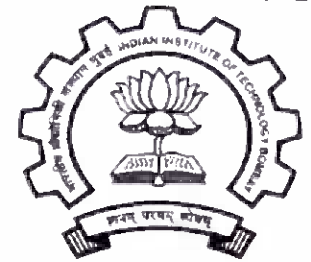
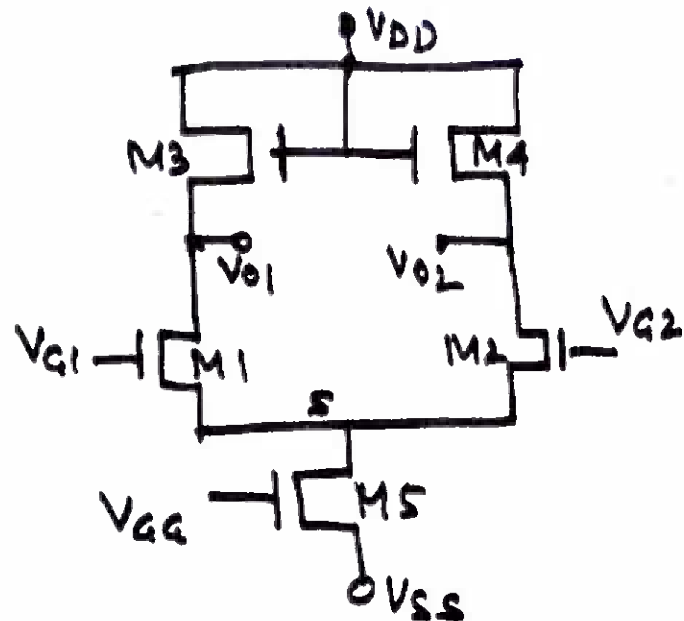


Slide No: 1

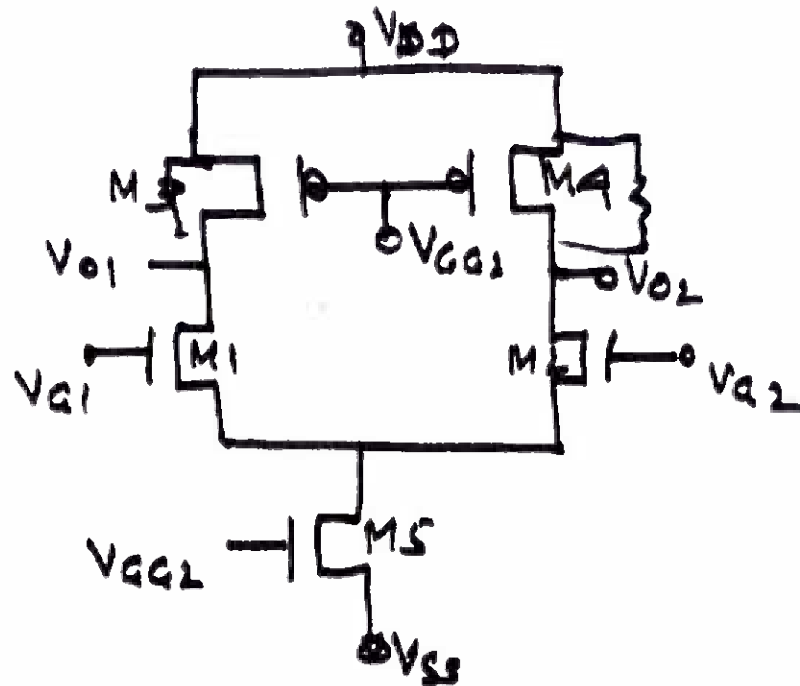
Differential Amplifier with Different Kind of Loads (Active)



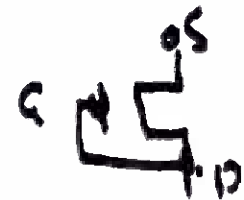
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Normal Active Load



