



Jet Aircraft Propulsion

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Lect-6

In this lecture...

- Brayton cycles
 - Ideal Brayton cycle
 - Variants of Brayton cycle
 - Actual/real Brayton cycle

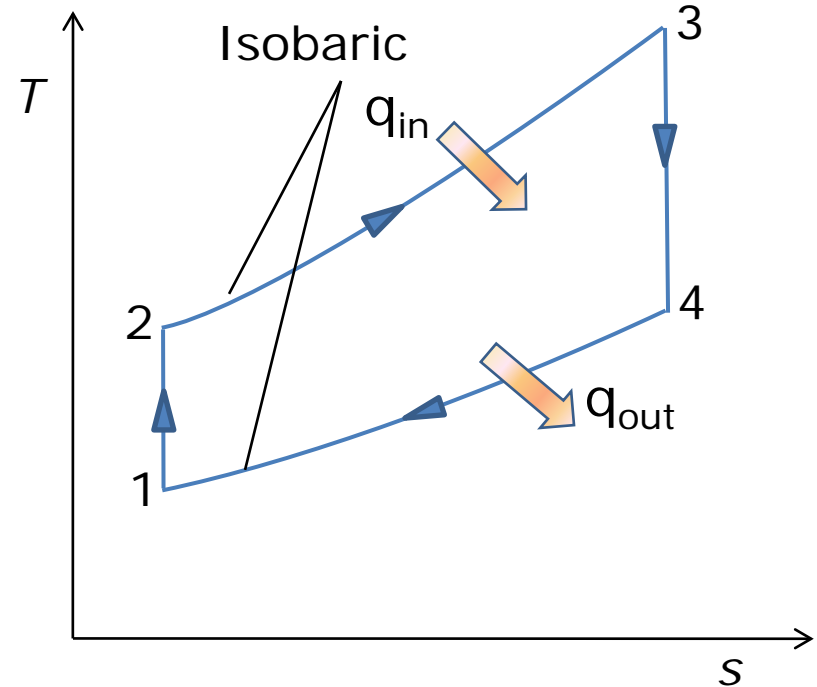
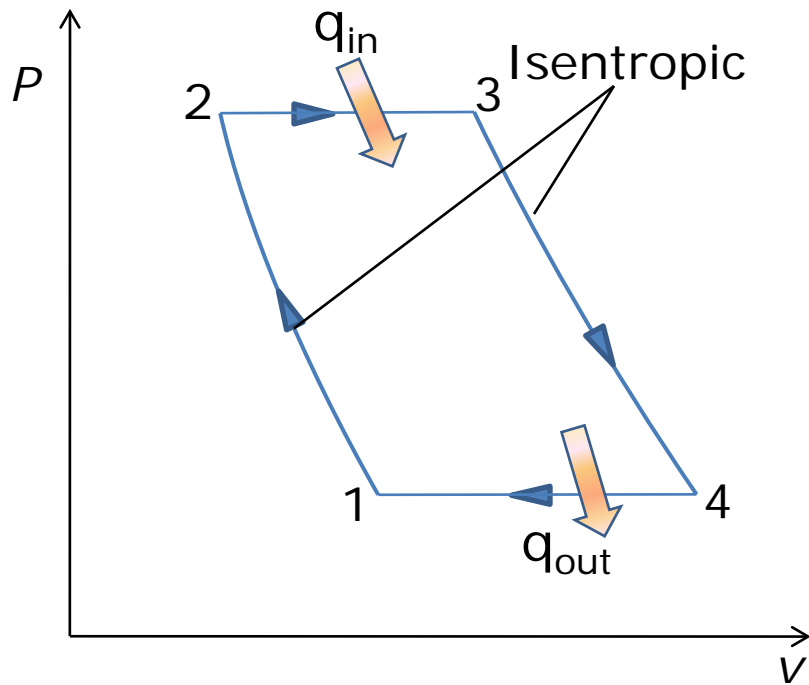
Brayton cycle

- The Brayton cycle was proposed by George Brayton in 1870 for use in reciprocating engines.
- Modern day gas turbines operate on Brayton cycle and work with rotating machinery.
- Gas turbines operate in open-cycle mode, but can be modelled as closed cycle using air-standard assumptions.
- Combustion and exhaust replaced by constant pressure heat addition and rejection.

