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EE 669 L 8 / Slide 1

II<sup>nd</sup> Case :- Limited Source Diffusion

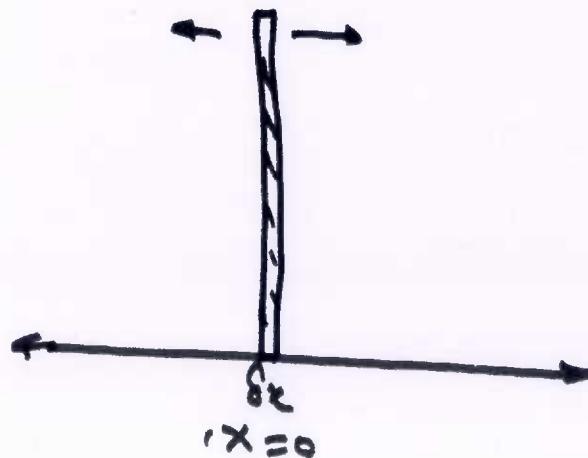
In this case fixed amount of Impurities

reside at the Surface and then Temperature

- Time cycle starts.

From Diffusion Equation we have:

$$\frac{d^2 N(x,s)}{dx^2} - \frac{s N(x,s)}{D} = \frac{N(x, t \leq 0)}{D} \quad \left( = \frac{Q}{s D} \right)$$



Let us have a Sheet charge with DOSE  $Q$  (no/area) as fixed quality and is like a  $\delta$  function at  $x=0$

For this case Initial Cond" is

$$N(x, t \leq 0^-) = Q \cdot \delta$$

We have solution of Diffusion Equation as  
for earlier constant source case as

$$N(x, s) = B(s) \exp \left\{ - \left( \frac{s}{D} \right)^{1/2} x \right\}$$

$$\propto [N(x=0, t \leq 0^-)] = \frac{Q}{s}$$

$$\Rightarrow \therefore N(x, s) = \frac{Q}{\sqrt{s \cdot D}} \exp \left[ - \left( \frac{s}{D} \right)^{1/2} x \right]$$

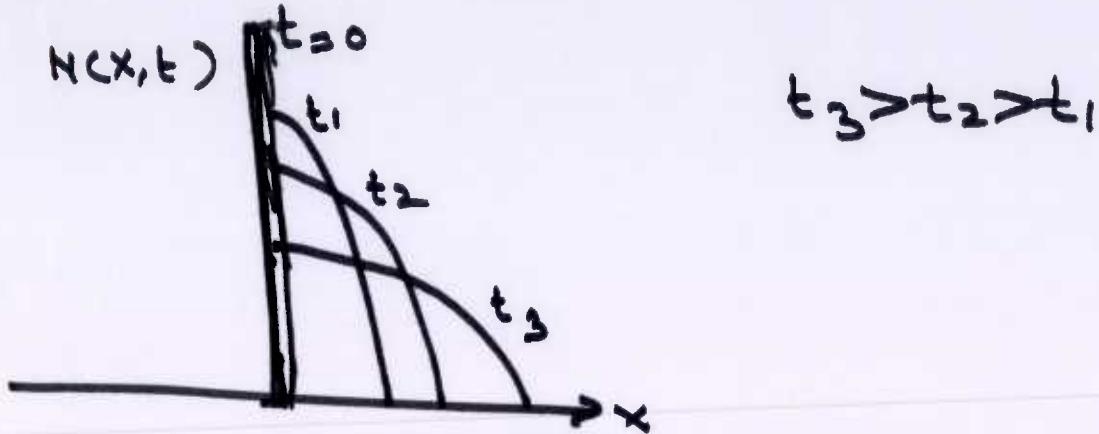
$$N(x, t) = \frac{Q}{\sqrt{\pi D t}} \exp \left( - \frac{x^2}{4 D t} \right)$$

This is essentially a Gaussian Profile



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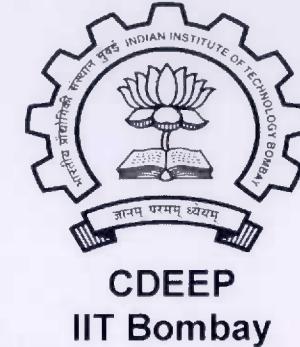
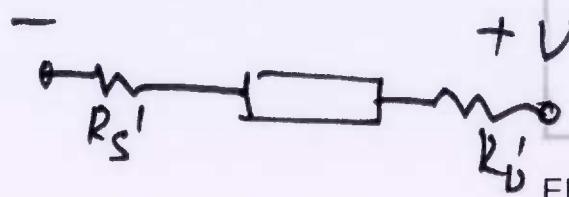
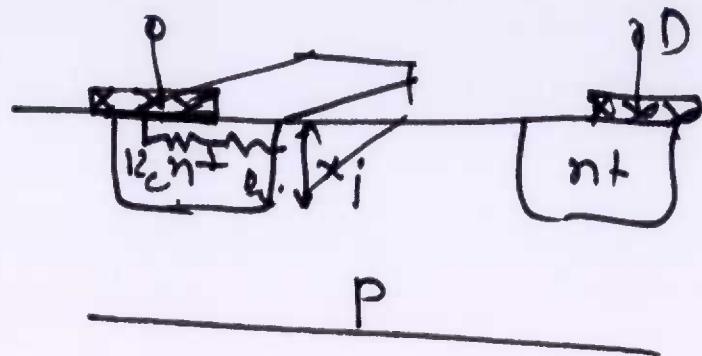
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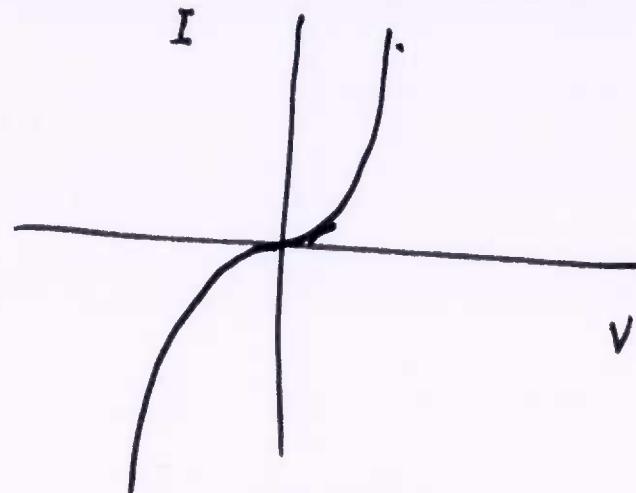
Some interesting points to note :