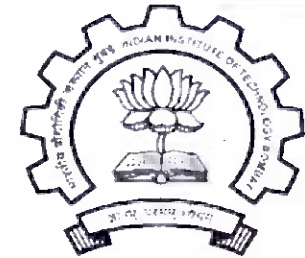
Current Source Load



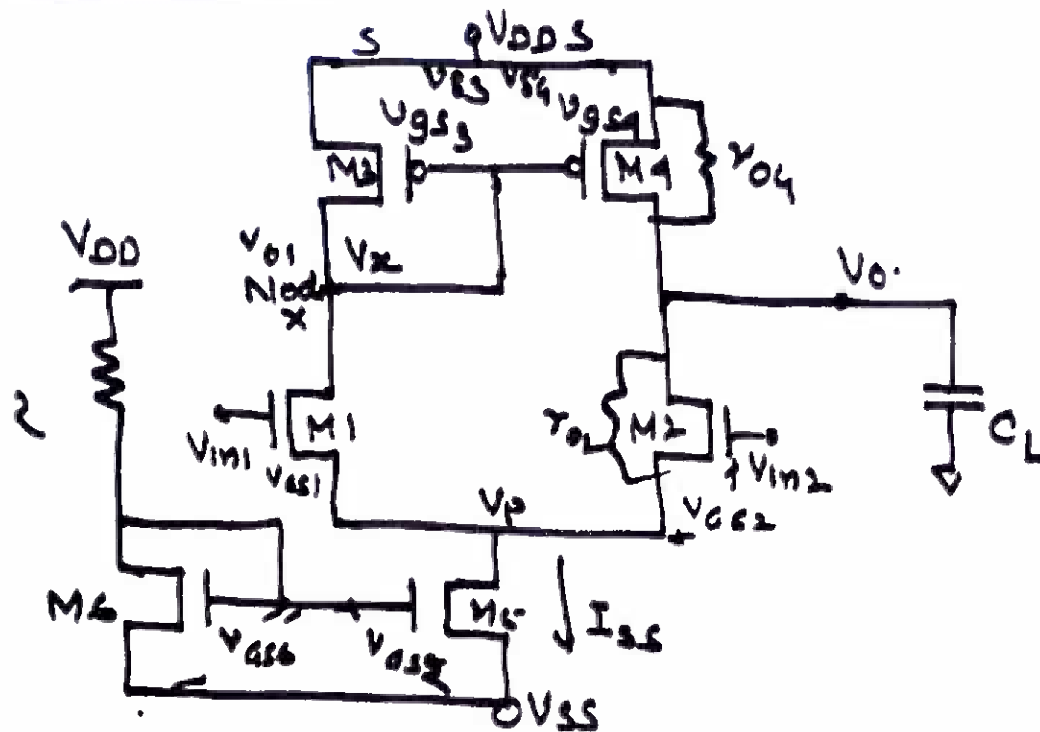
$$Y_{gm} = \downarrow \uparrow \oplus g_m V$$

$$\lambda = \frac{\lambda'}{L}$$

Current Mirror Load CMOS Diffamp



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Due to Mirror Connection between
M3 to M4

$$v_{g13} = v_{g34}$$

$$V_{in1} - V_{in2} = V_{id} = V_{GS1} - V_{GS2}$$

We as usual apply $\frac{V_{id}}{2}$ to Gate of M_1 and $-\frac{V_{id}}{2}$ to the Gate of M_2

