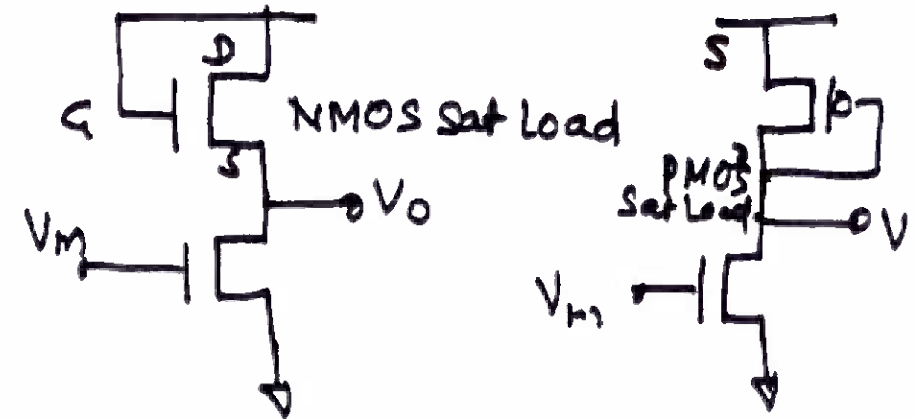
NMOS



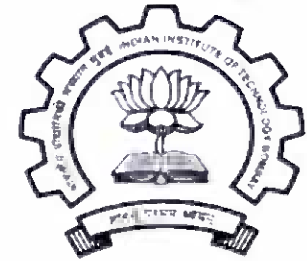
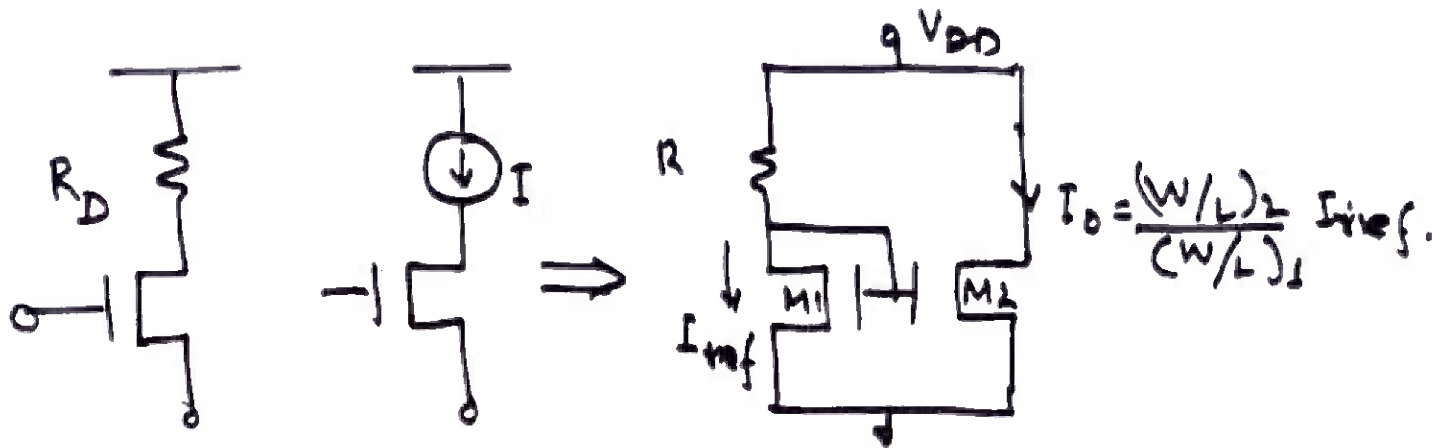
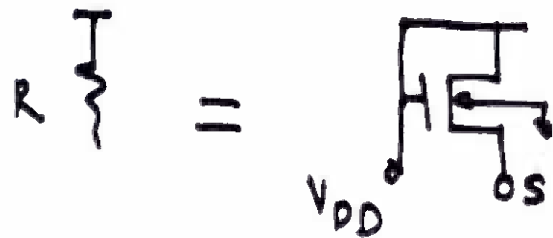
PMOS