Ideal Brayton cycle

- The Brayton cycle consists of four internally reversible processes:
 - 1-2 Isentropic compression (in a compressor)
 - 2-3 Constant-pressure heat addition
 - 3-4 Isentropic expansion (in a turbine)
 - 4-1 Constant-pressure heat rejection

Ideal Brayton cycle



Brayton cycle on $P-v$ and $T-s$ diagrams

Ideal Brayton cycle

- The energy balance for a steady-flow process can be expressed as:

$$(q_{in} - q_{out}) + (w_{in} - w_{out}) = \Delta h$$

The heat transfer to and from the working fluid can be written as :

$$q_{in} = h_3 - h_2 = c_p (T_3 - T_2)$$

$$q_{out} = h_4 - h_1 = c_p (T_4 - T_1)$$

Ideal Brayton cycle

- The thermal efficiency of the ideal Brayton cycle under the cold air standard assumptions becomes:

$$\eta_{th,Brayton} = \frac{W_{net}}{q_{in}} = 1 - \frac{q_{out}}{q_{in}} = 1 - \frac{T_4 - T_1}{T_3 - T_2} = 1 - \frac{T_1(T_4 / T_1 - 1)}{T_2(T_3 / T_2 - 1)}$$

Processes 1 - 2 and 3 - 4 are isentropic and

$$P_2 = P_3 \text{ and } P_4 = P_1.$$

$$\text{Therefore, } \frac{T_2}{T_1} = \left(\frac{P_2}{P_1} \right)^{(\gamma-1)/\gamma} = \left(\frac{P_3}{P_4} \right)^{(\gamma-1)/\gamma} = \frac{T_3}{T_4}$$

Ideal Brayton cycle

- Substituting these equations into the thermal efficiency relation and simplifying:

$$\eta_{th,Brayton} = 1 - \frac{1}{r_p^{(\gamma-1)/\gamma}}$$

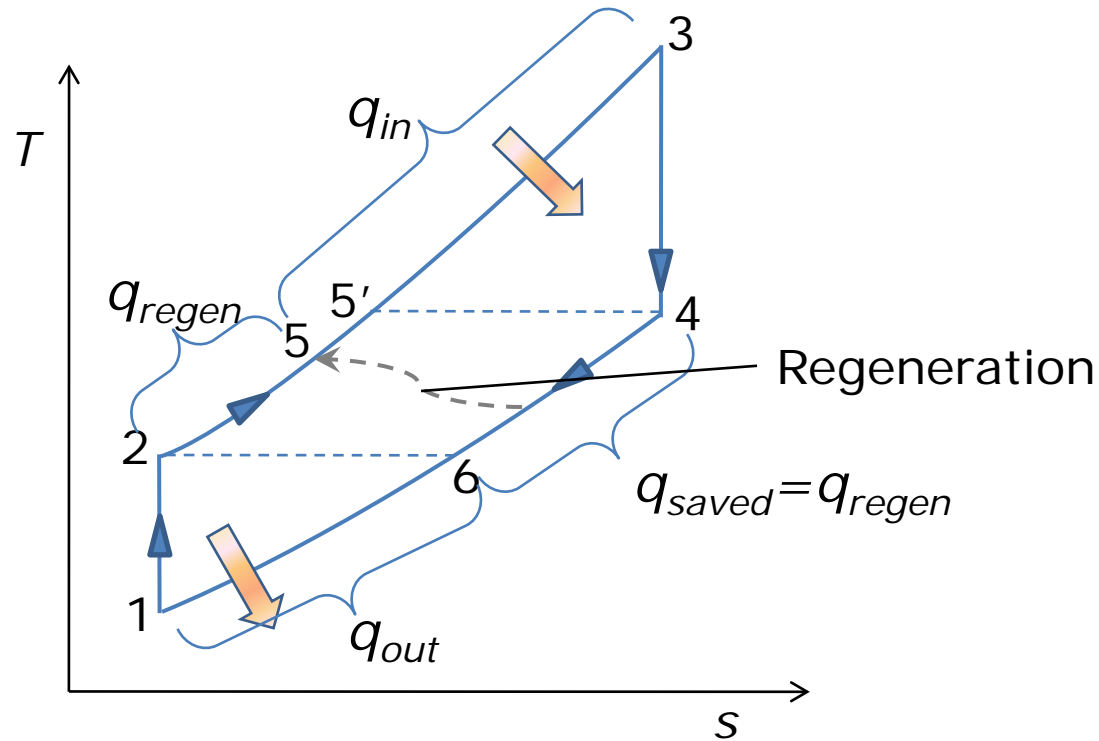
where, $r_p = \frac{P_2}{P_1}$ is the pressure ratio.