1. Since Impurity Dose was provided only once, it remains Constant.
2. However subsequent time cycles (at 'A Temperature'), spreads the Impurity Profile as

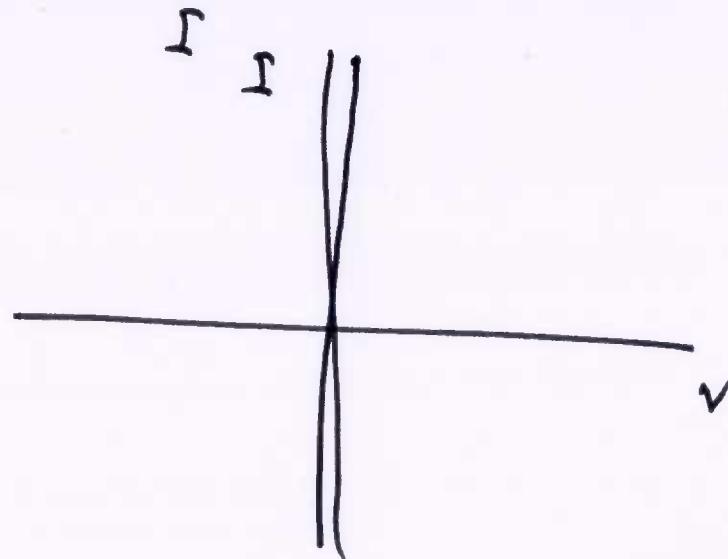
$$\int_0^{\infty} N(x) dx = Q$$



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Schottky  
Diode





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$$\text{Since } N(x,t) = \frac{Q}{\sqrt{\pi D t}} \exp \left[ -\left( \frac{x}{2\sqrt{Dt}} \right)^2 \right]$$

We conclude that  $\sqrt{Dt}$  Function decides  $N(x,t)$

Next we took erfc profile again.

Evaluation of Dose of Impurities in Constant Source Diffusion case

$$\text{In this case } N(x,t) = N_0 \operatorname{erfc} \left( \frac{x}{2\sqrt{Dt}} \right)$$

$$\text{We define } y = \frac{x}{2\sqrt{Dt}} \quad \therefore \quad \frac{dy}{dx} = \frac{1}{2\sqrt{Dt}}$$

From Fick's First Law

$$j(x,t) = -D \frac{\partial N}{\partial x}$$

At the surface ( $x=0$ ) Flux density is

$$j(0, t) = -D \frac{\partial N}{\partial x} \Big|_{x=0}$$

From erfc profile we get

$$\begin{aligned} \frac{\partial N}{\partial x} \Big|_{x=0} &= N_0 \frac{d}{dx} \left[ \operatorname{erfc} \left( \frac{x}{2\sqrt{Dt}} \right) \right] \\ &= N_0 \cdot \frac{d}{dy} [\operatorname{erfc}(y)] \cdot \frac{1}{2\sqrt{Dt}} \\ &= \frac{N_0}{2\sqrt{Dt}} \frac{d}{dy} (1 - \operatorname{erf}(y)) \\ &= -\frac{N_0}{2\sqrt{Dt}} \frac{d}{dy} [\operatorname{erf}(y)] \\ &= -\frac{N_0}{2\sqrt{Dt}} \cdot \frac{2}{\sqrt{\pi}} \cdot \exp(-y^2) \end{aligned}$$