CMOS



Loads in MOS Amplifiers

CDEEP
IIT BombayDiode
connected
load

Device in saturation

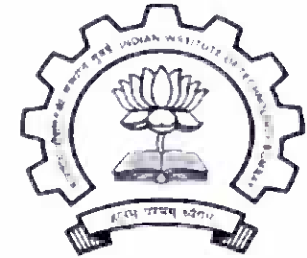
$$I_{DS} = \beta' (W/L) [V_{GS} - V_T]^2 (1 + \lambda V_{DS})$$

$$V_{GS} = V_{DS} = V_{DD} \quad \therefore (V_{GS} - V_T < V_{DS})$$

$$\therefore \frac{\partial I_{DS}}{\partial V_{DS}} = \beta [V_{DD} - V_T]^2 \lambda = \text{constant}$$

$$\therefore R = \frac{1}{\beta \lambda [V_{DD} - V_T]^2}$$

Slide No: 3



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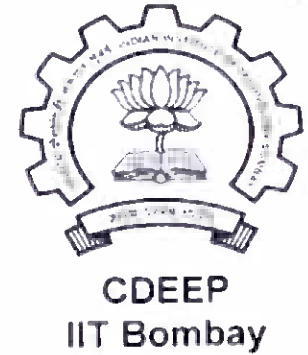
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Slide No: 4

(Circuit Basis)
Types of Amplifiers with MOSFETs.



- ① Common Source — Mostly Used
- ② Common Gate — Wider Bandwidth but Low Gain
- ③ Common Drain (Source Follower)

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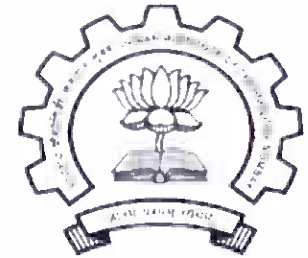
Lecture No. 7

