

EE 5500 – Introduction to Photonics

Quiz II

60 minutes, 20 points, closed book

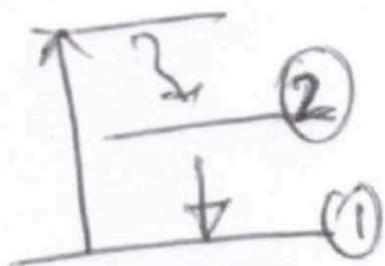
Remember...

- Make reasonable assumptions wherever necessary, but you should show all steps and justify assumptions for full credit. Use of figures may attract bonus points.
- Final answers will be graded ONLY if they are entered in the space provided.

Objective Type Questions (5 points)

1. Which of these is/are (maybe more than one) necessary condition(s) for laser operation?

- (a) Gain > loss (b) $N_2 > N_1$ (c) long T_2 (d) stimulated emission



Gain need not be greater than loss
 N_2 need not be greater than N_1
Long T_2 is desirable, not necessary

Stimulated emission is necessary for laser action

2. An Er-doped fiber laser pumped at 980 nm and operating at 1550 nm can be characterized as

- (a) 2-level (b) 3-level (c) 4-level (d) Cannot say

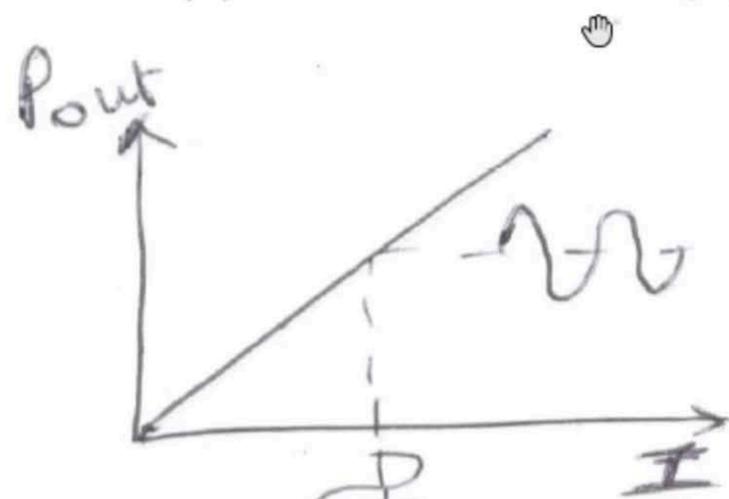
3. The average lifetime spent by a photon in a Fabry Perot laser cavity with loss = 10 cm^{-1} & $n=3$

- (a) 1 ps (b) 10 ps (c) 100 ps (d) 1 ns

$$\tau_{ph} = \frac{1}{v_g \alpha_s} = \frac{1}{\frac{3 \times 10^8}{3} \times 10 \times 100} = 10^{-11} \text{ s} \text{ or } \underline{10 \text{ ps}}$$

4. The modulation bandwidth of a LED does NOT depend on

- (a) drive current (b) heterostructure (c) recombination lifetime (d) any of these



$$f_{3dB} \propto \frac{1}{\tau_c} \Rightarrow \text{depends on recombination lifetime}$$

Not dependent on drive current

heterostructure helps to reduce recombination lifetime

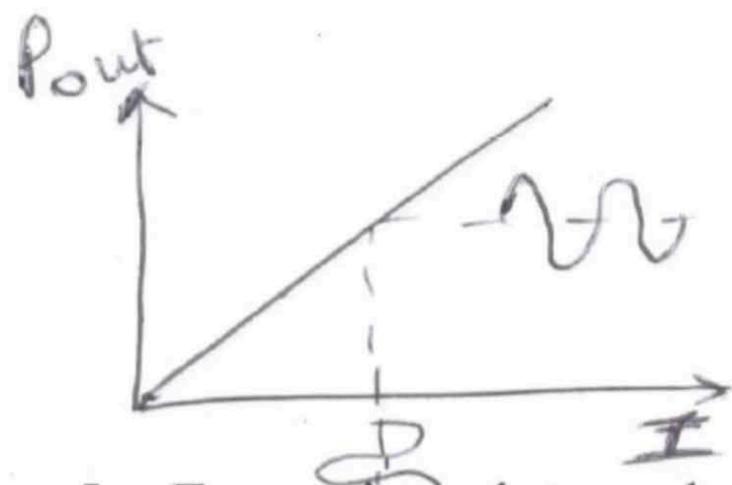
5. For a given internal efficiency, the responsivity of a photodiode scales as

- (a) $1/\lambda$ (b) $\sqrt{\lambda}$ (c) λ^2 (d) λ

$$R = \frac{I_p}{P_{in}} = \frac{\eta q}{h\nu} = \frac{\eta \lambda (\mu\text{m})}{1.24}$$

4. The modulation bandwidth of a LED does NOT depend on

- (a) drive current (b) heterostructure (c) recombination lifetime (d) any of these



$$f_{3dB} \propto \frac{1}{\tau_c}$$

NOT dependent on drive current

⇒ depends on recombination lifetime

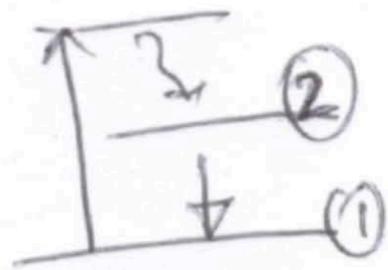
heterostructure helps to reduce recombination lifetime

5. For a given internal efficiency, the responsivity of a photodiode scales as

- (a) $1/\lambda$ (b) $\sqrt{\lambda}$ (c) λ^2 (d) λ

$$R = \frac{I_p}{P_{in}} = \frac{\eta q}{h\nu} = \frac{\eta \lambda (\mu m)}{1.24}$$

$$R \propto \lambda$$



Gain need not be greater than loss
 N_2 need not be greater than N_1
 Long T_2 is desirable, not necessary

Stimulated emission is necessary for laser action

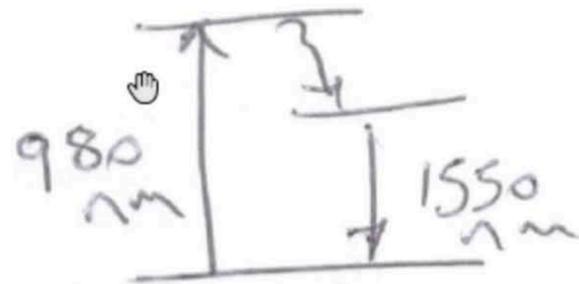
2. An Er-doped fiber laser pumped at 980 nm and operating at 1550 nm can be characterized as

(a) 2-level

(b) 3-level

(c) 4-level

(d) Cannot say



\Rightarrow 3-level laser

3. The average lifetime spent by a photon in a Fabry Perot laser cavity with loss = 10 cm^{-1} & $n=3$

(a) 1 ps

(b) 10 ps

(c) 100 ps

(d) 1 ns

$$\tau_{ph} = \frac{1}{v_g \alpha_s} = \frac{1}{\frac{3 \times 10^8}{3} \times 10 \times 100} = 10^{-11} \text{ s} \text{ or } \underline{10 \text{ ps}}$$

4. The modulation bandwidth of a LED does NOT depend on

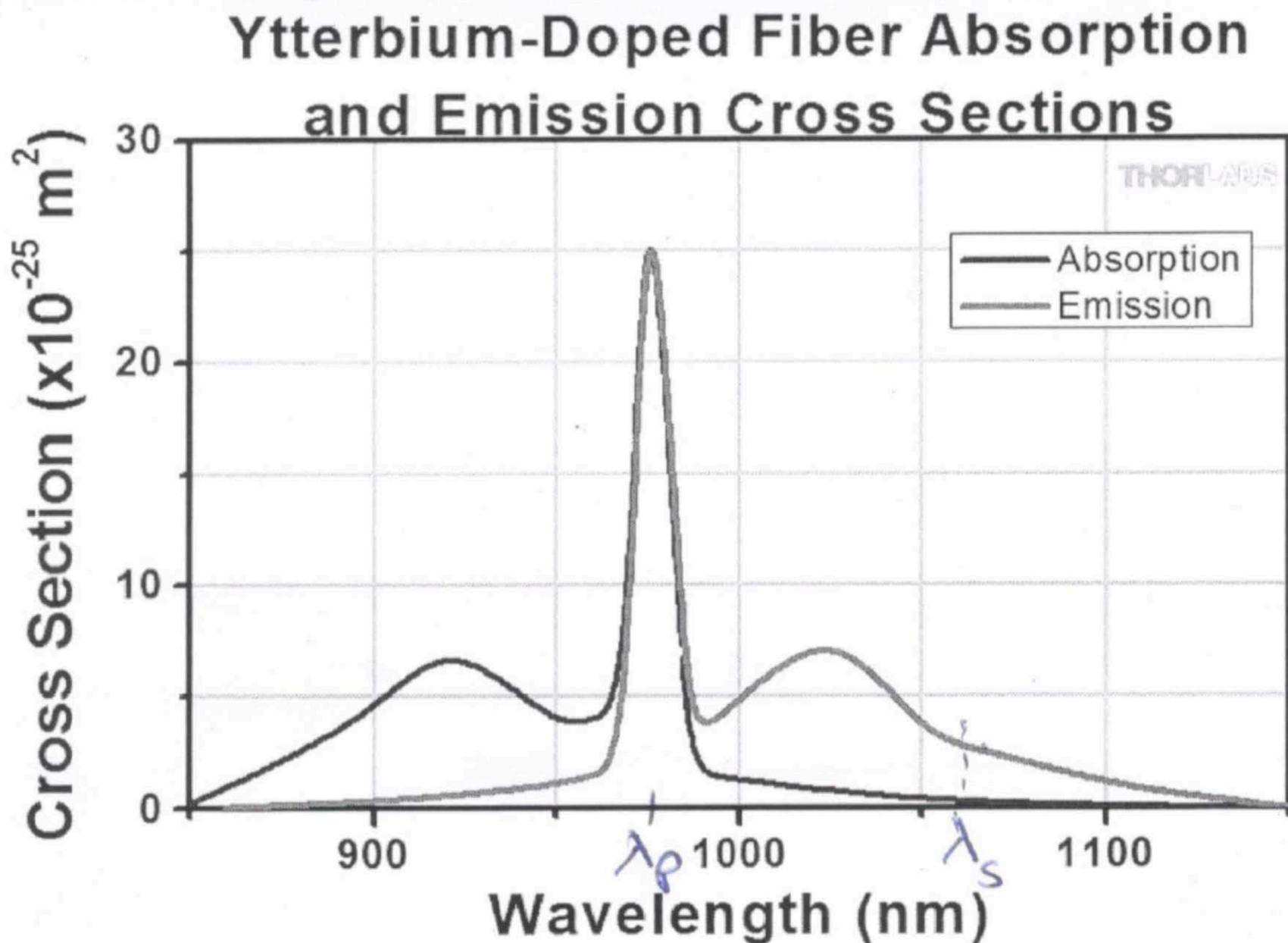
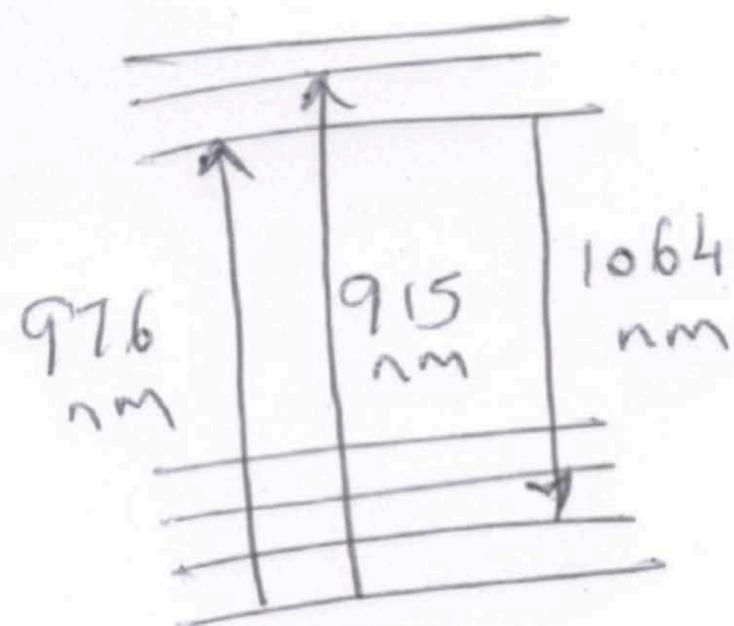
(a) drive current