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$$\frac{d}{dx} = \frac{d}{dy} \cdot \frac{dy}{dx}$$

$$\gamma J(0,t) = + \frac{N_0 D}{\sqrt{\pi t}} \exp(-y^2) \Big|_{y=0}$$

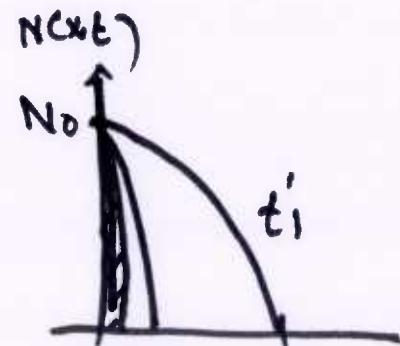
$$= + N_0 \sqrt{\frac{D}{\pi t}}$$

$$\text{Now Dose } Q = \int_0^{t_1} [J(0,t)] dt$$

where  $t_1$  is the time for diffusion at temperature  $T_1$ . At  $T_1$ ,  $D = D(T_1) = D_1$

$$\therefore Q_{T_1, t_1} = N_0 \sqrt{\frac{D_1}{\pi}} \left[ \int_0^{t_1} e^{-\frac{y^2}{2D_1 t}} dt \right]$$

$$= 2 N_0 \sqrt{\frac{D_1 t_1}{\pi}}$$

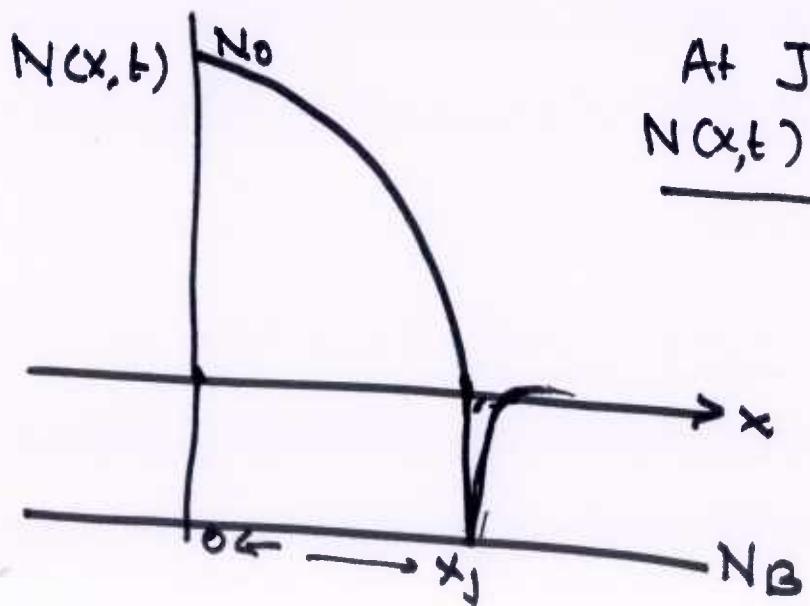
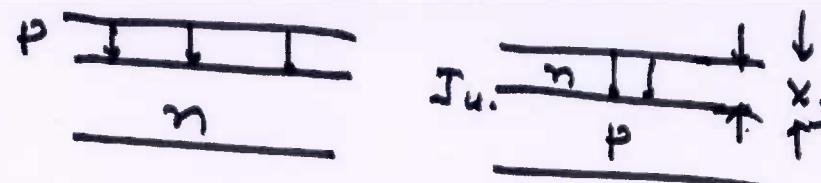
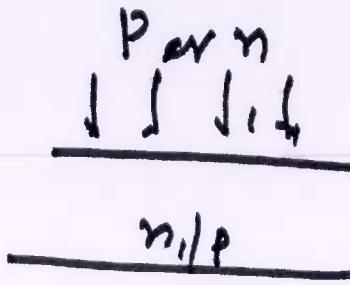


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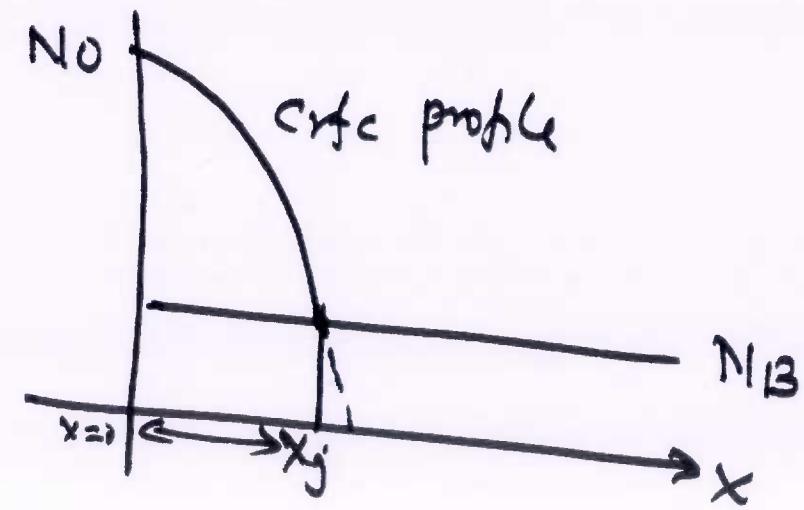
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# Junction Formation:

Starting Substrate has base concentration as  $N_B$ .  
It is one type of Semiconductor ( $n$  or  $p$ ).



At Junction  
 $N(x,t) - N_B = 0$





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Let us take an exple of Diffusion of n-type of Impurities in p-type Substrate with conc.  $N_B$ . As n-type impurities enter p - wafer, electron conc. Increases near surface and reduces as Profile shows.