Instructor's Name

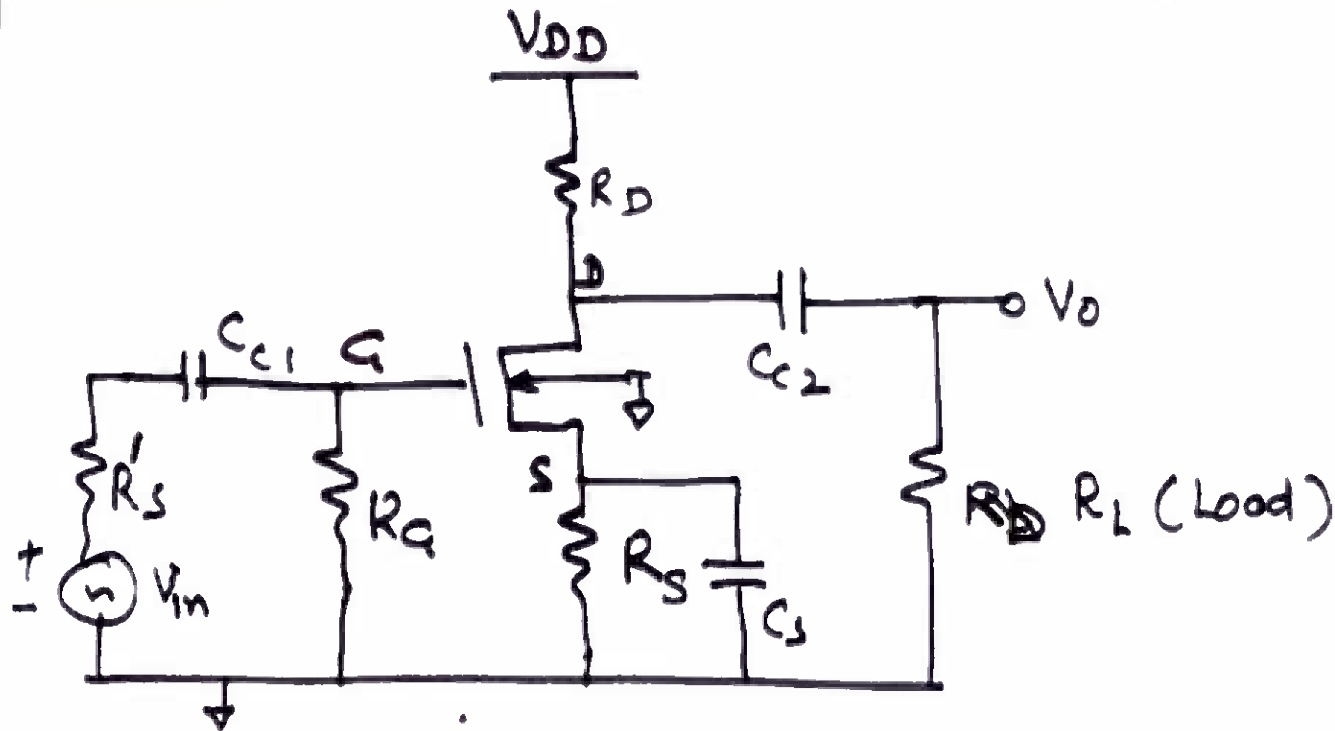
Prof. A. N. Chandorkar

Slide No: 5

Common Source Amplifier

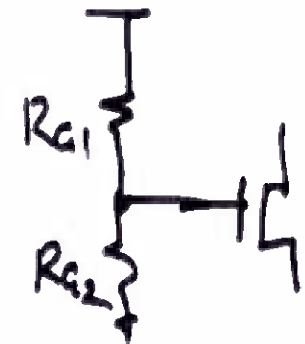


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Find $\frac{V_O}{V_{in}} = A_v$ of the Amplifier.

$$R_G = R_{C1} \parallel R_{C2}$$



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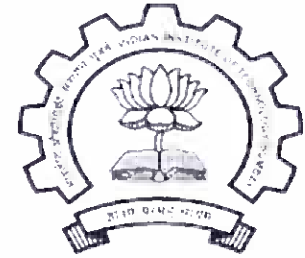
Analog Circuits

Lecture No. 7

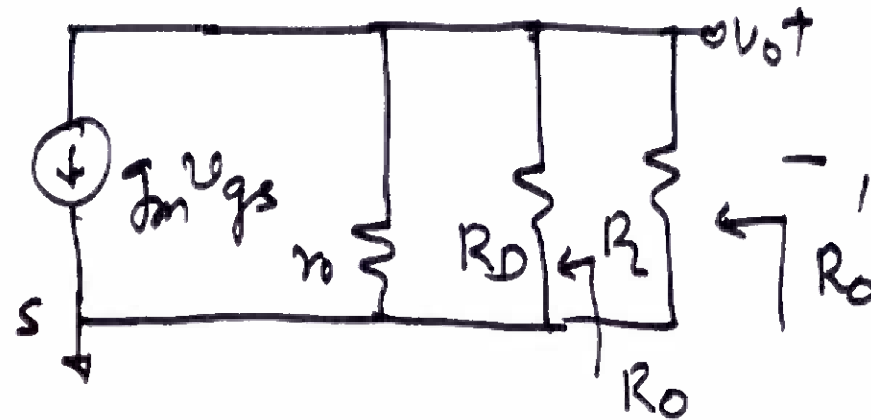
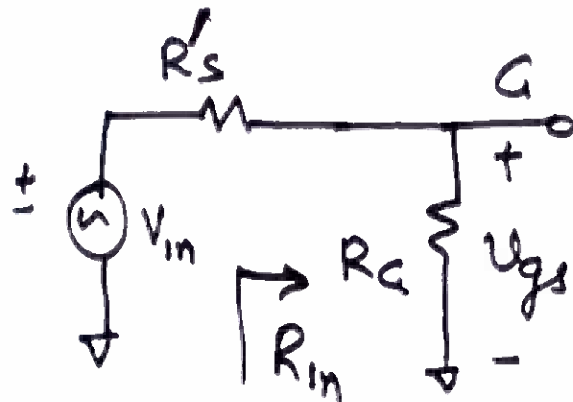
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Equivalent Ckt for Low frequency operation