(b) heterostructure

(c) recombination lifetime

(d) any of these

6. Suppose you are asked to design an optical amplifier at 1064 nm wavelength using a Yb-doped silica optical fiber, whose doping concentration is $3 \times 10^{24} \text{ m}^{-3}$ and its absorption and emission cross-sections are provided below.



- a. Based on the above graph, what are the possible pump wavelengths for the amplifier? Which one will you choose and why? (2 pts)

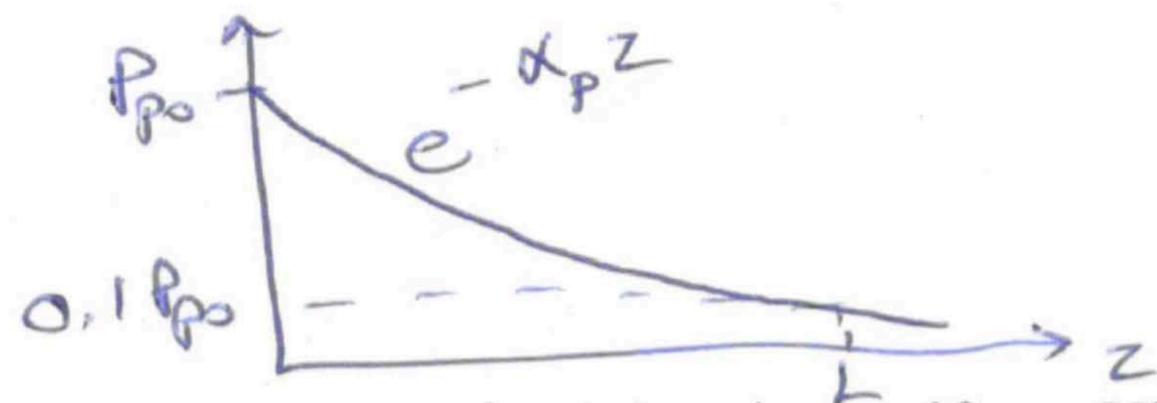
- a. Based on the above graph, what are the possible pump wavelengths for the amplifier? Which one will you choose and why? (2 pts)

915 nm & 976 nm. The latter is preferred since the absorption cross-section is 3x higher.

- b. Starting from appropriate rate equations, derive an expression for the small signal gain of the amplifier. (2 pts)

$$\frac{dP_s}{dz} = (N_2 \sigma_e^s - N_1 \sigma_a^s) P_s \Rightarrow G = \exp \left[\int_0^L (N_2 \sigma_e^s - N_1 \sigma_a^s) dz \right]$$

- c. Estimate the length of Yb fiber required to absorb 90% of the launched pump radiation. (2 pts)

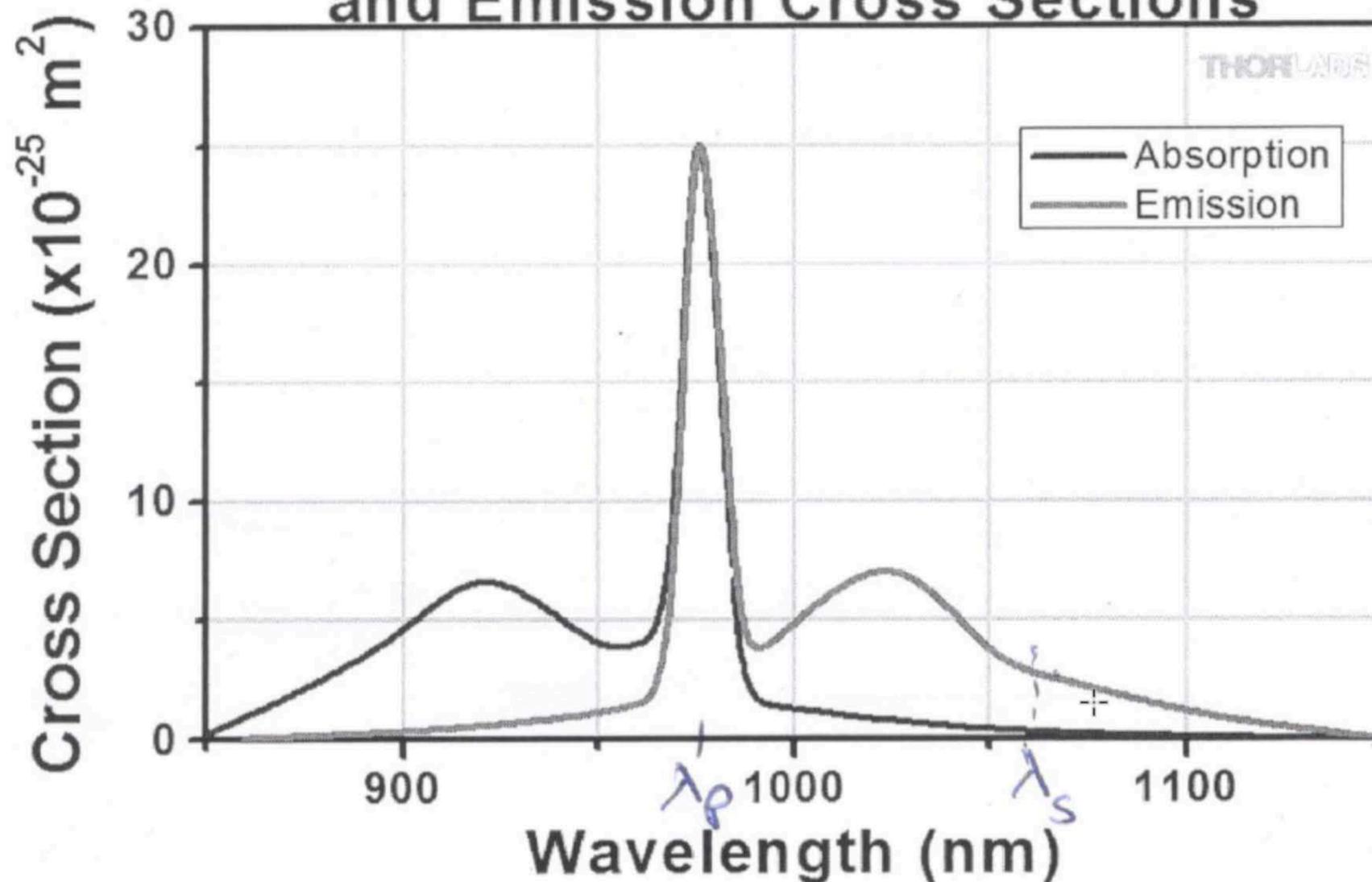
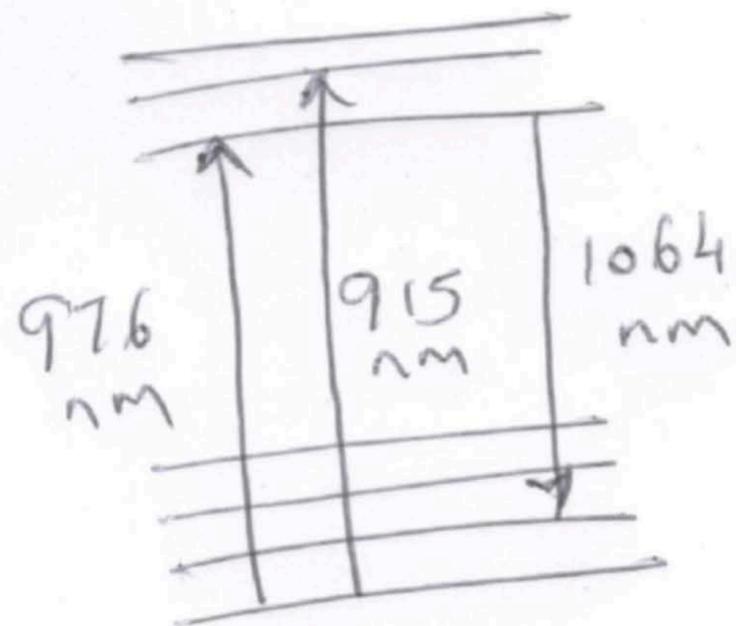


$$\alpha_p = N_a \sigma_a^p = 3 \times 10^{24} \times 2.5 \times 10^{-24} = 7.5 \text{ m}^{-1}$$

$$e^{-\alpha_p L} = 0.1 \Rightarrow L = \frac{1}{7.5} \ln(0.1) = \underline{\underline{14 \text{ mm}}}$$