At  $x = x_j$ , n-type dopants = p-type doping (Compensation)

For Constant Source Diffusion

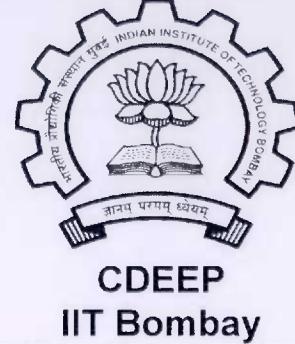
$$N(x, t) = N_0 \operatorname{erfc} \left( \frac{x}{2\sqrt{Dt}} \right)$$

If Diffusion is performed at Temperature  $T_1$ , then

$D(T_1) = D_1$  and  $t = t_1$ , time of diffusion.

$$\therefore Q(T_1, t_1) = 2N_0 \sqrt{\frac{D_1 t_1}{\pi}}$$

At Junction, net conc. is zero. Hence  
we say incoming impurity conc is exactly  
same as  $N_B$



$$\therefore N(x_j, t_i) = N_B$$

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$$\text{or } N_0 \operatorname{erfc} \left( \frac{x_j}{2\sqrt{D_i t_i}} \right) = N_B$$

$$\text{or } x_j = 2\sqrt{D_i t_i} \operatorname{erfc}^{-1} \left( \frac{N_B}{N_0} \right)$$

In specific case,  $T_i = 1000^\circ\text{C}$  and Diffusion of Phosphorous takes place in p-doped wafer with conc  $N_B = 5 \times 10^{15}/\text{cc}$  for total time of 60 minutes (3600 seconds)

$$\begin{aligned} \text{At } T = T_i : - \\ N_0 &= 3 \times 10^{20}/\text{cc} \quad \text{for Phosphorous} \\ D_i &= 3 \times 10^{14} \text{ cm}^2/\text{sec} \end{aligned}$$

$$\therefore \sqrt{D_1 t_1} = \sqrt{3 \times 10^{-14} \times 3600} = 1.04 \times 10^{-5} \text{ cm}$$

$$\begin{aligned} \text{Further } \operatorname{erfc}^{-1}\left(\frac{N_B}{N_0}\right) &= \operatorname{erfc}^{-1}\left(\frac{5 \times 10^{15}}{3 \times 10^{20}}\right) \\ &= \operatorname{erfc}^{-1}(1.66 \times 10^{-5}) = z \end{aligned}$$

$$\text{As } \operatorname{erfc}(x) = 1 - \operatorname{erf}(x)$$

$$\therefore x_j = 2\sqrt{D_1 t_1} \cdot 3.06$$

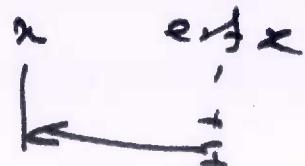
$$x_j = 2 \times 1.04 \times 10^{-5} \times 3.06$$

$$\text{or } x_j = 0.636 \mu\text{m}$$

~~$$\text{Let us say } x = 1.66 \times 10^{-5}$$~~

$$\begin{aligned} \text{Let us define } \operatorname{erfc} x &= 1.66 \times 10^{-5} \\ \text{or } \operatorname{erf} x &= 1 - 1.66 \times 10^{-5} \\ &= 0.999984 \end{aligned}$$

$$\begin{aligned} \therefore x &= \operatorname{erf}^{-1}(0.999984) \\ &= 3.06 \end{aligned}$$



In Practice , the Diffusion of Impurities  
is a Two-Step Process

(i) Predeposition (ii) Drive-In

(i) Predeposition :

Here we perform Constant Source diffusion at Temperature  $T_1$  for time  $t_1$ ,

$$\therefore D_1 = D_1(T_1), N_{01} = N_0(T_1)$$

$$\therefore N(x, t_1) = N_{01} \operatorname{erfc} \left( \frac{x}{2\sqrt{D_1 t_1}} \right)$$

And after time  $t_1$ , the dose of impurities  $Q(t_1)$   
at Surface =  $2 N_{01} \sqrt{\frac{D_1 t_1}{\pi}}$



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(ii) After Predeposition step, source of impurities are stopped. Then the wafers are reintroduced in the furnace at Temperature  $T_2$  for time  $t_2$  this process is continued. This process is called Drive-In.

$$\text{At } T_2, D_2(T_2) = D_2, \therefore D_t = D_2 t_2$$

In Drive-In, no new impurities are introduced, but available ones from Predeposition are Re-distributed (Q dose). This is the case of Limited Source Diffusion giving Gaussian Profile:

$$N(x, t_1, t_2) = \frac{Q}{\sqrt{\pi D_2 t_2}} \exp\left(-\frac{x^2}{4 D_2 t_2}\right)$$

$$\propto N(x, t_1, t_2) = \frac{2 N_{01}}{\pi} \sqrt{\frac{D_1 t_1}{D_2 t_2}} \exp\left(-\frac{x^2}{4 D_2 t_2}\right)$$