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$$V_{gs} = \frac{R_G}{R_G + R'_S} \cdot V_{in} \cong V_{in} \quad \text{if } R_G \gg R'_S$$

\downarrow
 MN - 100's of Ω

$$\therefore V_o = -g_m (r_o \parallel R_D \parallel R_L) V_{in}$$

$$\therefore A_v = \frac{V_o}{V_{in}} = -g_m (r_o \parallel R_D \parallel R_L) \left[\frac{R_G}{R_G + R'_S} \right]$$

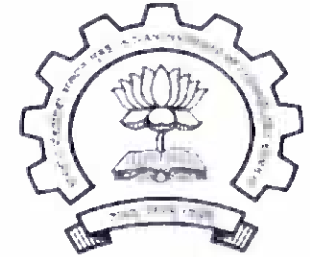
Slide No: 7

Input Impedance $R_{in} = R_i = R_G$

Output Impedance $R_o = r_o \parallel R_D$

If R_G is not $\gg R_s'$

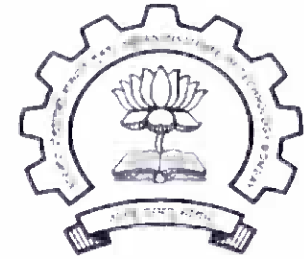
then
$$A_v = - \frac{R_G}{R_G + R_s'} \cdot g_m (r_o \parallel R_D \parallel R_L)$$



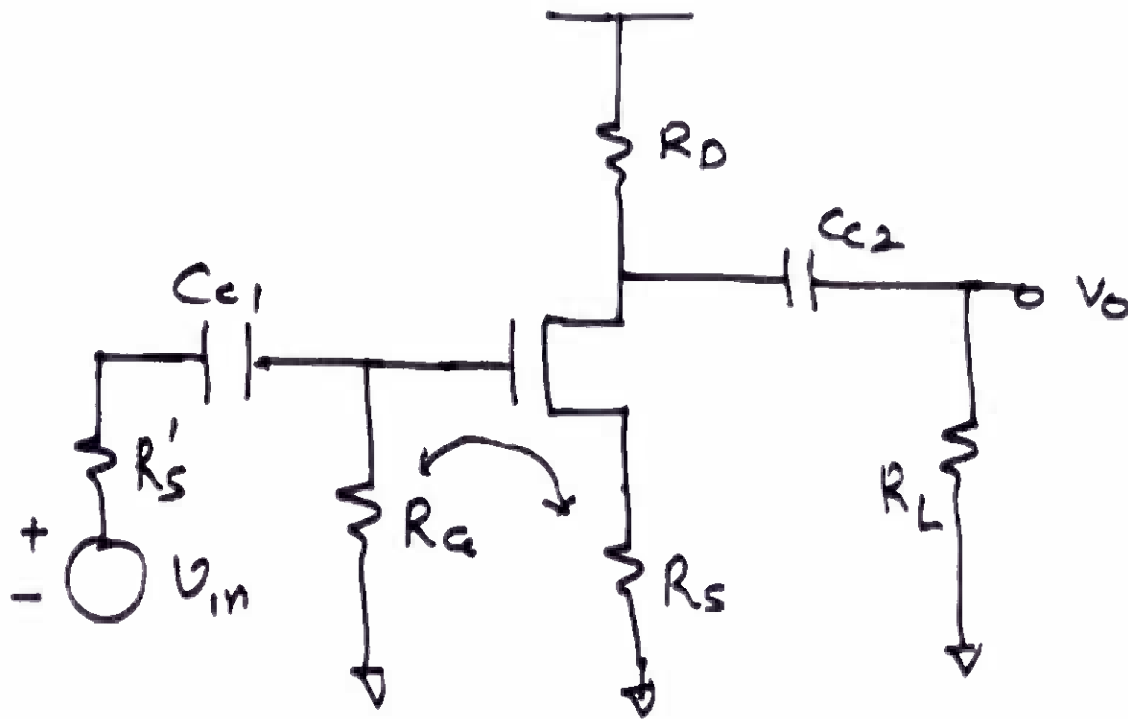
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CS Amplifier with Source Degeneration