- The thermal efficiency of a Brayton cycle is therefore a function of the cycle pressure ratio and the ratio of specific heats.

Ideal Brayton cycle with regeneration

- Regeneration can be carried out by using the hot air exhausting from the turbine to heat up the compressor exit flow.
- The thermal efficiency of the Brayton cycle increases as a part of the heat rejected is re-used.
- Regeneration decreases the heat input (thus fuel) requirements for the same net work output.

Ideal Brayton cycle with regeneration



T-s diagram of a Brayton cycle with regeneration

Ideal Brayton cycle with regeneration

- The extent to which a regenerator approaches an ideal regenerator is called the **effectiveness, ϵ** and is defined as

$$\epsilon = q_{regen,act} / q_{regen,max} = (h_5 - h_2) / (h_4 - h_2)$$

- Under the cold-air-standard assumptions, the thermal efficiency of an ideal Brayton cycle with regeneration is:

$$\eta_{th,regen} = 1 - \left(\frac{T_1}{T_3} \right) (r_p)^{(\gamma-1)/\gamma}$$

- The thermal efficiency depends upon the temperature as well as the pressure ratio.

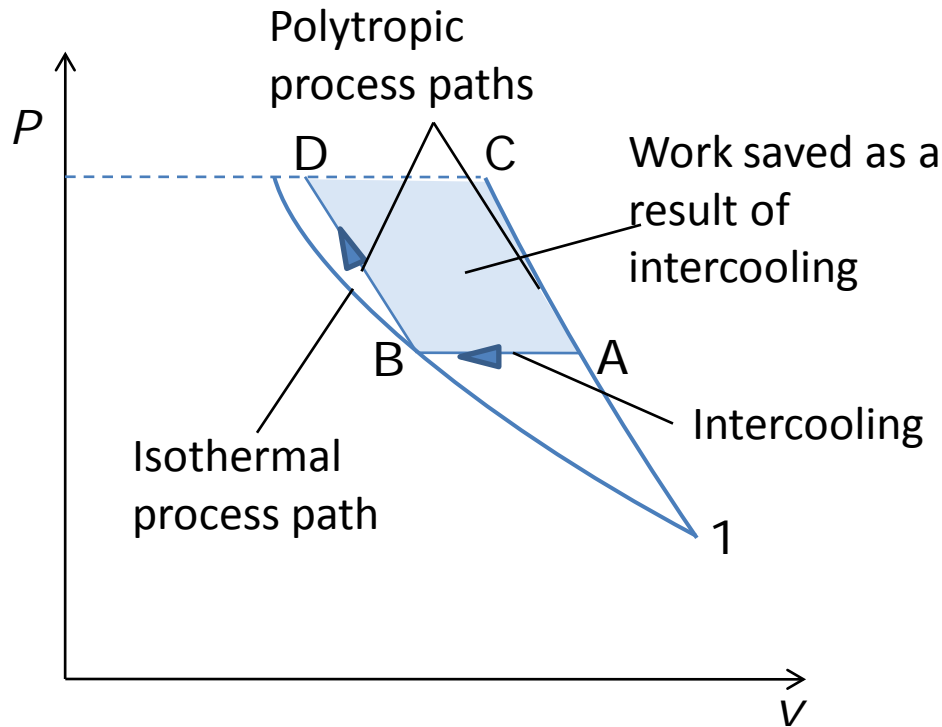
Ideal Brayton cycle with intercooling, reheating and regeneration