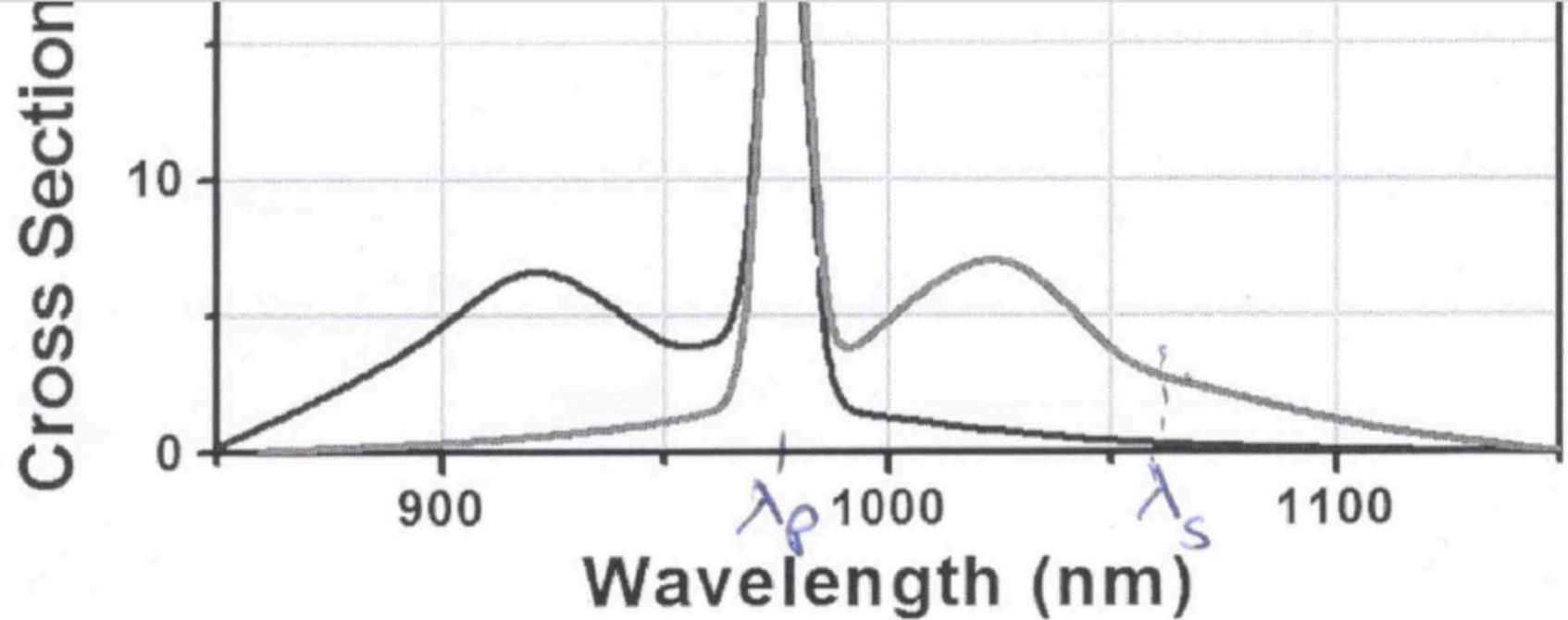
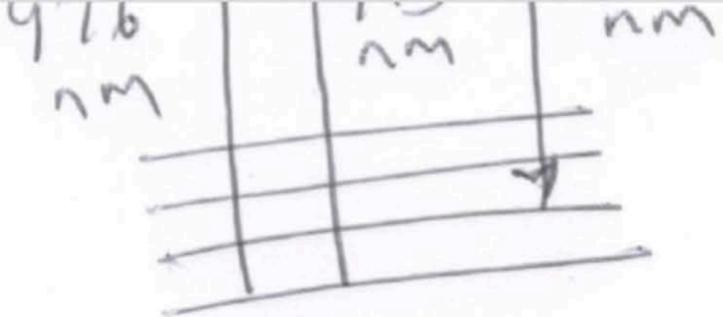
- d. Assuming uniform Yb ion excitation of 50% along the above length of fiber, what is the small-signal gain that could be achieved? (2 pts)

Ytterbium-Doped Fiber Absorption and Emission Cross Sections



- a. Based on the above graph, what are the possible pump wavelengths for the amplifier? Which one will you choose and why? (2 pts)

915 nm & 976 nm. The latter is preferred since the absorption cross-section is 3x higher.



- a. Based on the above graph, what are the possible pump wavelengths for the amplifier? Which one will you choose and why? (2 pts)

915 nm & 976 nm. The latter is preferred since the absorption cross-section is 3x higher.

- b. Starting from appropriate rate equations, derive an expression for the small signal gain of the amplifier. (2 pts)

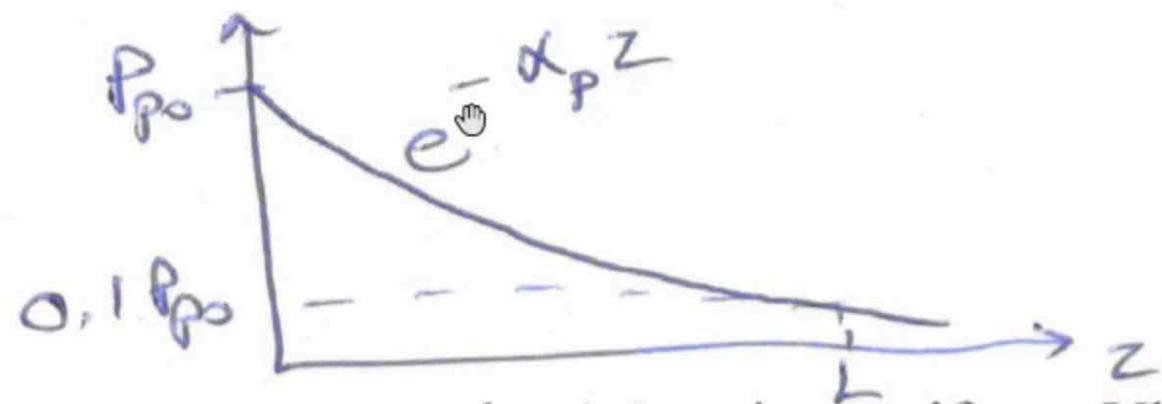
$$\frac{dP_s}{dz} = (N_2 \sigma_e^s - N_1 \sigma_a^s) P_s \Rightarrow G = \exp \left[\int_0^L (N_2 \sigma_e^s - N_1 \sigma_a^s) dz \right]$$

since the absorption cross-section is 3x higher.

- b. Starting from appropriate rate equations, derive an expression for the small signal gain of the amplifier. (2 pts)

$$\frac{dP_s}{dz} = (N_2 \sigma_e^s - N_1 \sigma_a^s) P_s \Rightarrow G = \exp \left[\int_0^L (N_2 \sigma_e^s - N_1 \sigma_a^s) dz \right]$$

- c. Estimate the length of Yb fiber required to absorb 90% of the launched pump radiation. (2 pts)



$$\alpha_p = N_a \sigma_a^p = 3 \times 10^{24} \times 2.5 \times 10^{-24} = 7.5 \text{ m}^{-1}$$

$$e^{-\alpha_p L} = 0.1 \Rightarrow L = \frac{1}{7.5} \ln(0.1) = \underline{14 \text{ mm}}$$

- d. Assuming uniform Yb ion excitation of 50% along the above length of fiber, what is the small-signal gain that could be achieved? (2 pts)

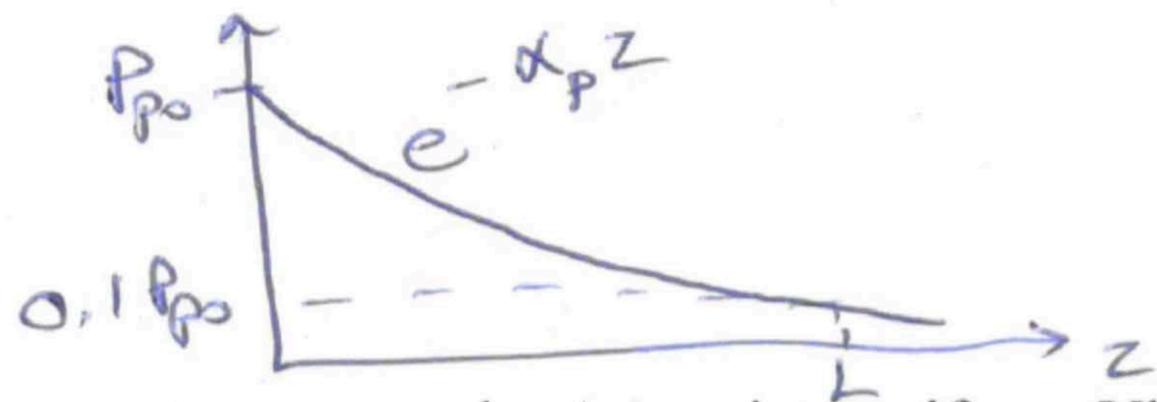
Assuming 50% excitation, $N_1 = N_2 = 0.5 N_a$

at 1064 nm (λ_s), $\sigma_e^s = 3 \times 10^{-25} \text{ m}^2$

$$\frac{dP_s}{dz} = (N_2 \sigma_e^s - N_1 \sigma_a^s) P_s \Rightarrow G = \exp \left[\int_0^L (N_2 \sigma_e^s - N_1 \sigma_a^s) dz \right]$$

c. Estimate the length of Yb fiber required to absorb 90% of the launched pump radiation.

(2 pts)



$$\alpha_p = N_a \sigma_a^p = 3 \times 10^{24} \times 2.5 \times 10^{-24} = 7.5 \text{ m}^{-1}$$

$$e^{-\alpha_p L} = 0.1 \Rightarrow L = \frac{1}{7.5} \ln(0.1) = \underline{\underline{14 \text{ mm}}}$$

d. Assuming uniform Yb ion excitation of 50% along the above length of fiber, what is the small-signal gain that could be achieved?