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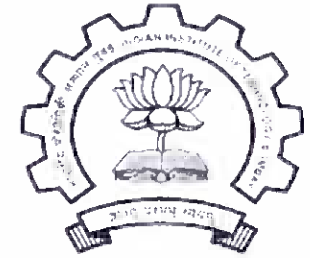


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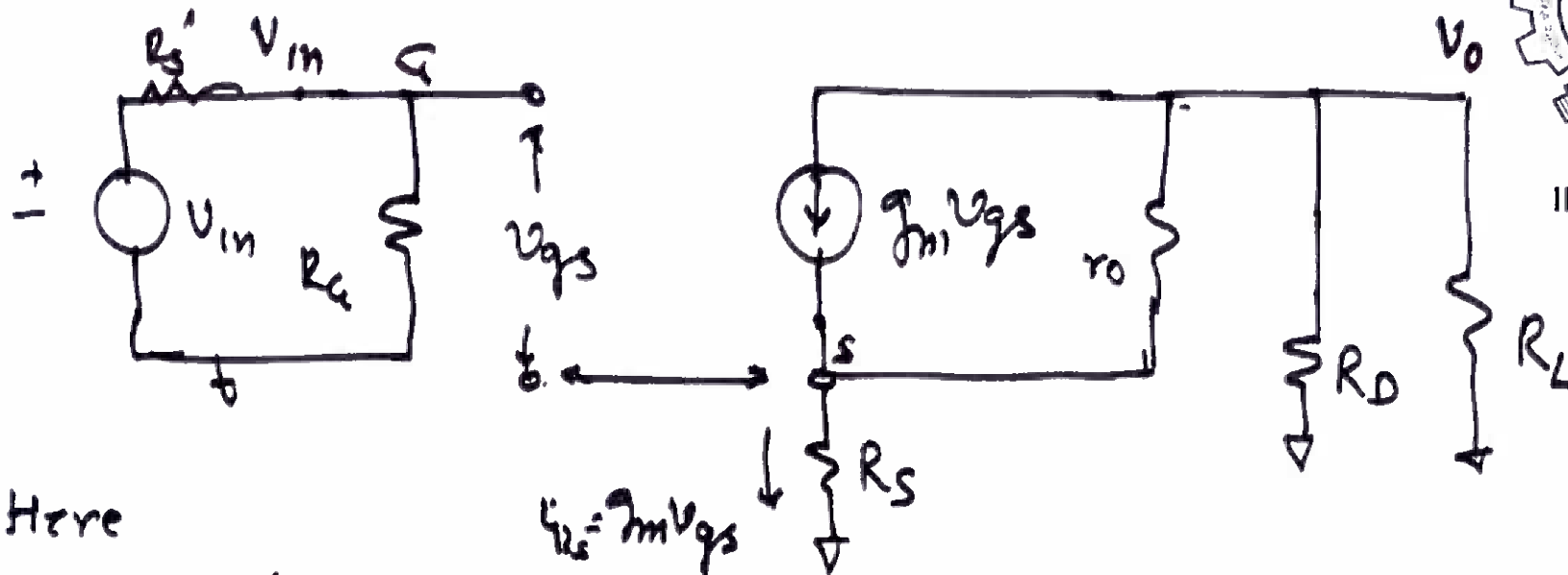
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Here