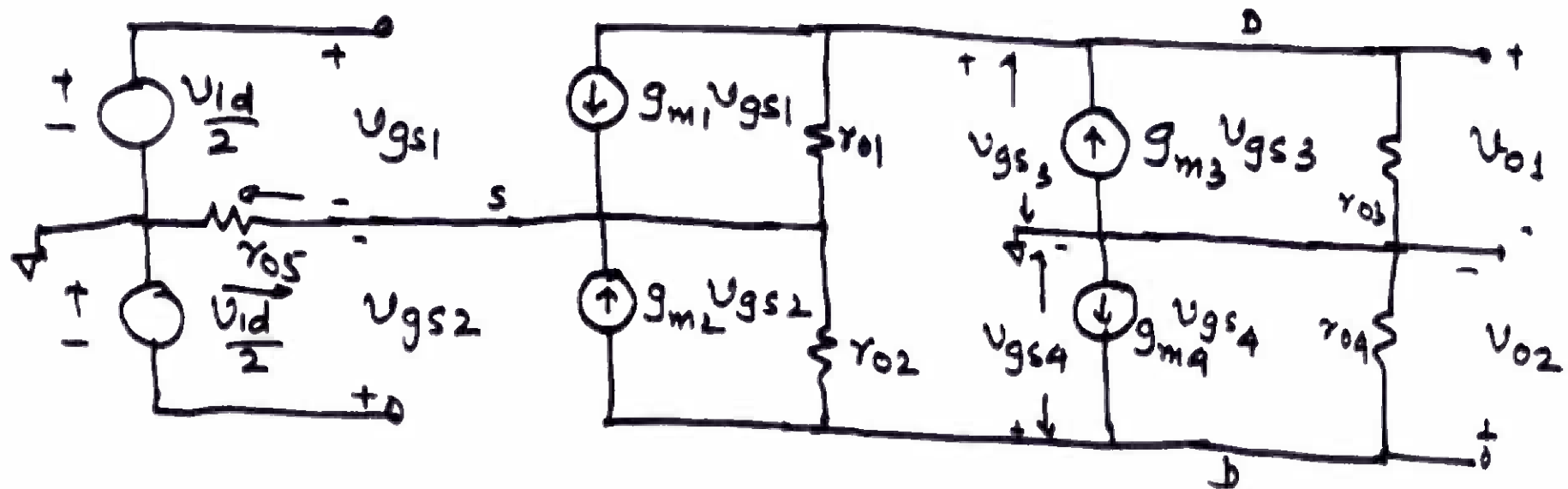
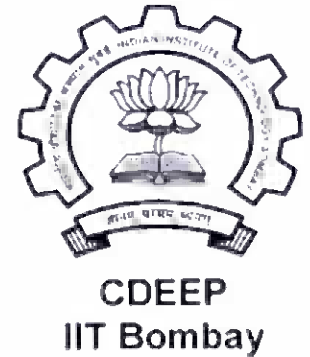
$$V_{GS1} = V_{G1} \quad V_{GS2} = V_{G2}$$

If r_{os} is v. high
Then $V_p \rightarrow 0$ (V_{ss})
for ac.