(2 pts)

Assuming 50% excitation, $N_1 = N_2 = 0.5 N_a$

$$\text{At } 1064 \text{ nm } (\lambda_s), \quad \sigma_e^s = 3 \times 10^{-25} \text{ m}^2$$

$$\sigma_a^s = 0.1 \times 10^{-25} \text{ m}^2$$

8

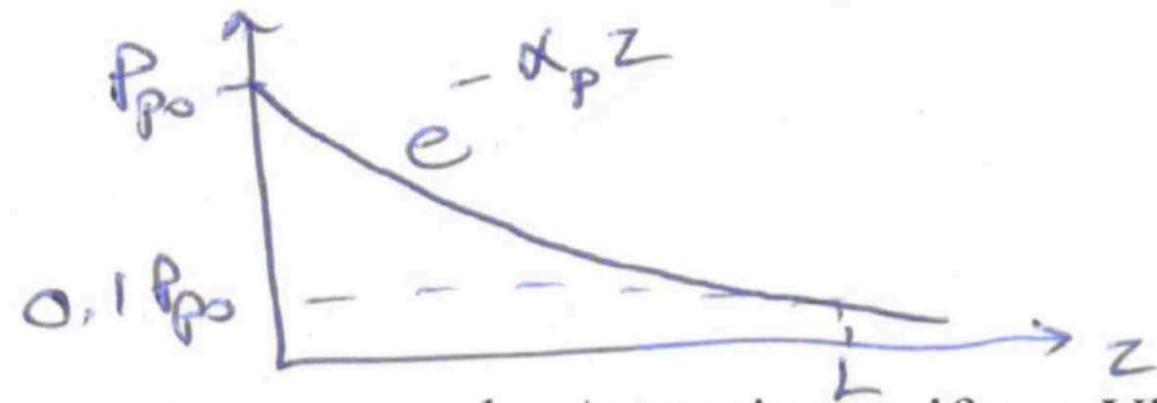
-25

-37

$$\frac{dP}{dz} = (N_2 \sigma_e^s - N_1 \sigma_a^s) P \Rightarrow G = \exp \left[\int_0^L (N_2 \sigma_e^s - N_1 \sigma_a^s) dz \right]$$

c. Estimate the length of Yb fiber required to absorb 90% of the launched pump radiation.

(2 pts)



$$\alpha_p = N_a \sigma_a^p = 3 \times 10^{24} \times 2.5 \times 10^{-24} = 7.5 \text{ m}^{-1}$$

$$e^{-\alpha_p L} = 0.1 \Rightarrow L = \frac{1}{7.5} \ln(0.1) = \underline{\underline{14 \text{ mm}}}$$

d. Assuming uniform Yb ion excitation of 50% along the above length of fiber, what is the small-signal gain that could be achieved? (2 pts)

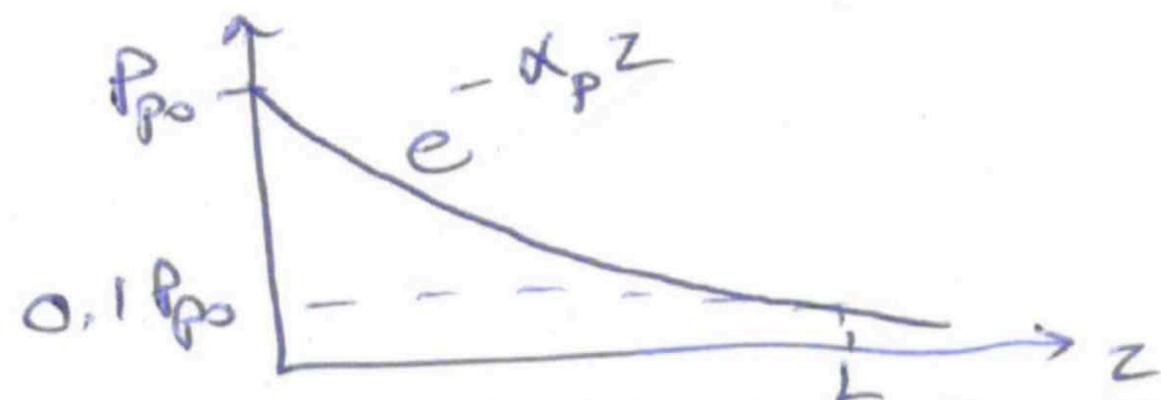
Assuming 50% excitation, $N_1 = N_2 = 0.5 N_a$

At 1064 nm (λ_s), $\sigma_e^s = 3 \times 10^{-25} \text{ m}^2$

$\sigma_a^s = 0.1 \times 10^{-25} \text{ m}^2$

$$\left[0.5 \times 3 \times 10^{24} \times 2.9 \times 10^{-25} \times 14 \times 10^{-3} \right]$$

c. Estimate the length of Yb fiber required to absorb 90% of the launched pump radiation. (2 pts)



$$\alpha_p = N_a \sigma_a^p = 3 \times 10^{24} \times 2.5 \times 10^{-24} = 7.5 \text{ m}^{-1}$$

$$e^{-\alpha_p L} = 0.1 \Rightarrow L = \frac{1}{7.5} \ln(0.1) = \underline{14 \text{ mm}}$$

d. Assuming uniform Yb ion excitation of 50% along the above length of fiber, what is the small-signal gain that could be achieved? (2 pts)

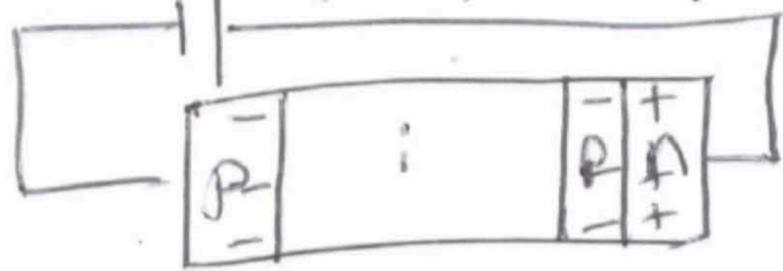
Assuming 50% excitation, $N_1 = N_2 = 0.5 N_a$

At 1064 nm (λ_s), $\sigma_e^s = 3 \times 10^{-25} \text{ m}^2$ +

$$\sigma_a^s = 0.1 \times 10^{-25} \text{ m}^2$$

$$G = \exp \left[0.5 \times 3 \times 10^{24} \times 2.9 \times 10^{-25} \times 14 \times 10^{-3} \right]$$

$$= 1.006$$



Add p-layer between n & i layers
 \Rightarrow most of V_b drops across p-n junction

- d. If the width of the multiplication region is $2 \mu\text{m}$ and the voltage drop across it is 50 V, what is the multiplicative gain (M) that could be achieved in the APD? (2 pts)

$$E\text{-field in multiplication region} = \frac{50 \text{ V}}{2 \mu\text{m}} = 2.5 \times 10^5 \text{ V/cm}$$

$$\Rightarrow \alpha_e = 2 \times 10^4 \text{ cm}^{-1}$$

Useful Constants:

Planck's constant (h) = 6.6256×10^{-34} J.s

Boltzmann's constant (k_B) = 1.38×10^{-23} J/K

Electric charge (q) = 1.602×10^{-19} C

Velocity of light (c) = 3×10^8 m/s

Useful Formulae

- $M = (1-k) / \{ \exp [-(1-k)\alpha_e w_m] - k \}$
- $F = k.M + (1-k).(2 - 1/M)$

$$\alpha_e w_m = 4$$

3

$$M = \frac{0.5}{e^{-2} - 0.5} = \frac{-1.37}{-}$$

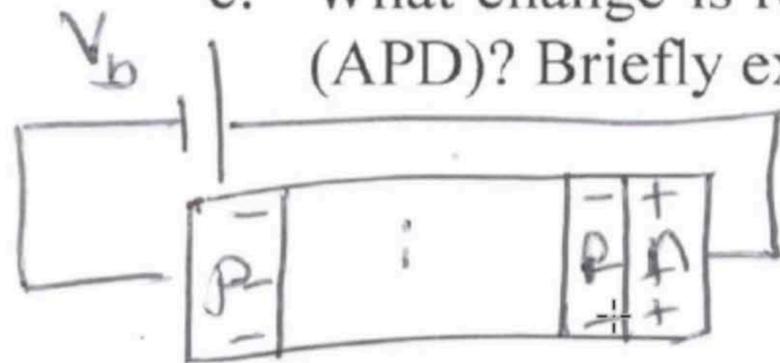
- a. Assuming negligible contribution from RC time constant and a saturation drift velocity of 10^5 m/s for 5 V reverse bias, what is the maximum width of the intrinsic region allowed to support the above bandwidth? (2 pts)

$$f_{3dB} = \frac{1}{2\pi(\tau_{tr} + \tau_{RC})} \quad \text{where } \tau_{tr} = \frac{W}{v_{dr}} = \frac{1}{2\pi \cdot f_{3dB}} \Rightarrow W = \frac{v_{dr}}{2\pi \times f_{3dB}}$$

- b. For the above structure, what is the expected responsivity? (2 pts)

$$R = \frac{\eta \lambda}{1.24} \quad \text{where } \eta = (1 - R_f) \zeta (1 - e^{-\alpha W}) \approx 0.8 \Rightarrow R = \underline{1 \text{ A/W}}$$

- c. What change is required in the above structure to realize an avalanche photodiode (APD)? Briefly explain with the help of appropriate schematic diagram. (1 pt)

