

In an Integrated Circuit fabrication, many films of different materials are deposited.



CDEEP
IIT Bombay

EE669 Slide 01
L-24

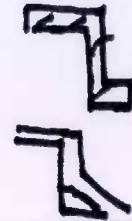
These films are of either Metals, Metal-silicides, and Dielectrics like SiO_2 , Si_3N_4 .

Requirements of Deposition

- i Desired Composition, Low Contaminates
- ii Good Electrical properties of films (Desired)
- iii Mechanical Properties should also be good.
Adhesion is one such important Property

iv Uniform thickness across Wafer and
• Run to Run.

v. Most important requirement is
Good Step Coverage



CDEEP
IIT Bombay

EE669 / Slide L-24 02

vi If 'Interconnect' is desired from metal films,
then they should give very low Resistance/length.

vii Better Electromigration resistance



viii Non - Corrosive

ix Economical

x Compatible to other processes in IC fabrication.

$$J_c \geq 10^5 \text{ Am/cm}^2$$

Two Major Deposition Techniques :

1. Physical Vapour Deposition (PVD)

(a) Evaporation

(b) Sputtering

2. Chemical Vapour Deposition (CVD)

a. At. Pressure CVD (APCVD)

b. Low Pressure CVD (LPCVD)

c. Plasma Enhanced CVD (PECVD)

d. Hot-Wire CVD (HWCVD)



CDEEP
IIT Bombay

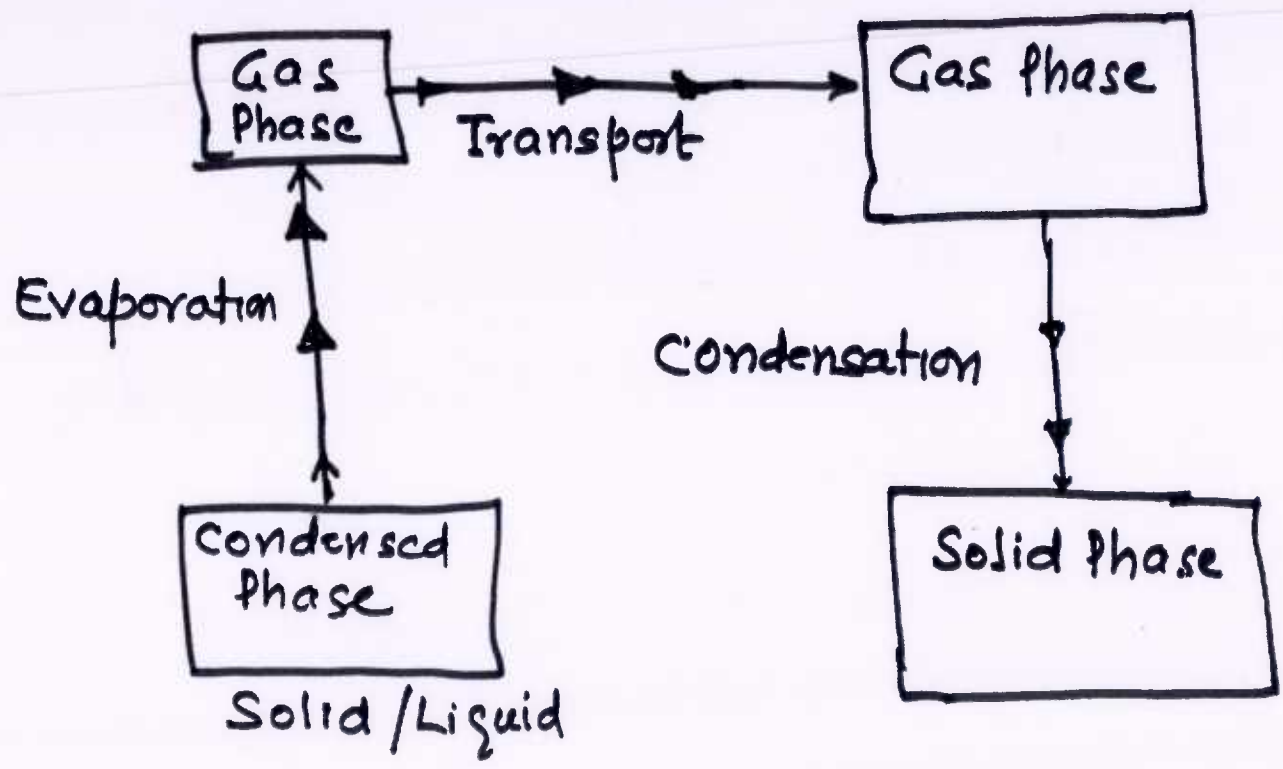
EE 669 / Slide L-24-03



CDEEP
IIT Bombay

EE669 / Slide 24 - 5-04

Typical PVD process looks like
a Four Step Process



Evaporation System Requirement



CDEEP
IIT Bombay

1. Vacuum :

- Need 10^{-6} torr or better vacuum for better quality films.