For the Differential Amplifier with Active load

$$V_{gs1} = -V_{gs2} = V_{gs} = \frac{V_{id}}{2}$$

The Equivalent Ckt is

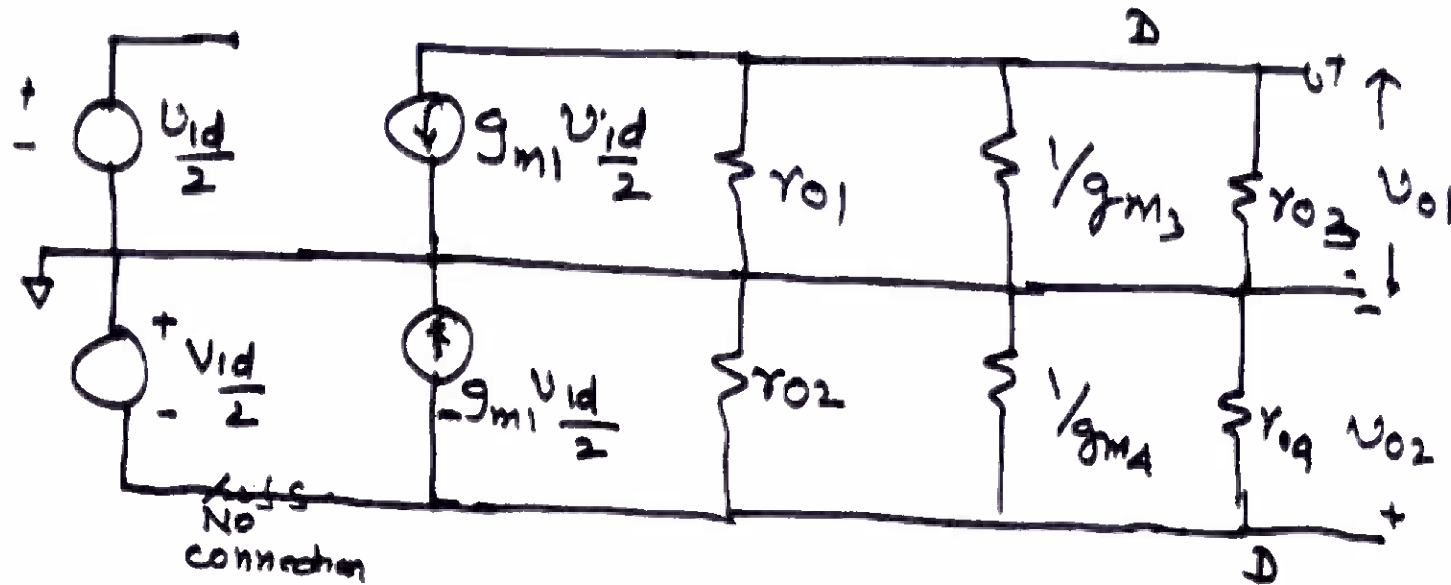


As current through r_{O5} is $g_{m1} \frac{V_{id}}{2}$ & $-g_{m2} \frac{V_{id}}{2}$, we can assume '0' current in r_{O5} (ac current) $\therefore$ terminal S can be treated as Ground.

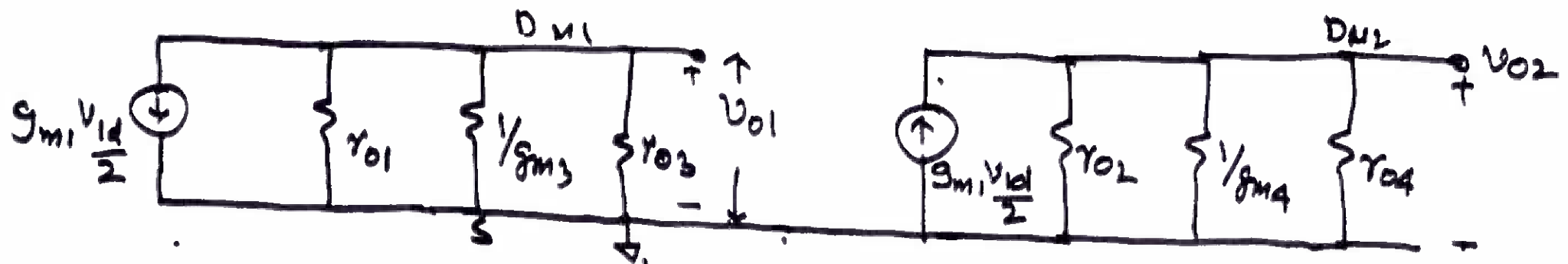
Then the Equivalent circuit reduces to



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Assuming
 $g_{m1} = g_{m2}$



$$v_{id} = v_{id/2} - (+v_{id/2})$$

$$\therefore A_{vd1} = \frac{v_{o1}}{v_{id/2}} = \frac{-g_{m1}}{2(g_{m3} + g_{o1} + g_{o3})}$$

Normally $g_m \gg g_o$

$$\begin{aligned} \therefore A_{vd1} &\approx -\frac{g_{m1}}{2g_{m3}} = -\frac{1}{2} \frac{\sqrt{2\beta_n(\frac{W_1}{L_1}) I_{ss/2}}}{\sqrt{2\beta_n(\frac{W_3}{L_3}) I_{ss/2}}} \quad \left\{ \begin{array}{l} L_1 = L_2 \\ = L_3 \\ = L_4 \end{array} \right. \\ &= -\frac{1}{2} \sqrt{\frac{W_1}{W_3}} \end{aligned}$$

Similarly

$$A_{vd2} \approx +\frac{g_{m1}}{2g_{m3}} = +\frac{1}{2} \sqrt{\frac{W_1}{W_3}} \quad \left\{ \begin{array}{l} g_{m1} = g_{m2} \\ g_{m3} = g_{m4} \end{array} \right.$$

$$\therefore A_{vd} = \frac{v_{o1} - v_{o2}}{v_{id}} = -\frac{g_{m1}}{2g_{m3}} - \frac{g_{m1}}{2g_{m4}} = -\frac{g_{m1}}{g_{m3}} = -\sqrt{\frac{W_1}{W_3}}$$



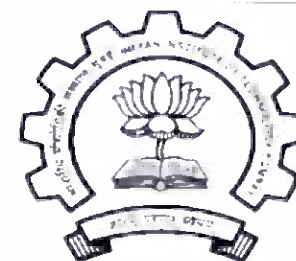
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Output Resistances.