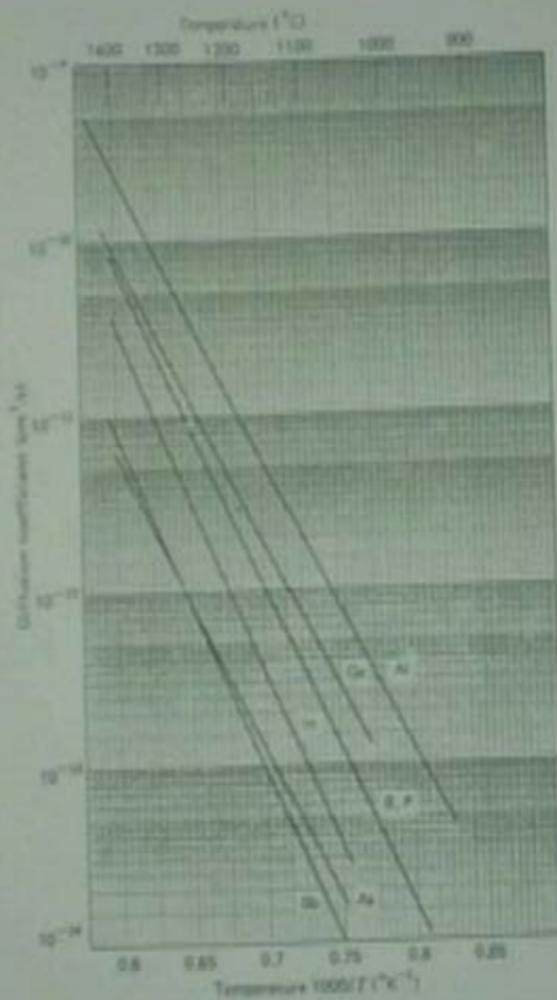


Fig. 4.7 Average diffusion coefficients for substitutional diffusants in silicon.

formed. This experimental technique essentially duplicates the fabrication process used in integrated circuit technology. Consequently, the results are reasonably accurate.

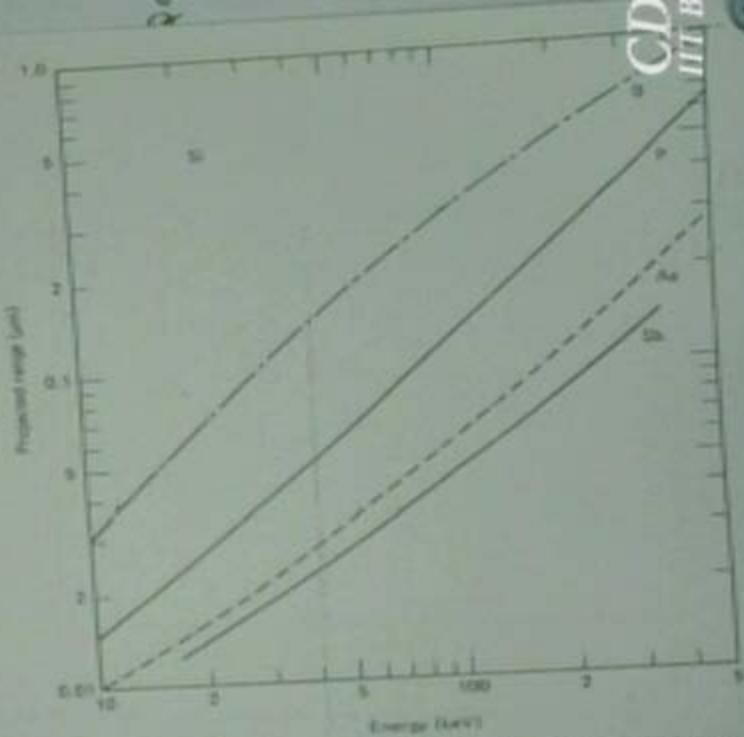
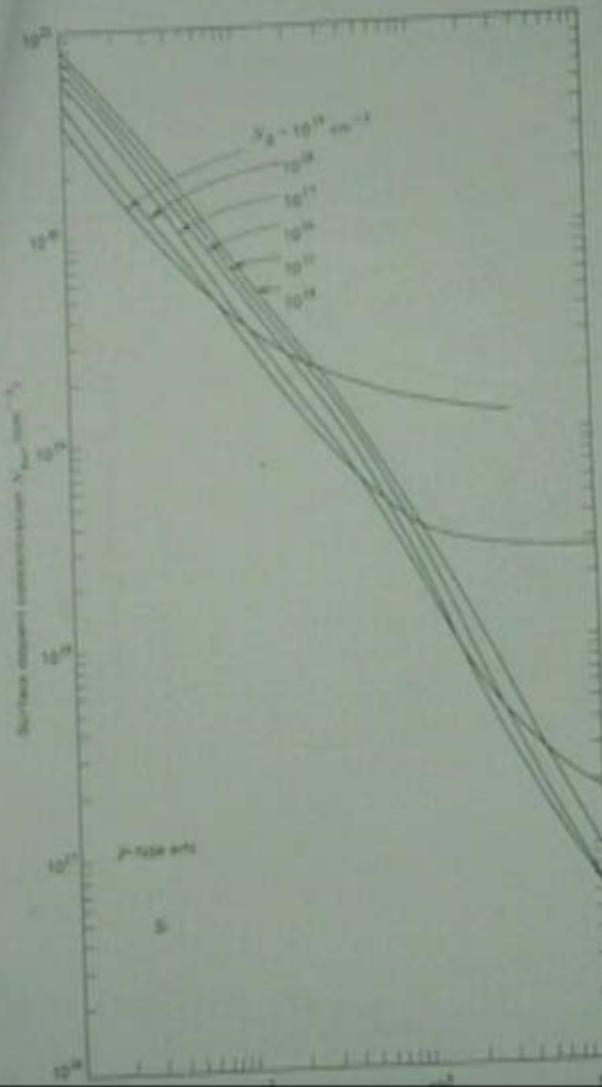
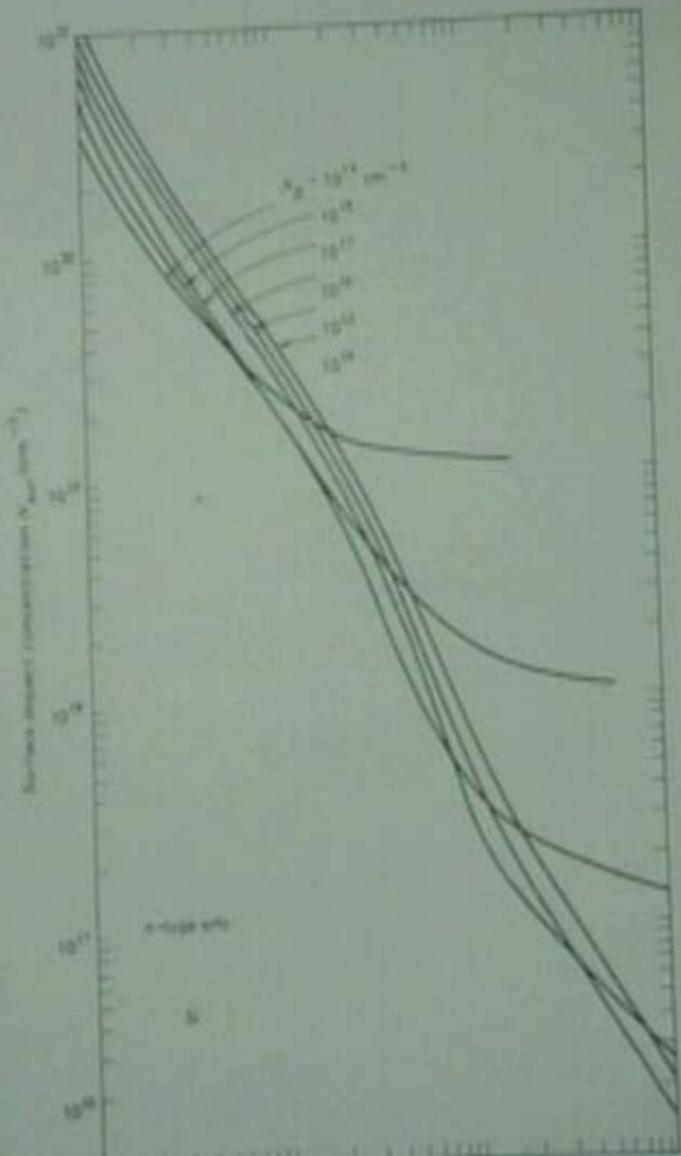