- Better vacuum be Ultra High Vacuum which could be around 10^{-9} torr.

EEEGG/ Slide 05
L-24

2. Heating System

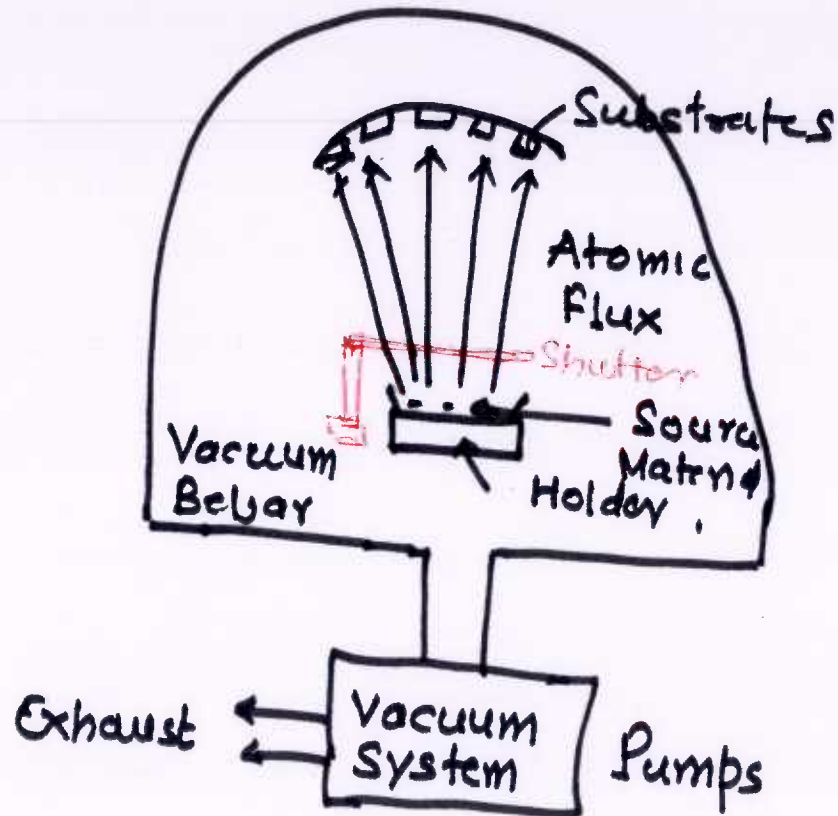
}	Thermal Heating] 1-10 kW Power
	Electron-Beam related	

3. A Bell-Jar to keep vacuum.

4. Thickness Monitor

5. Mechanical Shutter System

Control on evaporating flux reaching substrate



CDEEP
IIT Bombay

EE669 / Slide 06
L-24

Modeling of Evaporation:

- (i) We define p^* as Partial Pressure of a gas in equilibrium with its Condensed Phase at a given Temperature T .

EE669 / Slide 07
L-24

Generally p^* is only function of Temperature (T).

- (ii) p is defined as ambient hydrostatic pressure acting upon evaporant in Condensed State

According to Hertz principle, the evaporation rate is $\propto (p^* - p)$

In vacuum, p is closed to zero



CDEEP
IIT Bombay

ciii) V_g and V_c are volume of evaporant in Gas Phase and Condensed Phase respectively.

(iv) If we define ΔH_e as enthalpy-change from one phase going to the, other, then

according to Clausius Clapeyron Equation

$$\frac{dp^*}{dT} \propto \frac{\Delta H_e}{T(V_g - V_c)} \approx \frac{\Delta H_e}{T V_g}$$

(Normally $V_g \gg V_c$)