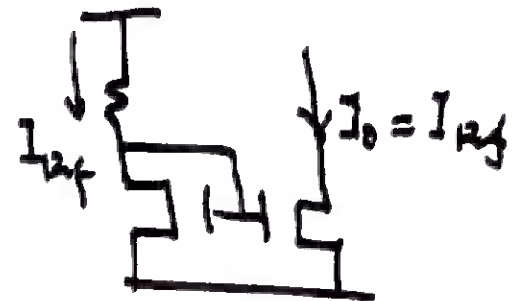
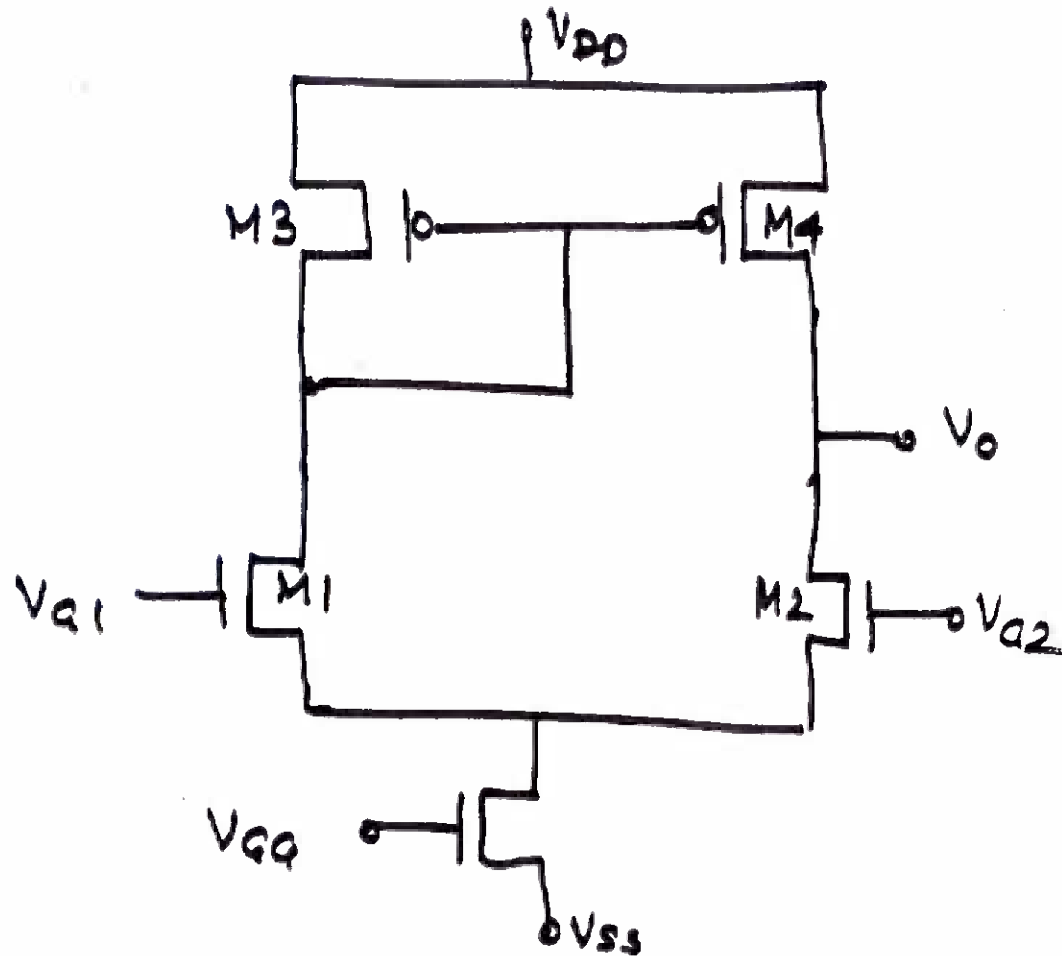
$$R_{O1} = \frac{1}{g_{m3} + g_{o1} + g_{o3}} \approx \frac{1}{g_{m3}}$$

$$R_{O2} = \frac{1}{g_{m4} + g_{o2} + g_{o4}} \approx \frac{1}{g_{m4}}$$

$$\therefore R_{O0} = R_{O1} + R_{O2} = \frac{1}{g_{m3}} + \frac{1}{g_{m4}} = \frac{2}{g_{m3}}$$