$$R_G \gg R_s'$$

$$i_{ds} = g_m V_{gs}$$

$r_o \rightarrow \text{V. High } (\lambda \text{ very low})$

We

$$V_{in} = V_{gs} + g_m V_{gs} \cdot R_s = V_{gs} (1 + g_m R_s)$$

$$\therefore V_{gs} = \frac{V_{in}}{1 + g_m R_s}$$

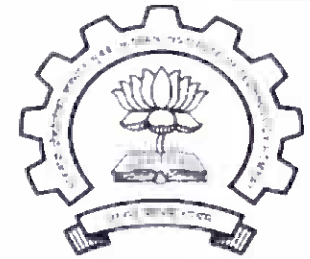
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$$\text{Now } v_o = -g_m v_{gs} \cdot (R_D \parallel R_L)$$

$$\text{or } v_o = -g_m (R_D \parallel R_L) \cdot \frac{v_{in}}{1 + g_m R_S}$$

$$\therefore A_v = \frac{v_o}{v_{in}} = -\frac{g_m}{1 + g_m R_S} \cdot (R_D \parallel R_L)$$

If $g_m R_S \gg 1$ Then

$$A_v = -\frac{R_D \parallel R_L}{R_S}$$

$$\text{Given } R_{G1} = 165 \text{ k}\Omega \quad V_{DD} = 5 \text{ V}$$

$$R_{G2} = 35 \text{ k}\Omega \quad V_{SS} = -5 \text{ V}$$

$$R_D \parallel R_L = 7 \text{ k}\Omega \quad R_S = 0.5 \text{ k}\Omega$$

$$R_S' = 0 \quad \beta_n = 2 \text{ mA/V}^2 \quad \Delta \lambda = 0, \quad V_{TN} = 0.8 \text{ V}$$

$$R_G = R_{G1} \parallel R_{G2}$$

$$\text{From DC analysis, } V_{GSQ} = 1.5 \text{ V}$$

$$V_{DSQ} = 6.25 \text{ V} \quad I_{DSQ} = 0.5 \text{ mA}$$

$V_{DSQ} > V_{GSQ} - V_T$
Device in Sat.

$$\therefore g_m = \sqrt{2 \beta_n I_{DSQ}} = 1.4 \text{ mA/V}$$



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$$\text{Also } r_o = \frac{1}{\lambda I_{D_S}} = \infty$$

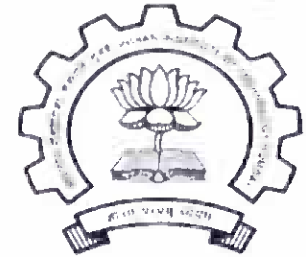
$$\therefore A_v = - \frac{g_m}{1 + g_m R_s} (R_D \parallel R_L)$$

$$= - \frac{1.4 \times 10^3}{1 + 1.4 \times 10^3 \times 0.5 \times 10^3} (7 \times 10^3)$$