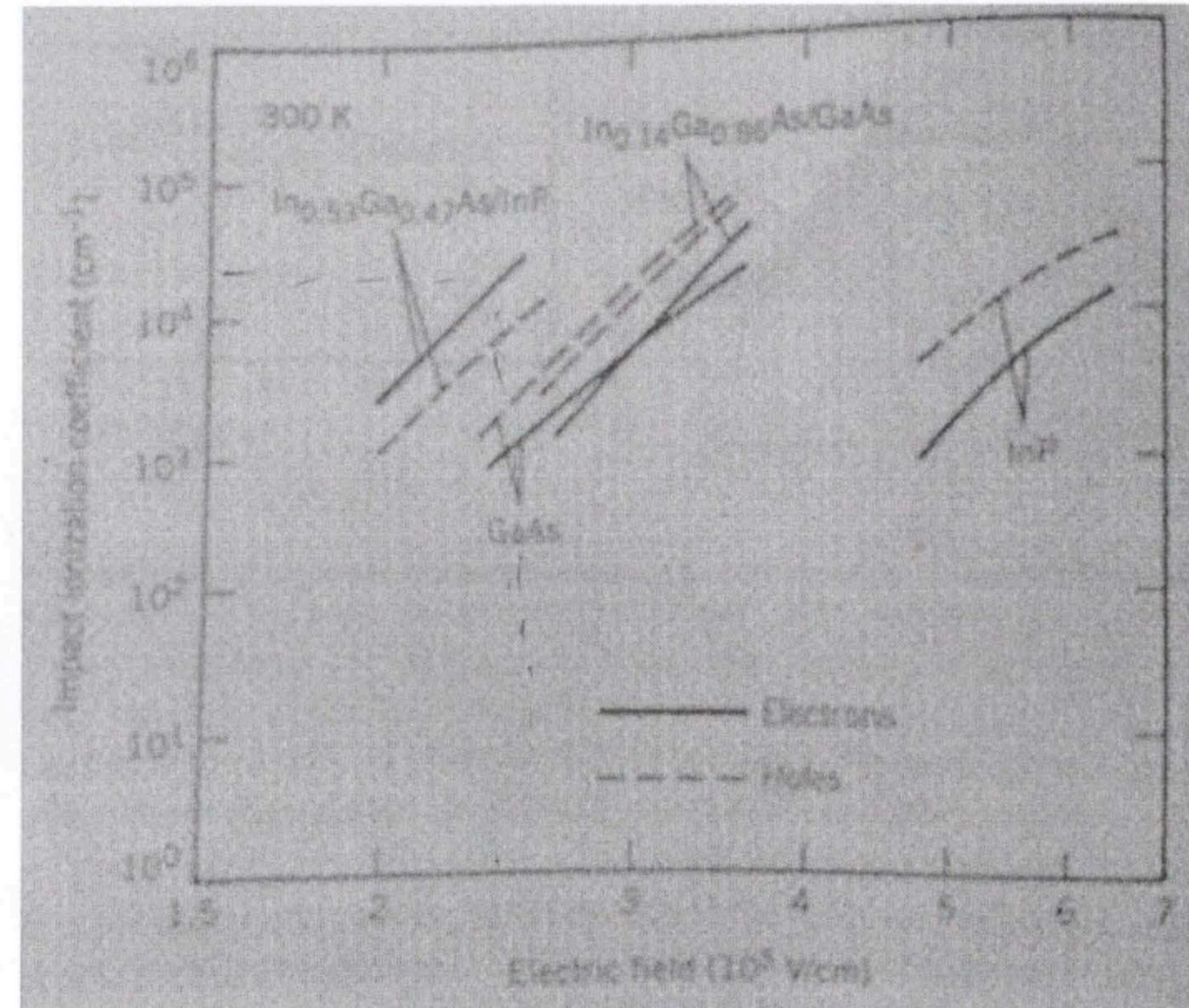
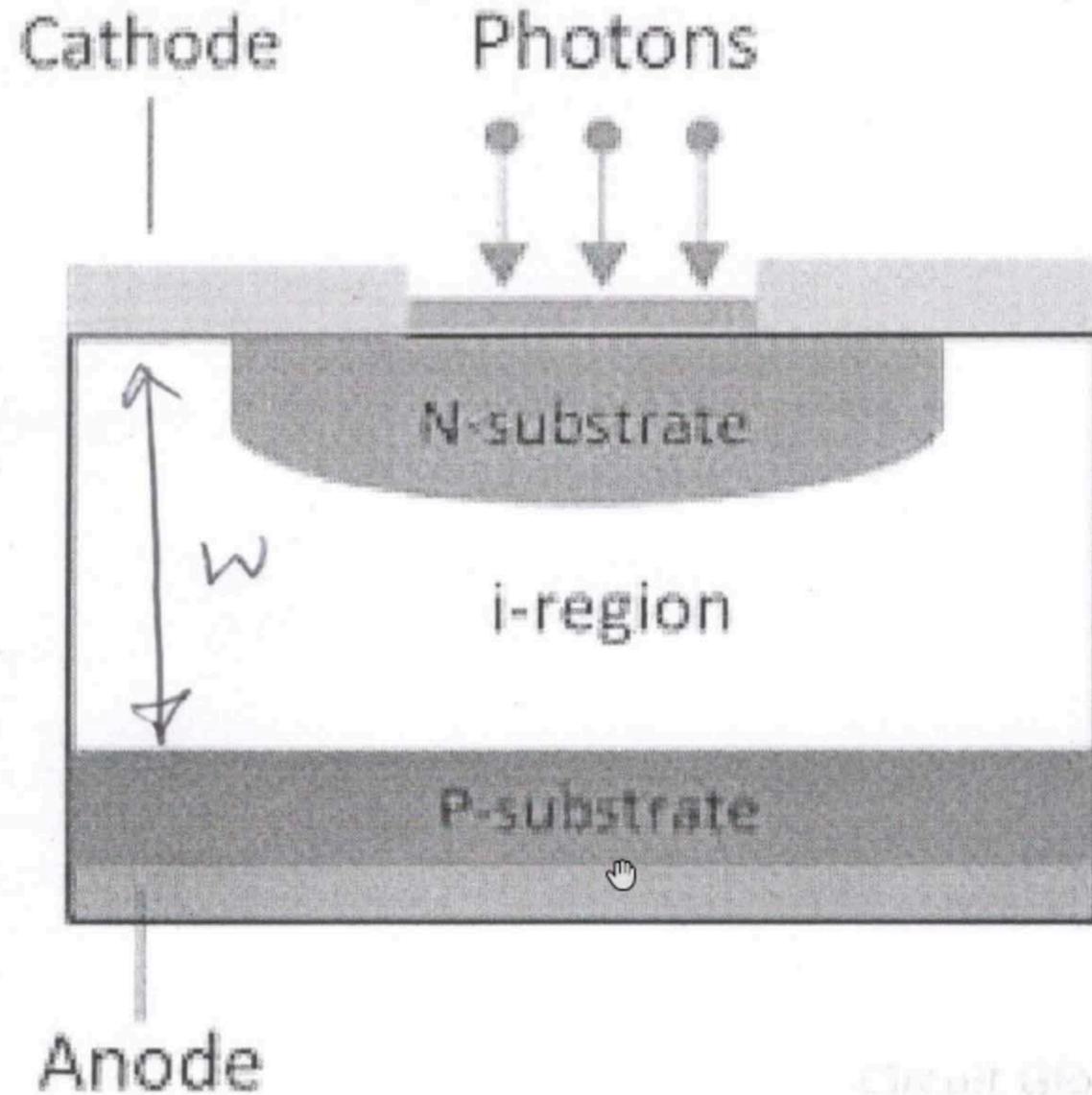


Add p-layer between n & i layers
 \Rightarrow most of V_b drops across p-n junction

- d. If the width of the multiplication region is $2 \mu\text{m}$ and the voltage drop across it is 50 V, what is the multiplicative gain (M) that could be achieved in the APD? (2 pts)

$$E\text{-field in multiplication region} = \frac{50 \text{ V}}{2 \mu\text{m}} = 2.5 \times 10^5 \text{ V/cm}$$

7. You have been asked to design a PIN photodiode with a bandwidth of 2.5 GHz for an optical fiber communication system using $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ material ($k = 0.5$). The operation conditions include: photo-electron conversion efficiency of 0.8, anti-reflection coated facet, and an absorption coefficient of $0.5 \times 10^5 \text{ cm}^{-1}$ at 1550 nm.



a. Assuming negligible contribution from RC time constant and a saturation drift

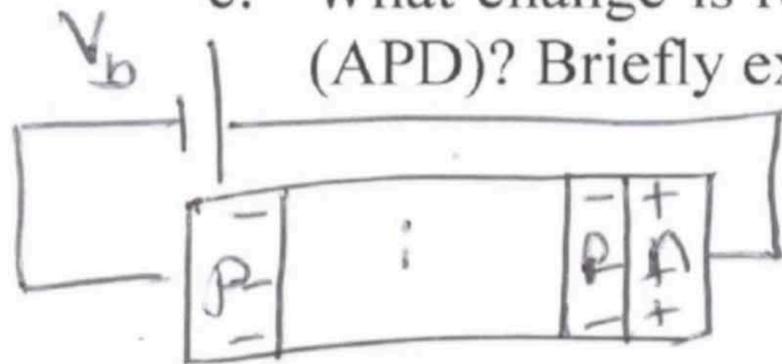
- a. Assuming negligible contribution from RC time constant and a saturation drift velocity of 10^5 m/s for 5 V reverse bias, what is the maximum width of the intrinsic region allowed to support the above bandwidth? (2 pts)

$$f_{3dB} = \frac{1}{2\pi(\tau_{tr} + \tau_{RC})} \quad \text{where } \tau_{tr} = \frac{W}{v_{dr}} = \frac{1}{2\pi \cdot f_{3dB}} \Rightarrow W = \frac{v_{dr}}{2\pi \cdot f_{3dB}}$$

- b. For the above structure, what is the expected responsivity? (2 pts)

$$R = \frac{\eta \lambda}{1.24} \quad \text{where } \eta = (1 - R_f) \cdot (1 - e^{-\alpha W}) \approx 0.8 \Rightarrow R = 1 \text{ A/W}$$