Fig. 6.12 Projected range of boron, phosphorus, arsenic, and antimony  
Adapted from Gibbons, Johnson, and Myroffe [9].





C  
III

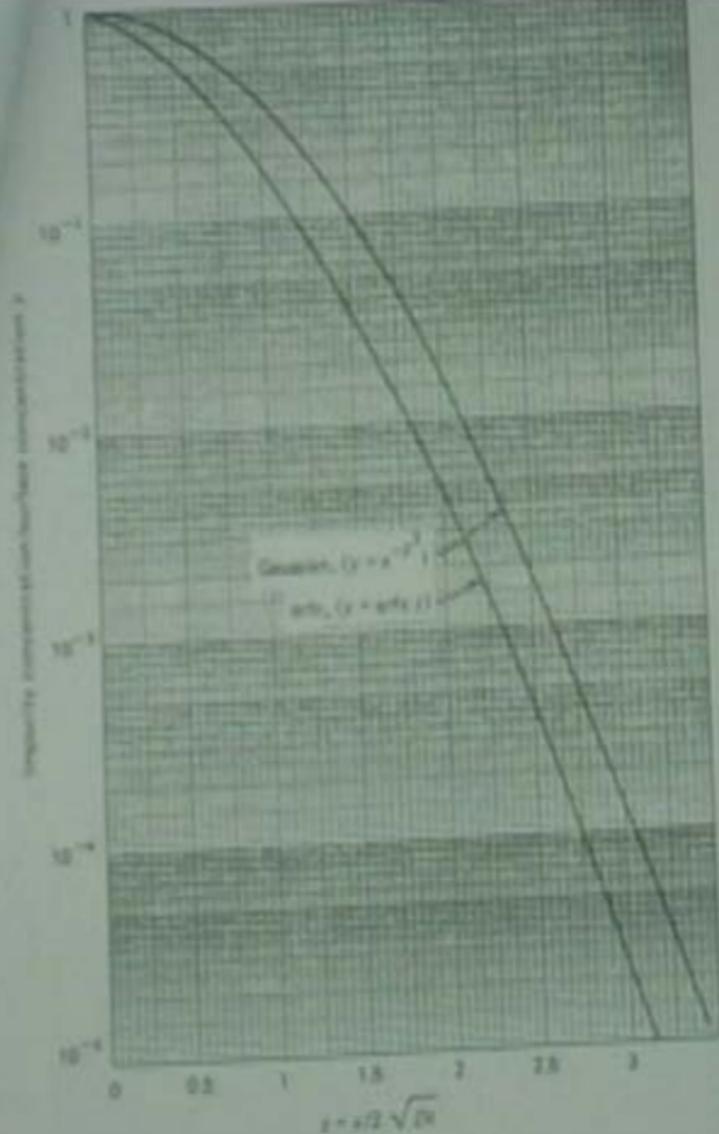


Fig. 4.17. The arctan and gaussian profiles.