$$A_v = -5.76$$

If we use $1 + g_m R_s = g_m R_s$

$$A_v = - \frac{7 \times 10^3}{0.5 \times 10^3} = -14$$



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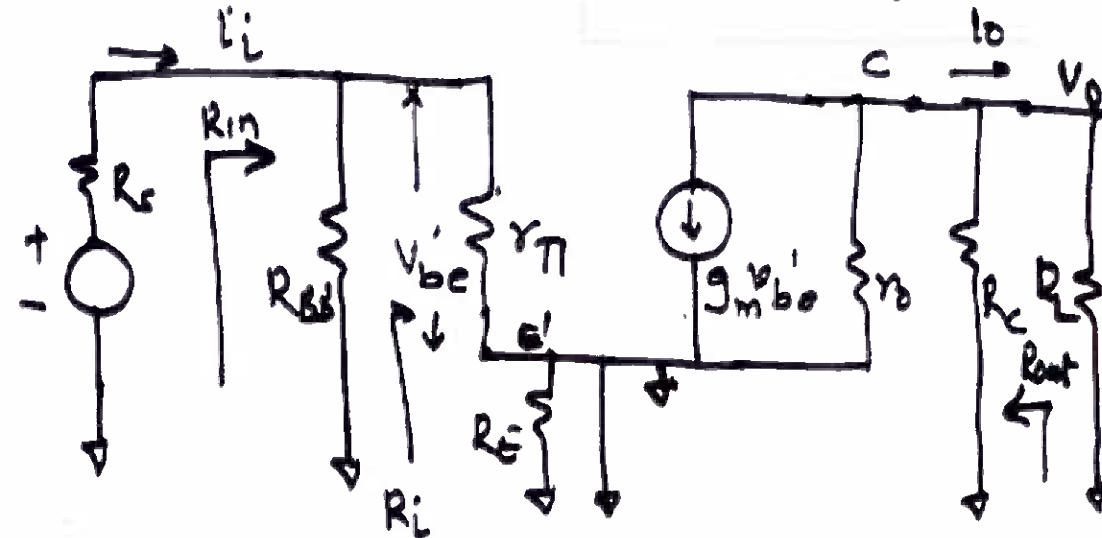
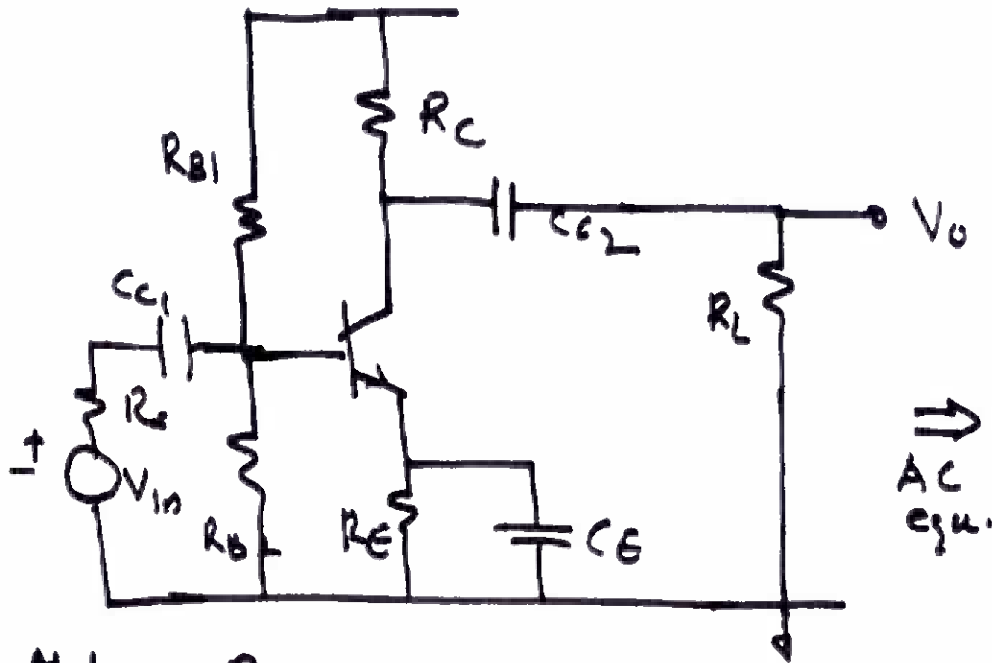
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A BJT Amplifier { Low frequency operation }



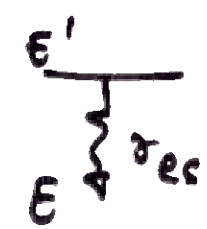
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At Low Frequency

$$\frac{1}{C_E S} \rightarrow 0 ; \quad \frac{1}{C_{c1} S} = \frac{1}{C_{c2} S} \rightarrow 0$$

$$\frac{1}{S(C_B + C_{c1})} \rightarrow \infty \quad \frac{1}{C_{c2} S} \rightarrow \infty$$





$$R_{in} = \frac{V_{in}}{i_i} = R_B \parallel R_i$$

$$R_B = R_{B1} \parallel R_{B2}$$

(Very High Value)