- The net work of a gas-turbine cycle is the difference between the turbine work output and the compressor work input.
- It can be increased by either decreasing the compressor work or increasing the turbine work, or both.
- The work required to compress a gas between two specified pressures can be decreased by carrying out the compression process in stages and cooling the gas in between: **multi-stage compression with intercooling.**

Ideal Brayton cycle with intercooling, reheating and regeneration

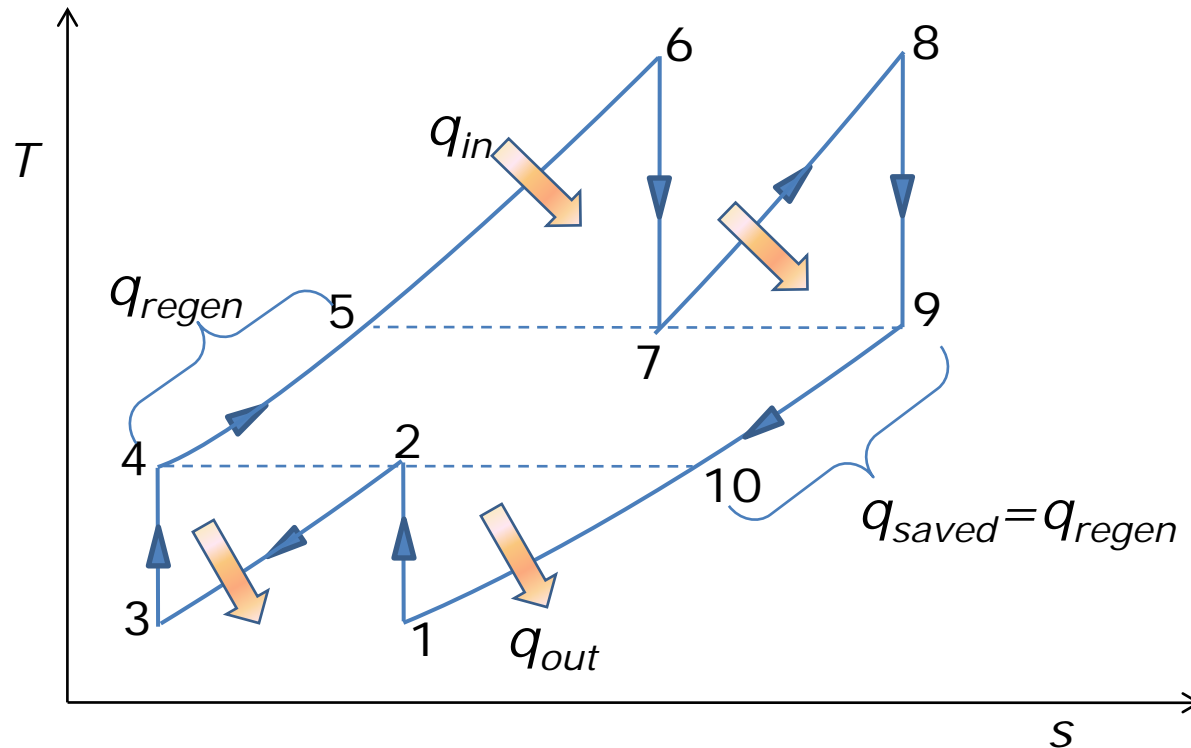
- Similarly the work output of a turbine can be increased by: **multi-stage expansion with reheating**.
- As the number of stages of compression and expansion are increased, the process approaches an isothermal process.
- A combination of intercooling and reheating can increase the net work output of a Brayton cycle significantly.

Ideal Brayton cycle with intercooling, reheating and regeneration



Work inputs to a single-stage compressor (process: $1AC$) and a two-stage compressor with intercooling (process: $1ABD$).