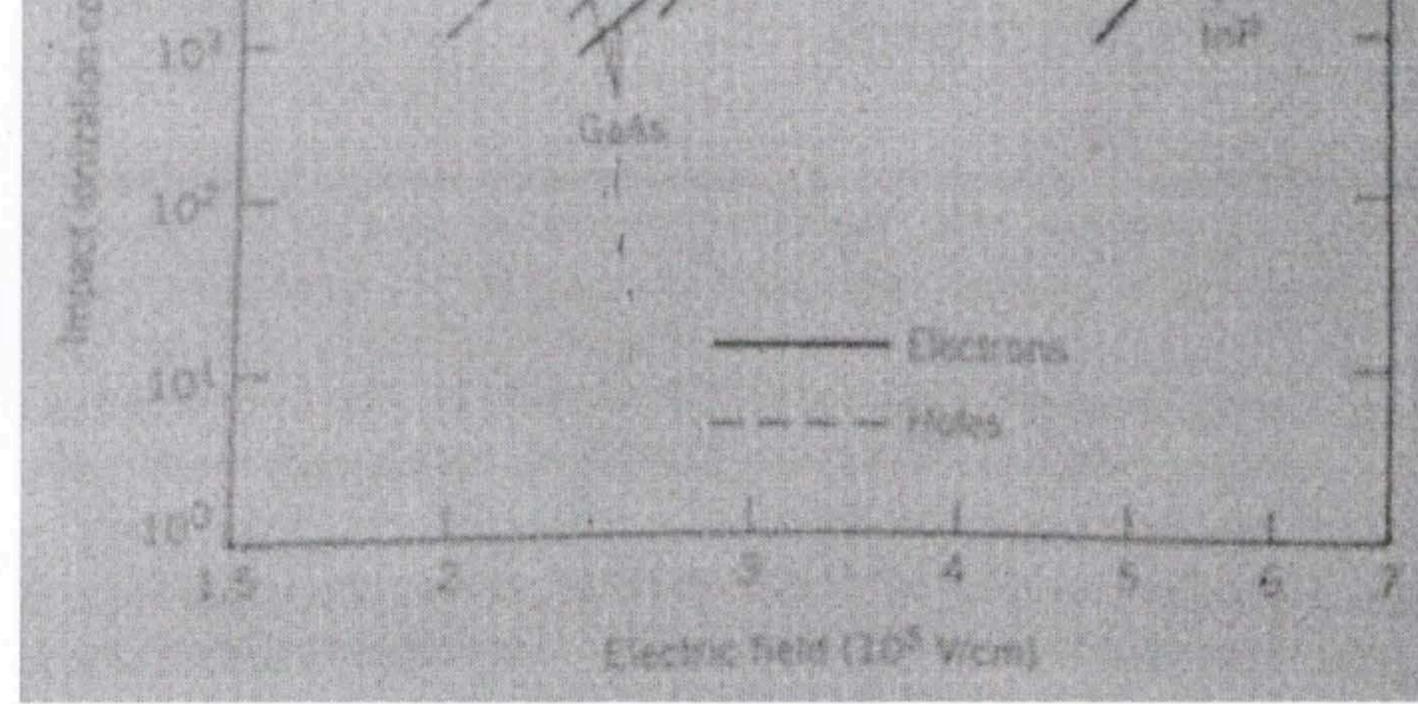
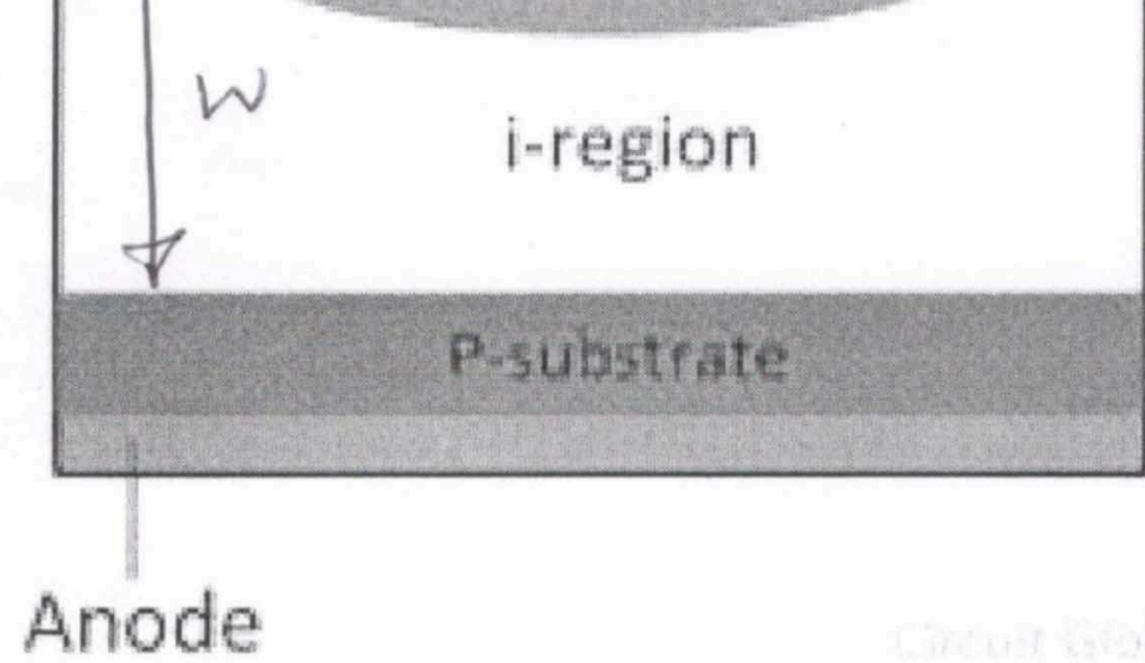
- c. What change is required in the above structure to realize an avalanche photodiode (APD)? Briefly explain with the help of appropriate schematic diagram. (1 pt)



Add p-layer between n & i layers
 \Rightarrow most of V_b drops across p-n junction

- d. If the width of the multiplication region is $2 \mu\text{m}$ and the voltage drop across it is 50 V, what is the multiplicative gain (M) that could be achieved in the APD? (2 pts)

$$E\text{-field in multiplication region} = \frac{50 \text{ V}}{2 \mu\text{m}} = 2.5 \times 10^5 \text{ V/cm}$$



- a. Assuming negligible contribution from RC time constant and a saturation drift velocity of 10^5 m/s for 5 V reverse bias, what is the maximum width of the intrinsic region allowed to support the above bandwidth? (2 pts)

$$f_{3dB} = \frac{1}{2\pi(\tau_{tc} + \tau_{RC})} \quad \text{where } \tau_{tr} = \frac{w}{v_{dr}} = \frac{1}{2\pi \cdot f_{3dB}} \Rightarrow w = \frac{v_{dr}}{2\pi \cdot f_{3dB}}$$

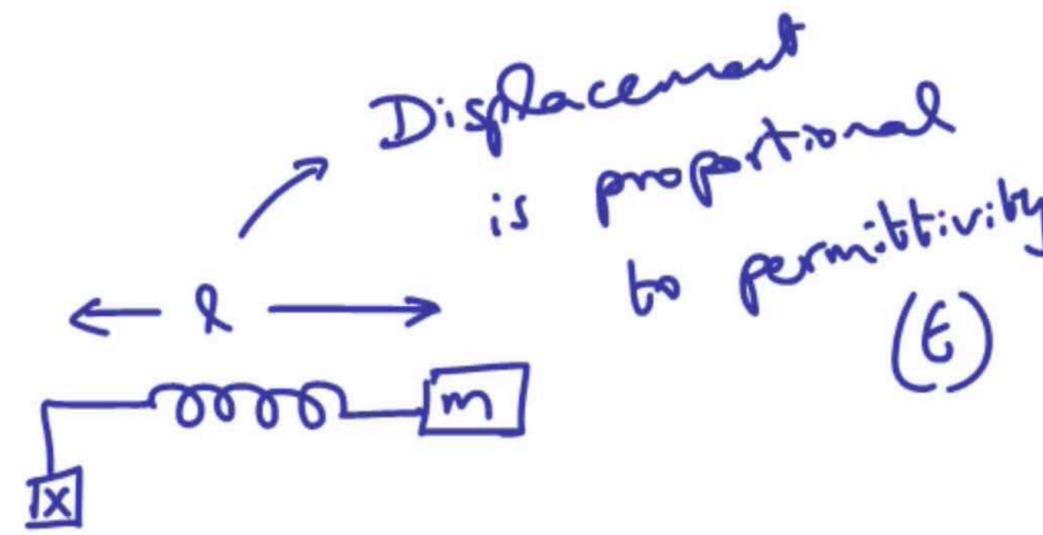
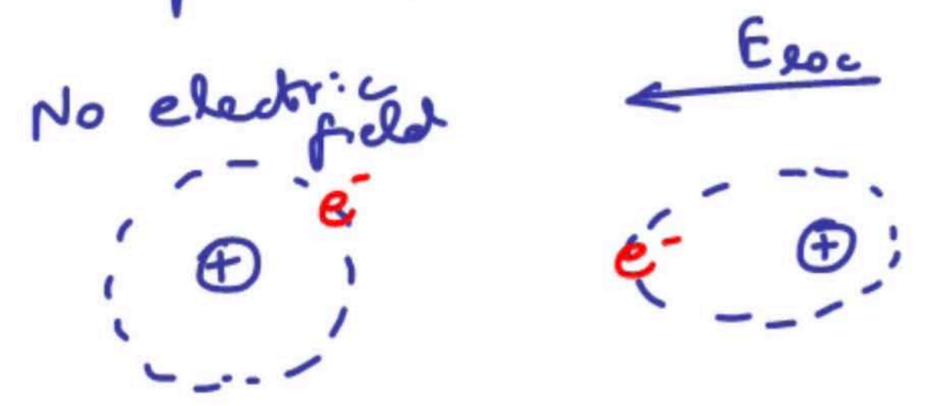
- b. For the above structure, what is the expected responsivity? (2 pts)

$$R = \frac{\eta \lambda}{1.24} \quad \text{where } \eta = (1 - R_f) \epsilon (1 - e^{-\alpha w}) \approx 0.8 \Rightarrow R = 1 \text{ A/W}$$

- c. What change is required in the above structure to realize an avalanche photodiode

Learning Outcome: Identify the fundamental principles for photon/light manipulation

How does light propagate in a medium?