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Current Mirror Load



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We see

$$-V_{gs4} = V_{s4} - V_x = V_{s3} - V_x = V_{gs3}$$

However V_x is output V_{o1} due to Diffamp Inputs

$$\therefore V_x = V_{o1} = -g_{m1} \left(\frac{V_{id}}{2} \right) [r_{o1} \parallel r_{o3} \parallel 1/g_{m5}]$$

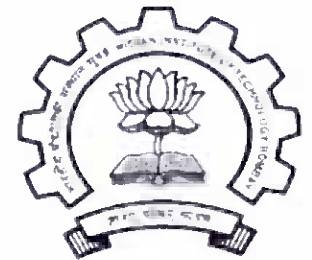
We define $\frac{1}{r_{o13gm}} = \frac{1}{r_{o1}} + \frac{1}{r_{o3}} + g_{m5}$

$$\begin{aligned} \text{Then } V_x = V_{o1} &= -g_{m1} \left(\frac{V_{id}}{2} \right) r_{o13gm} \\ &\equiv -\frac{g_{m1}}{g_{m3}} \left(\frac{V_{id}}{2} \right) \end{aligned}$$

If $r_{o1} \& r_{o3} \gg 1/g_{m5}$
Then $r_{o13gm} = 1/g_{m5}$



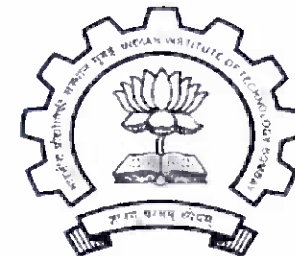
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$$\text{Output Resistance } R_o = r_{o2} \parallel r_{o4}$$

Clearly the Diffamp with Current Mirror Load has following features

1. The Difference Gain $A_{vid} \propto \sqrt{(W/L)_1} + \sqrt{(W/L)_2}$
 $\propto \frac{1}{\sqrt{I_{ss}}}$
 $\propto 1/\lambda$ values of $M2$ & $M4$
 2. The Output Resistance $R_o = r_{o2} \parallel r_{o4} = \frac{1}{g_{o2} + g_{o4}}$
 $= \left(\frac{1}{\lambda_2 + \lambda_4} \right) \cdot \frac{1}{I_{ss}}$
- $\therefore R_o \propto \frac{1}{I_{ss}}$



$$\text{Then } V_o = \left[\frac{g_{m1} g_{m4} V_{id}}{2 g_{m3}} + \frac{g_{m2} V_{id}}{2} \right] r_{o24}$$

$$= \left[\frac{g_{m1} V_{id}}{2} + \frac{g_{m1} V_{id}}{2} \right] r_{o24}$$

$$= \frac{g_{m1} V_{id}}{g_{o2} + g_{o4}}$$

$$\therefore \frac{V_o}{V_{id}} = \frac{g_{m1}}{g_{o2} + g_{o4}} = A_{vdd}$$

$$\text{or } A_{vdd} = \frac{\sqrt{\beta_n' (W/L)_1 I_{SS}}}{(\lambda_2 + \lambda_4) (I_{SS}/2)} = \frac{2 \sqrt{\beta_n' (W/L)_1 / I_{SS}}}{\lambda_2 + \lambda_4}$$

$$\therefore v_{gs4} = -\frac{g_{m1} v_{id}}{2 g_{m3}} - 0$$

Now we see that V_o (Main Output at 2nd node) is governed by inputs at M2 as well as at M4 (v_{gs4}).

$$\begin{aligned} \text{i.e. } V_o &= v_o|_{v_{gs4}} + v_o|_{-v_{id}/2} \text{ (at M2)} \\ &= + \left[-g_{m4} v_{gs4} + g_{m2} \cdot \frac{v_{id}}{2} \right] r_{o24} \end{aligned}$$

$$\frac{1}{r_{o24}} = \frac{1}{r_{o2}} + \frac{1}{r_{o4}}$$

We can make Make M1 & M2 identical, so also M3 & M4 identical
Then $g_{m1} = g_{m2}$, $r_{o1} = r_{o2}$, $g_{m3} = g_{m4}$, $r_{o3} = r_{o4}$



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