By Ideal Gas Laws

$$p^* V_g = RT$$

where R is Universal Gas Constant



CDEEP
IIT Bombay

CE669 Slide 08
L-24

Clausius - Clapeyron Equation



CDEEP
IIT Bombay

EE 669 L 24 / Slide 09
L-24

$$\therefore \frac{dp^*}{p^*} = \frac{\Delta H_e}{RT^2} dT$$

$$\text{or } \ln p^* = - \frac{\Delta H_e}{RT} + c^*$$

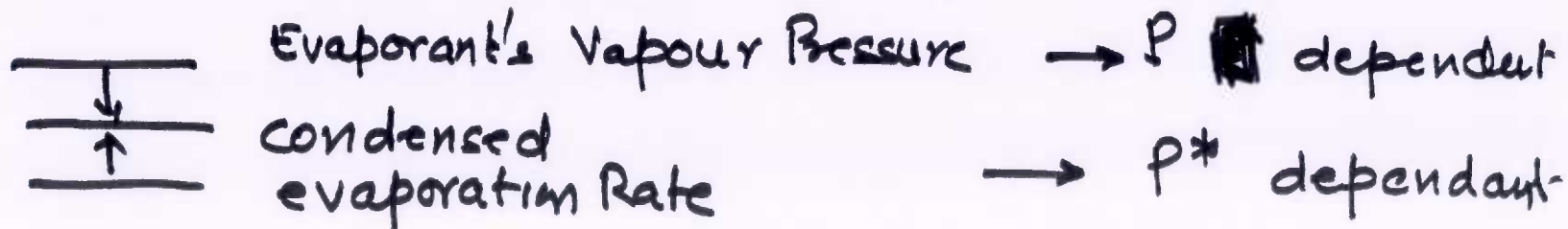
let $c^* = \ln C_1$

$$\therefore p^* = C_1 e^{-\Delta H_e/RT}$$

Clearly p^* is only function of Temperature T

(V) Evaporation Rate R_{ev}

We have two Fluxes:



If A is cross-section area of flux coming out of evaporator, then

$$\frac{1}{A} \frac{dN_e}{dt} = \frac{1}{(2\pi m kT)^{1/2}} (P^* - P)$$

where $\frac{1}{A} \frac{dN_e}{dt}$ represents net Evaporation Rate

$$\text{or } R_{ev} = \frac{1}{A} \frac{dN_e}{dt} = \frac{1}{(2\pi m kT)^{1/2}} (P^* - P)$$

Hertz - Knudsen equation for R_{ev} also takes care of return flux which is decided by α_v called Sticking Coeff for vapour molecules on the surface and thus is written as



CDEEP
IIT Bombay

EE 669 L24 / Slide 10

$$R_{ev} = \frac{1}{A} \frac{dN_e}{dt} = \alpha_v (2\pi m k T)^{-1/2} (P^* - P)$$

In vacuum, two things are affected

ci) P the pressure due to return flux

could be closed to $\rightarrow 0$ (Zero). Knudsen cell can ensure this.

Δ ci) The mean free path of evaporant atoms increases i.e.

$$\lambda = \frac{kT}{\sqrt{2} \pi \sigma^2 P}$$

Clearly better vacuum means higher mean free path.

Higher Mean Free Path means, unlikely events of collision between evaporant atoms \Rightarrow Unidirectional Flow.

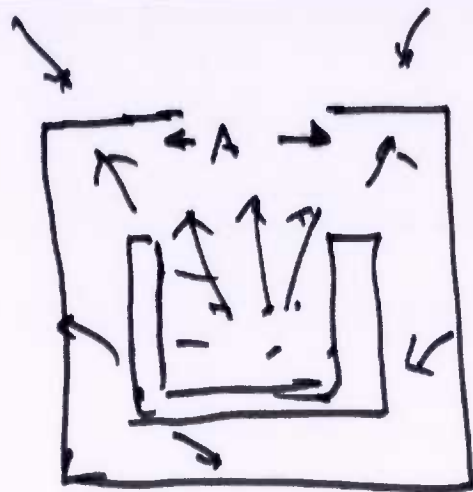


CDEEP
IIT Bombay

EE 669 L 24 / Slide 11

$$\therefore R_{ev} = \frac{\alpha_v p^*}{\sqrt{2\pi m k T}}$$

In Knudsen Cell, we can make $\alpha_v = 1$



$$\text{Then } R_{ev} = \frac{p^*}{\sqrt{2\pi m k T}}$$

Then the Film Growth Rate

$$F_{GR} = \frac{R_{ev} \rho m}{\rho} \quad \rho \text{ is density}$$

$$= \sqrt{\frac{m}{2\pi k T}} \frac{p^*}{\rho} = 5.83 \times 10^{-3} A \left(\frac{m}{T}\right)^{1/2} p^*$$

$$\Rightarrow \text{cm/sec.}$$

Here 'A' is area.



CDEEP
IIT Bombay

EE 669 L24 / Slide 12

Evaporation process starts from first melting of the evaporant substance and with increase of Temperature, vapour pressure increases, and evaporation of the substance starts.