Ideal Brayton cycle with intercooling, reheating and regeneration

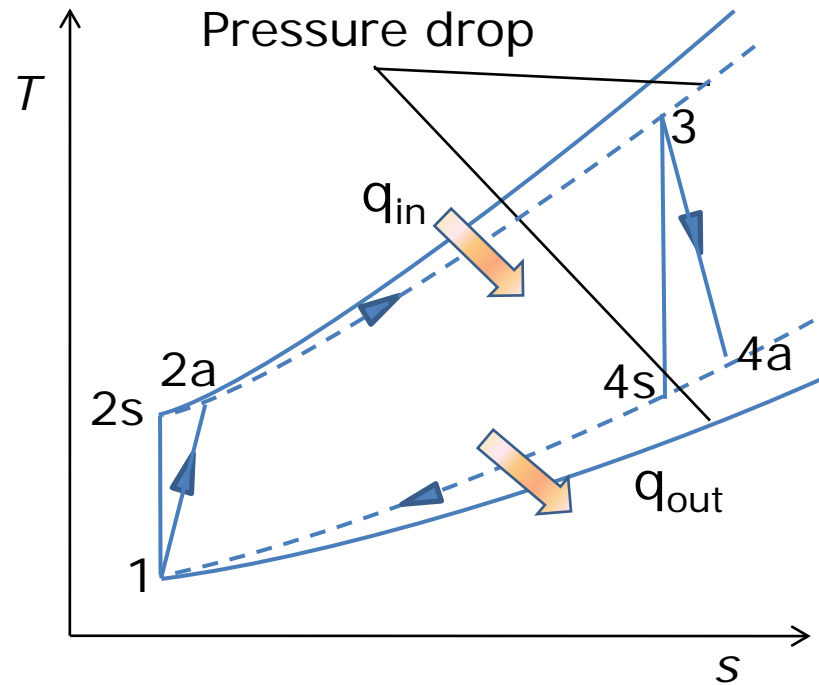


T-s diagram of an ideal gas-turbine cycle with intercooling, reheating, and regeneration

Actual/Real Brayton cycle

- Actual Brayton cycles differ from the ideal cycles in all the four processes.
- The compression process and expansion processes are non-isentropic.
- Pressure drop during heat addition and heat rejection.
- The presence of irreversibilities causes the above deviations.

Actual/Real Brayton cycle



Actual Brayton cycle $T-s$ diagram

Actual/Real Brayton cycle

- The deviation of actual compressors and turbines from the isentropic versions can be accounted for by using the isentropic efficiencies.

$$\eta_C = \frac{\text{Isentropic work}}{\text{Actual work}} \cong \frac{h_{2s} - h_1}{h_{2a} - h_1}$$

$$\eta_T = \frac{\text{Actual work}}{\text{Isentropic work}} \cong \frac{h_3 - h_{4a}}{h_3 - h_{4s}}$$

- Where, $2a$ and $4a$ are the actual states at the compressor and turbine exit and $2s$ and $4s$ are the corresponding isentropic states.

Actual/Real Brayton cycle

- As a result of non-isentropic compression and expansion, the compressor needs more work than the ideal cycle and turbine generates less work.
- Isentropic efficiencies reflect the amount of deviation of the actual compression/expansion processes from the ideal.
- Total pressure losses in the heat addition/rejection processes also need to be considered.

Actual/Real Brayton cycle

- Other differences between ideal and actual Brayton cycles
 - Change of specific heats with temperature
 - Heat exchanger effectiveness (in case of regenerative cycles)
 - Mass flow rate of fuel
 - Combustion efficiency
- These parameters are often used in actual cycle analysis.

Actual/Real Brayton cycle

- Variants of the simple Brayton cycle
 - Reheating
 - Intercooling
 - Regeneration
- Actual cycles with the above will be different from the ideal cycles in terms of the irreversibilities present.
- Isentropic efficiencies, total pressure losses, heat exchanger effectiveness for each additional components of the cycle.

Actual/Real Brayton cycle

- Actual Brayton cycle with intercooling
 - Isentropic efficiencies of each stage of intercooling
 - Heat exchanger effectiveness of the intercooling duct
- Actual Brayton cycle with reheating
 - Isentropic efficiencies of each stage of reheating
 - Total pressure loss and combustion efficiency during reheating

Actual/Real Brayton cycle

- Actual Brayton cycle with regeneration
 - Heat exchanger effectiveness
- Actual Brayton cycle with all three of these modifications need to be analysed considering the above discussed irreversibilities.

In this lecture...

- Brayton cycles
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In the next lecture...

- Jet engine cycles for aircraft propulsion
 - Turbojet engine
 - Turbojet engine with afterburning
 - Turbofan and its variants
 - Turboprop and turboshaft engines