where $R_i = r_{\pi}$ as $R_B \gg r_{\pi}$

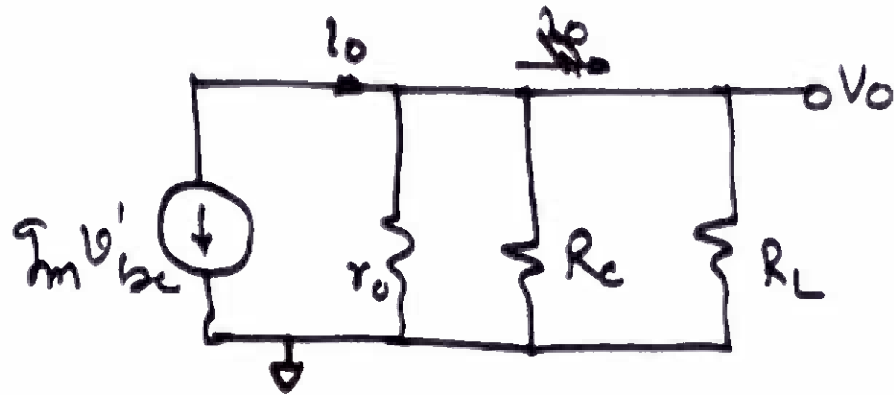
$$\therefore R_{in} = R_L = r_{\pi}$$

Now

$$v_{be'} = \frac{R_{in}}{R_{in} + R_s} \cdot v_{in} = v_{in} \frac{(R_B \parallel r_{\pi})}{R_s + (R_B \parallel r_{\pi})}$$

$$= \frac{r_{\pi}}{r_{\pi} + R_s} v_{in} \quad \text{if } R_B \gg r_{\pi}$$

At the Output mode Eq. Ckt is



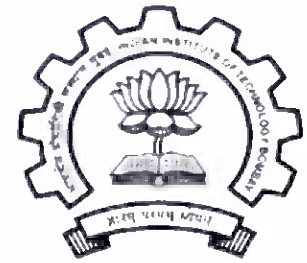
$$i_o = -g_m v'_{be}$$

$$v_o = i_o (r_o \parallel R_c \parallel R_L) = -g_m (r_o \parallel R_c \parallel R_L) v'_{be}$$

$$\therefore \frac{v_o}{v'_{be}} = A'_{v_o} = -g_m (r_o \parallel R_c \parallel R_L)$$

$$\therefore v_o = -g_m (r_o \parallel R_c \parallel R_L) \cdot \frac{r_{\pi}}{r_{\pi} + R_s} \cdot v_{in}$$

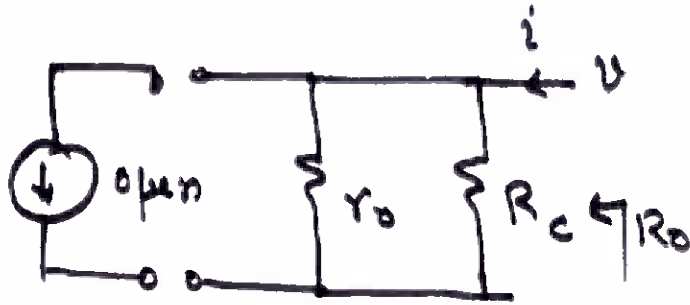
$$\therefore A_v = \frac{v_o}{v_{in}} = \frac{-g_m r_{\pi}}{r_{\pi} + R_s} (r_o \parallel R_c \parallel R_L) = \frac{-\beta (R'_L)}{r_{\pi} + R_s} = \frac{-\beta (Load)}{R_i + R_s} \quad \text{Eq. Ckt}$$



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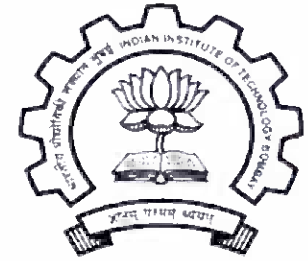
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$$R_o = R_{out}$$



$$R_o = \frac{v}{i}$$

$$\therefore R_o = (r_o \parallel R_c)$$



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