CDEEP
IIT Bombay

EE 669 L24 / Slide 13

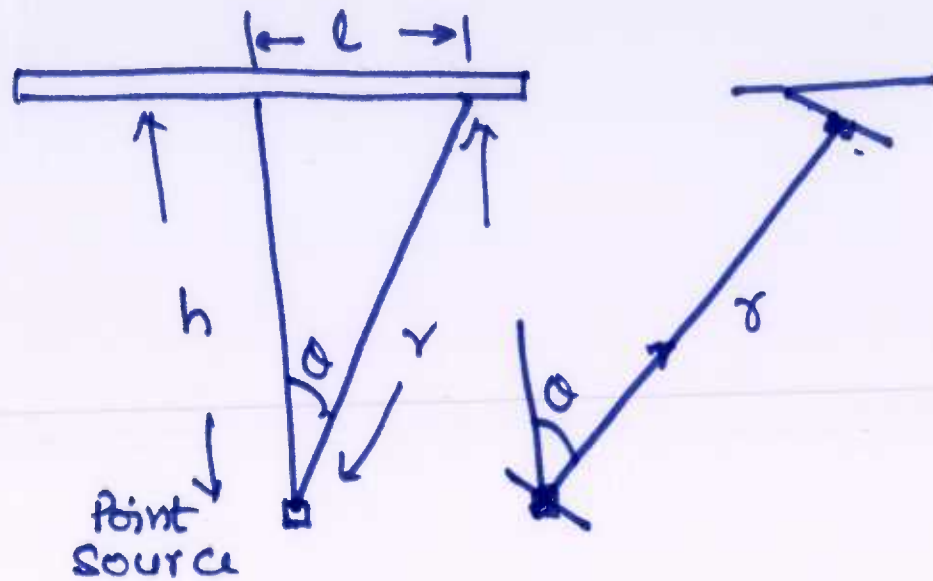
Source of evaporation could be either a Point Source or a 'small area' source.

Assuming Point source, we wish to find deposition rate along plane of the target (substrate on which evaporated film deposits)



CDEEP
IIT Bombay

EE 669 L 24 / Slide 14



Let Ω is the solid angle over which source emits, ρ is the density of evaporant substance and h , r and l are vertical, radius of curvature (solid \curvearrowleft) and horizontal distance between vertical position on the target to the point which subtends an angle θ at source.

If vacuum is better ($< 10^{-6}$ torr), then mean free path is good no. like 100 cm.

Since distance between source & target, vertically is around 30 cm (max.) [$h \approx 30$ cm], we can assume flux transport reaching target with scattering and at low pressure, return flux from target can also be treated v.v. small.

In this case $\Omega = 2\pi$

Then Flux reaching \angle vertical core = $F = \frac{R_{evp}}{2\pi r^2}$

$$\therefore \text{Growth rate} = \frac{R_{evp}}{2\pi r^2} \frac{m}{\rho}$$

From geometric consideration $h^2 + l^2 = r^2$

$$\text{and } \cos \theta = \frac{h}{r}$$



CDEEP
IIT Bombay

EE 669 L 24 / Slide 15

Growth rate at point 'l' from vertical point on substrate is

$$= \frac{R_{evp} \cdot m}{2\pi r^2 \rho} \cos\theta$$

since $h^2 + l^2 = r^2 \quad \therefore r = \sqrt{h^2 + l^2}$

We have $\cos\theta = \frac{h}{r}$ and $\frac{\cos\theta}{r^2} = \frac{h}{r^3}$

$$\therefore \frac{\cos\theta}{r^3} = \frac{h}{(h^2 + l^2)^{3/2}}$$

$$\text{Film Growth rate} = \frac{R_{evp} \cdot m}{2\pi \rho} \frac{h}{(h^2 + l^2)^{3/2}}$$



CDEEP
IIT Bombay

EE 669 L 24 / Slide 16

Evaporation Sources :

- i Resistance Heated
- ii E-beam heated

(i) Usually heating source is made out of wires filaments of Tungsten, Tantalum or Molybdom filaments.

Current needed to reach 1800°C temperature in filament is generally of order of 200-300 Amp

Typical deposition rate around $1-25 \text{ \AA} / \text{min}$.

Materials which can be evaporated by this technique are : Al, Sn, Cr, Sb, Ge, In, Au, Ag, Mg etc and CdS, PbS, CdSe, NaCl, KCl, MgF_2 , CaF_2 etc



CDEEP
IIT Bombay

EE 669 L 24 / Slide 17

Typical Resistance Heated filaments

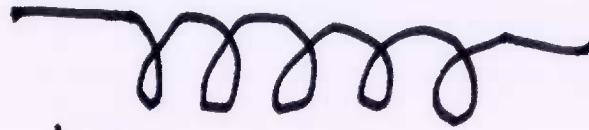


CDEEP
IIT Bombay

EE 669 L 24 / Slide 18



Hairpin

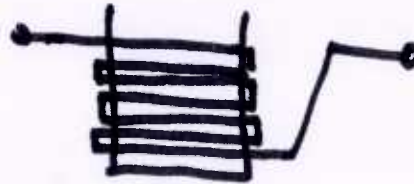


Wire helix



Basket

BN



Crucible