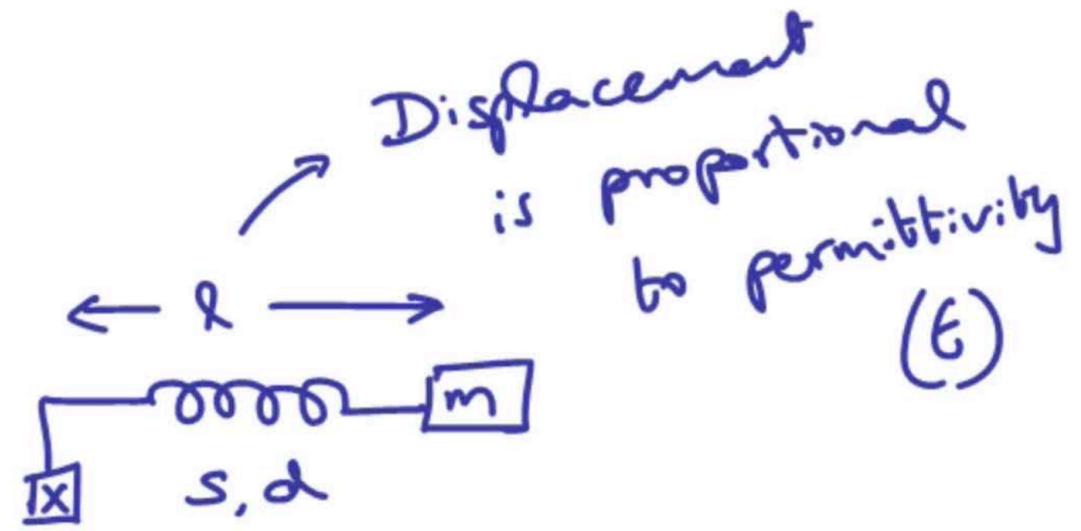
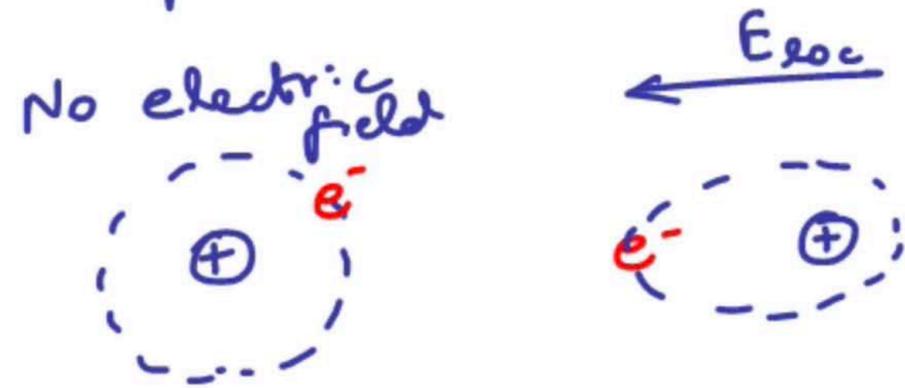


Equation of motion,
$$m \cdot \frac{d^2 l}{dt^2} + d \cdot \frac{dl}{dt} + s \cdot l = -e E_{loc}$$

for time-periodic excitation ($e^{i\omega t}$)

photon/light manipulation

How does light propagate in a medium?



Equation of motion,

$$m \cdot \frac{d^2 l}{dt^2} + d \cdot \frac{dl}{dt} + s \cdot l = -e E_{loc}$$

$$\epsilon = \epsilon' - j\epsilon''$$

for time-periodic excitation ($e^{j\omega t}$)

$$l = \frac{-e/m E_{loc}}{\omega_0^2 - \omega^2 + j\omega \frac{d}{m}}$$

damping
coeff.
 d/m

resonance freq. \leftarrow
 $\omega_0 = \sqrt{s/m}$

Equation of motion,

$$m \cdot \frac{d^2x}{dt^2} + d \cdot \frac{dx}{dt} + kx = F_0 e^{j\omega t}$$

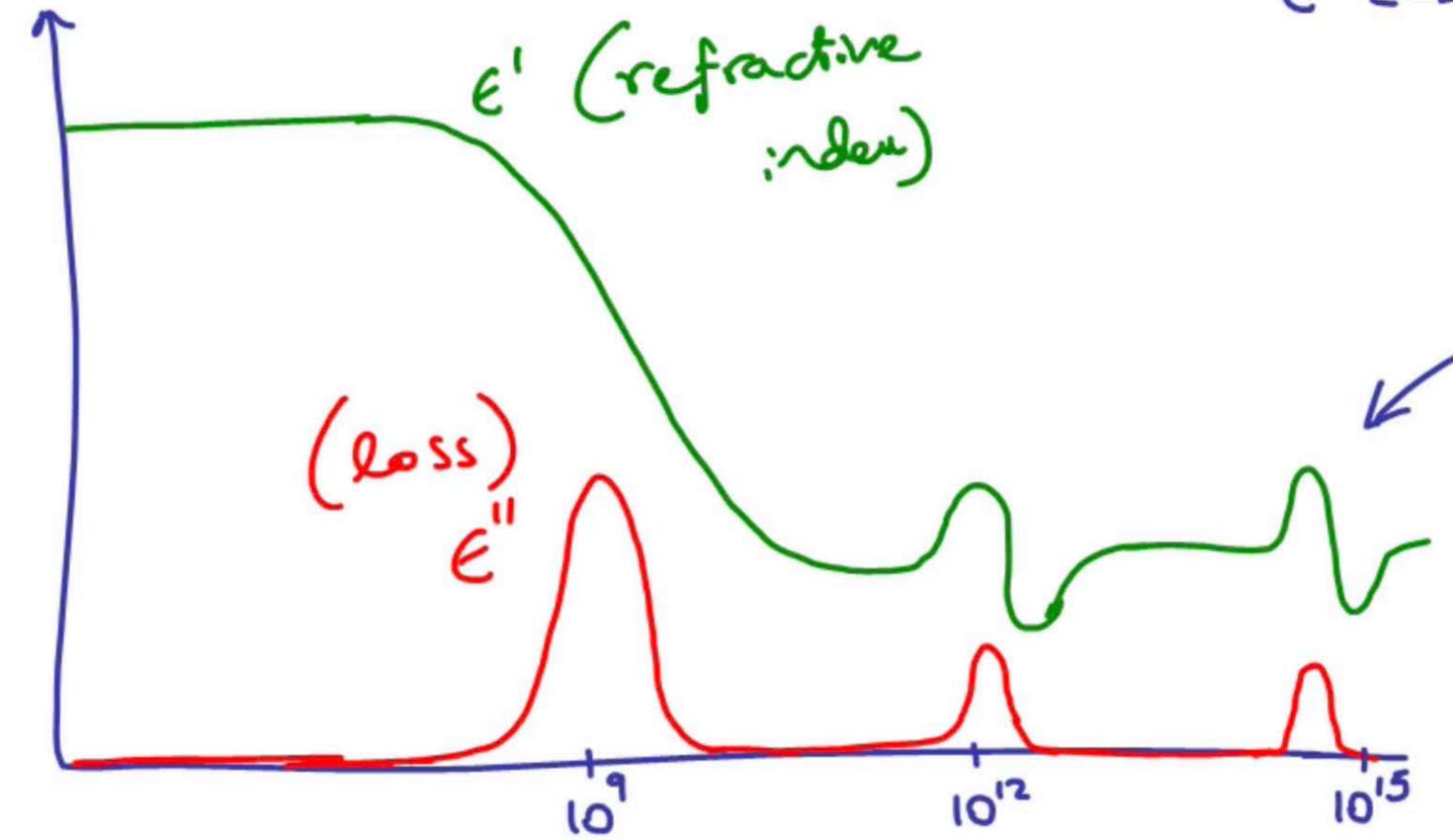
For time-periodic excitation ($e^{j\omega t}$),

$$\underline{Z} = \frac{-e/m E_{loc}}{\omega_0^2 - \omega^2 + j\omega \frac{d}{m}}$$

damping
coeff.
 d/m

resonance freq. \leftarrow
 $\omega_0 = \sqrt{\frac{s}{m}}$

$\epsilon' \Leftrightarrow \epsilon''$ (Kramers-Kronig relation)



Electronic
resonance

Frequency

Capture Effects Tools Help

Duration: 1:13:47

Audio: [Progress bar]

Delete Pause Stop

Equation of motion,

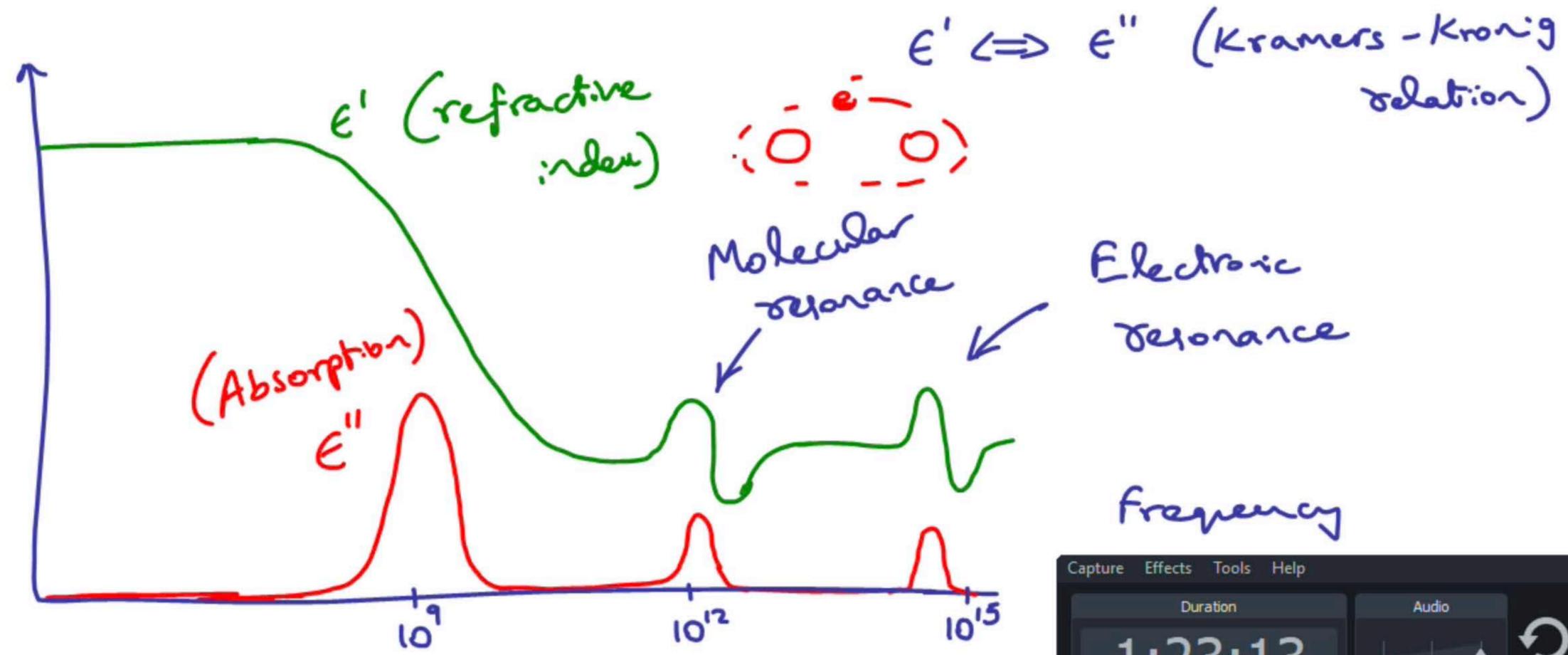
$$m \cdot \frac{d^2x}{dt^2} + d \cdot \frac{dx}{dt} + kx = F_0 e^{j\omega t}$$