#### 4.5.1.2 Diffusion from a Limited Source

Here a finite quantity of the diffusing matter is first placed on the wafer, and it is assumed that all of

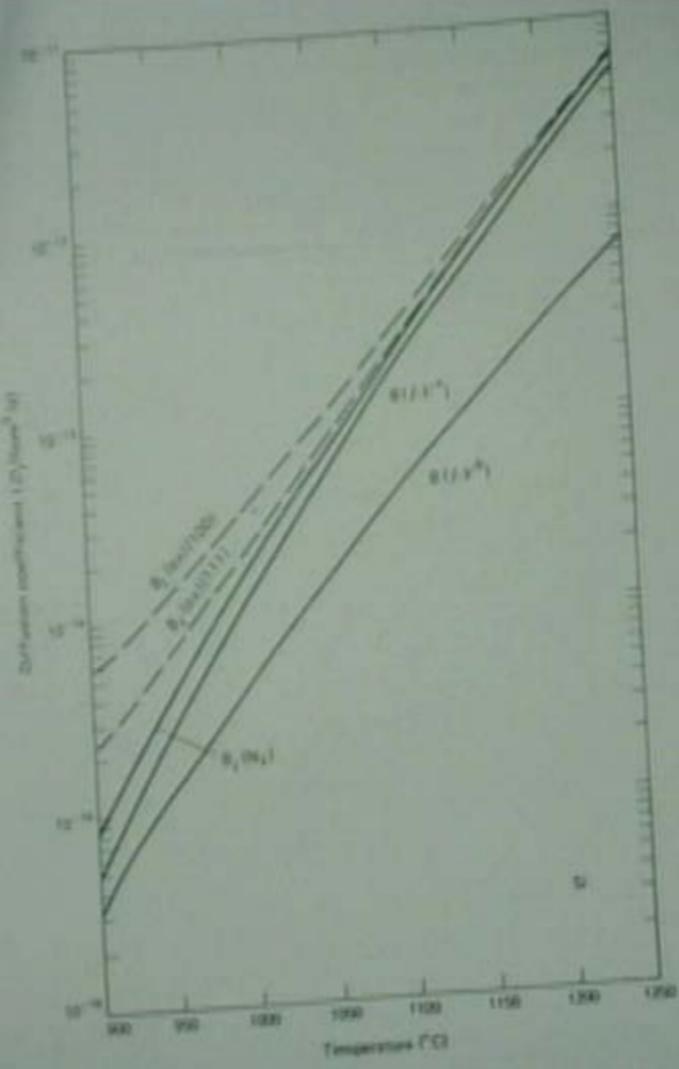


Fig. 4.4. Diffusivities of boron in silicon. From R. Chikazawa, Microelectronic Processing, © 1990, p. 103. Reprinted by permission of the publisher, John Wiley & Sons, Inc.

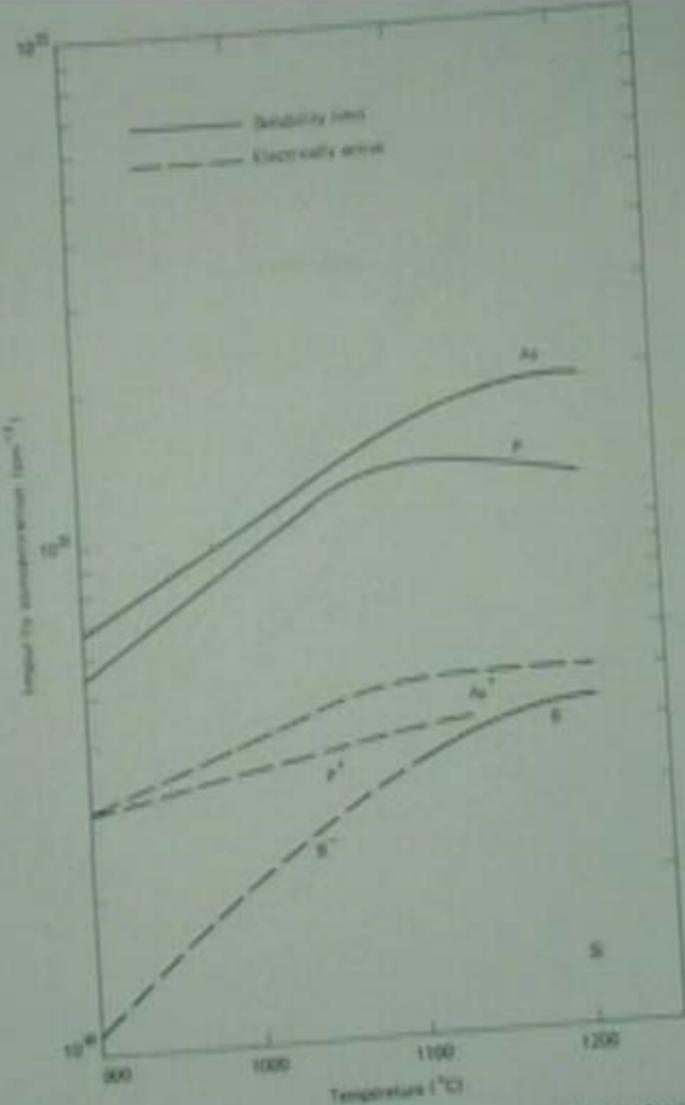


Fig. 4.11 Solubility limits for boron, arsenic, and phosphorus. From R. Colaković, *Micromaterials: Processing and Device Design* [10], 1988. Reprinted with permission of the publisher, John Wiley & Sons.

Table A.1 Error Function erf z\*

<i>t</i>	erf(t)	<i>t</i>	erf(t)	<i>t</i>	erf(t)	<i>t</i>	erf(t)
0.00	0.000 000	0.10	0.120 500	0.20	0.447 700	0.30	0.966 105
0.01	0.001 233	0.11	0.129 244	0.21	0.449 410	0.31	0.961 277
0.02	0.002 565	0.12	0.137 899	0.22	0.450 838	0.32	0.958 413
0.03	0.003 894	0.13	0.146 464	0.23	0.451 784	0.33	0.955 516
0.04	0.005 111	0.14	0.154 939	0.24	0.452 650	0.34	0.952 588
0.05	0.006 322	0.15	0.163 323	0.25	0.453 436	0.35	0.951 623
0.06	0.007 522	0.16	0.171 618	0.26	0.454 144	0.36	0.951 429
0.07	0.008 719	0.17	0.179 818	0.27	0.454 773	0.37	0.951 463
0.08	0.009 898	0.18	0.187 923	0.28	0.455 326	0.38	0.951 347
0.09	0.011 067	0.19	0.195 938	0.29	0.455 803	0.39	0.951 462
0.10	0.012 223	0.20	0.203 863	0.30	0.456 298	0.40	0.951 348
0.11	0.013 367	0.21	0.211 693	0.31	0.456 713	0.41	0.951 297
0.12	0.014 502	0.22	0.219 431	0.32	0.456 788	0.42	0.951 038
0.13	0.014 632	0.23	0.227 076	0.33	0.456 971	0.43	0.951 043
0.14	0.015 757	0.24	0.234 586	0.34	0.456 982	0.44	0.951 427
0.15	0.016 876	0.25	0.242 029	0.35	0.456 124	0.45	0.951 376
0.16	0.017 987	0.26	0.249 377	0.36	0.456 096	0.46	0.951 107
0.17	0.018 992	0.27	0.256 628	0.37	0.456 080	0.47	0.951 413
0.18	0.020 000	0.28	0.263 782	0.38	0.455 837	0.48	0.951 491
0.19	0.021 000	0.29	0.270 840	0.39	0.455 608	0.49	0.951 257
0.20	0.022 703	0.30	0.277 801	0.40	0.455 318	0.50	0.951 795
0.21	0.023 307	0.31	0.284 666	0.41	0.455 056	0.51	0.951 607
0.22	0.024 798	0.32	0.291 433	0.42	0.454 534	0.52	0.951 502
0.23	0.025 623	0.33	0.298 104	0.43	0.454 059	0.53	0.951 578
0.24	0.026 760	0.34	0.304 678	0.44	0.453 595	0.54	0.951 175
0.25	0.027 736	0.35	0.311 156	0.45	0.453 090	0.55	0.951 672
0.26	0.028 600	0.36	0.317 537	0.46	0.452 528	0.56	0.951 196
0.27	0.029 478	0.37	0.323 823	0.47	0.452 514	0.57	0.951 691
0.28	0.030 340	0.38	0.329 018	0.48	0.452 734	0.58	0.951 374
0.29	0.031 203	0.39	0.334 103	0.49	0.451 899	0.59	0.951 647
0.30	0.032 067	0.40	0.347 101	0.50	0.451 068	0.60	0.951 095
0.31	0.033 938	0.41	0.354 065	0.51	0.450 983	0.61	0.951 323
0.32	0.034 726	0.42	0.359 913	0.52	0.450 940	0.62	0.951 543
0.33	0.035 527	0.43	0.374 524	0.53	0.449 913	0.63	0.951 347
0.34	0.036 302	0.44	0.379 143	0.54	0.448 914	0.64	0.950 736
0.35	0.037 982	0.45	0.379 648	0.55	0.447 782	0.65	0.951 113
0.36	0.038 139	0.46	0.379 100	0.56	0.447 584	0.66	0.951 472
0.37	0.039 296	0.47	0.381 446	0.57	0.447 312	0.67	0.951 823
0.38	0.040 009	0.48	0.383 687	0.58	0.447 016	0.68	0.952 126
0.39	0.041 729	0.49	0.385 843	0.59	0.446 671	0.69	0.952 476
0.40	0.042 342	0.50	0.386 968	0.60	0.446 323	0.70	0.952 796
0.41	0.043 762	0.51	0.388 383	0.61	0.445 453	0.71	0.953 016
0.42	0.044 468	0.52	0.389 564	0.62	0.445 129	0.72	0.953 335
0.43	0.045 087	0.53	0.391 564	0.63	0.444 795	0.73	0.953 654