For time-periodic excitation ($e^{j\omega t}$),

$$\rho = \frac{-e/m E_{loc}}{\omega_0^2 - \omega^2 + j\omega \frac{d}{m}}$$

damping
Coeff.
 d/m

resonance freq. \leftarrow
 $\omega_0 = \sqrt{\frac{s}{m}}$



Capture Effects Tools Help

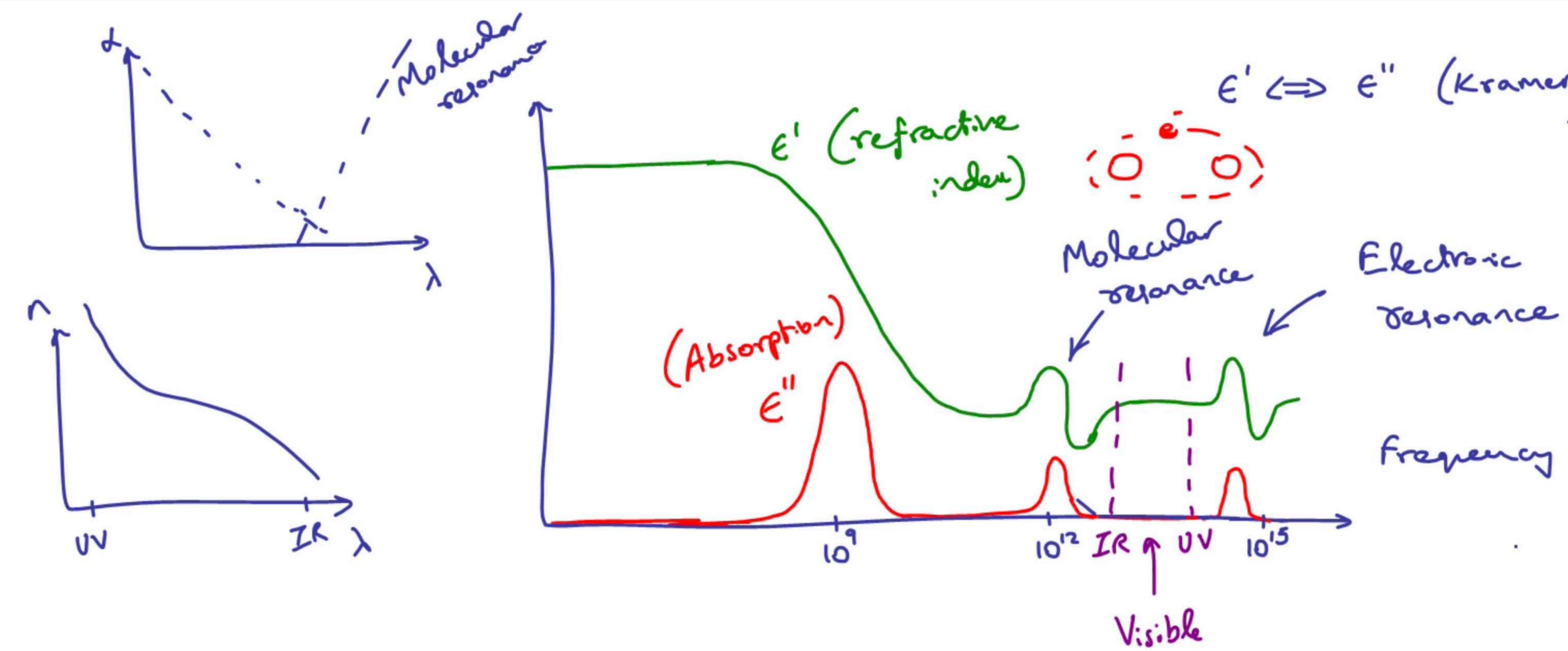
Duration: 1:23:13

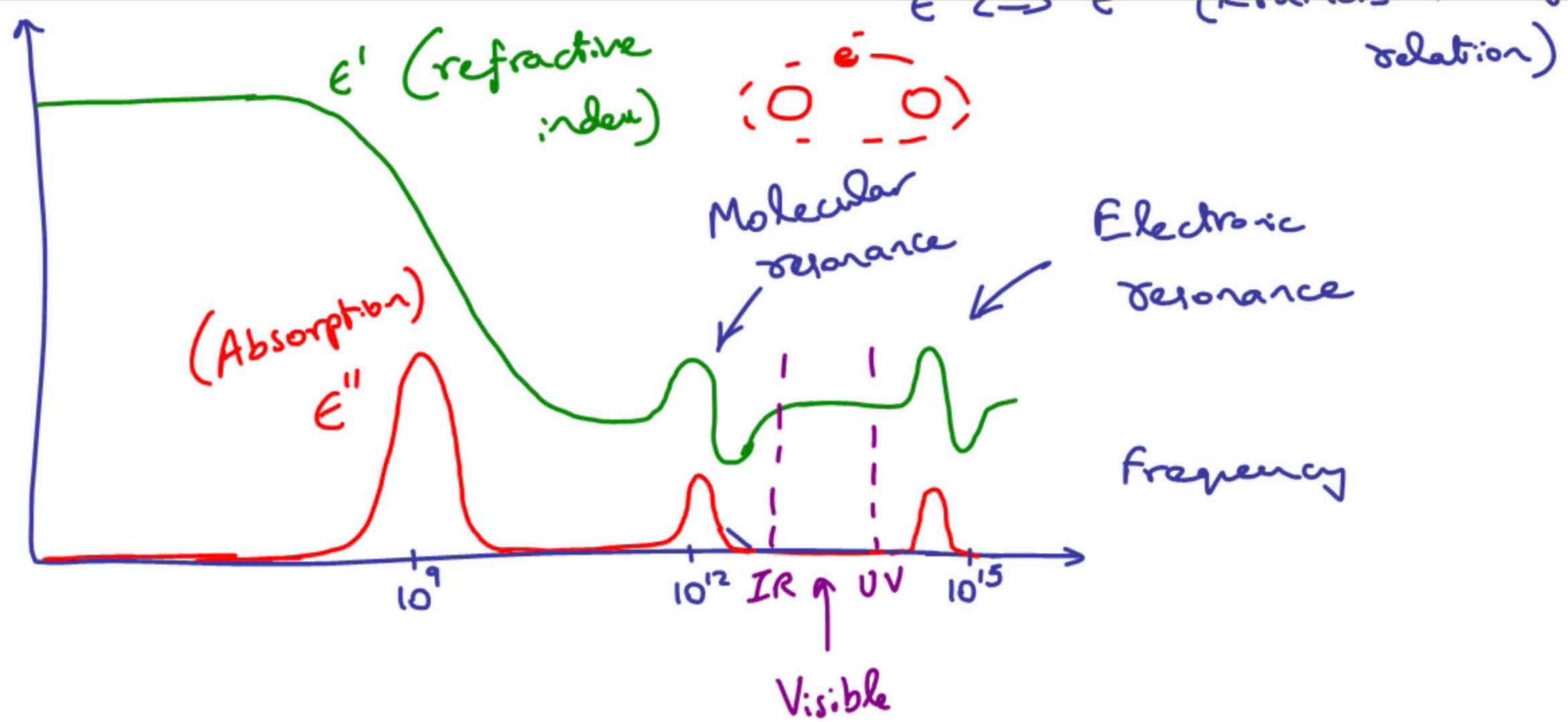
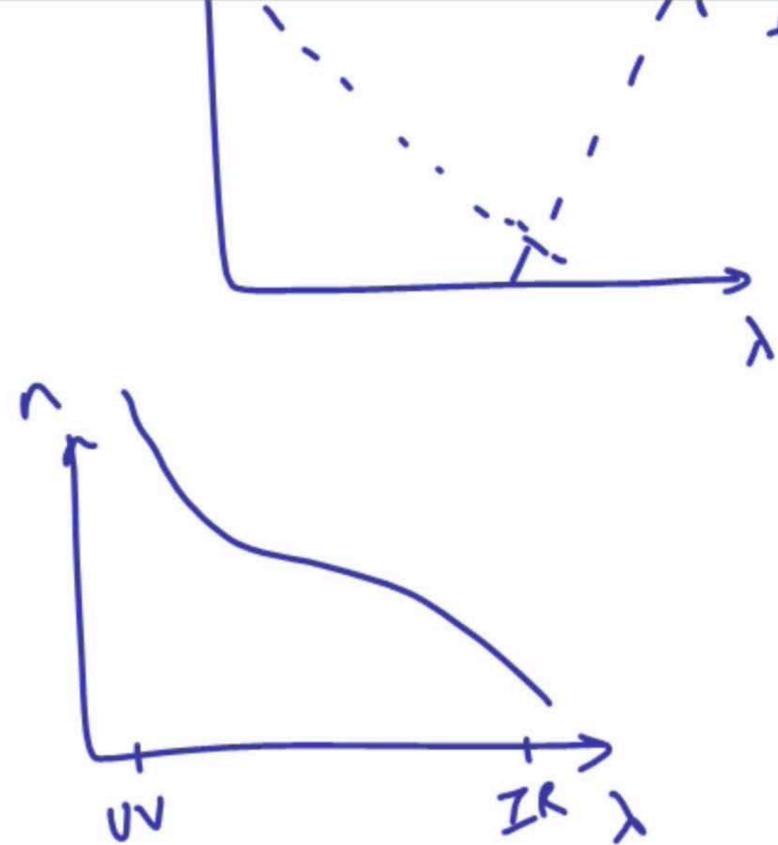
Audio: [Progress bar]

Delete Pause Stop

resonance freq. $\leftarrow \omega_0 = \sqrt{\frac{s}{m}}$ damping coeff. γ

$\epsilon' \Leftrightarrow \epsilon''$ (Kramers-Kronig relation)





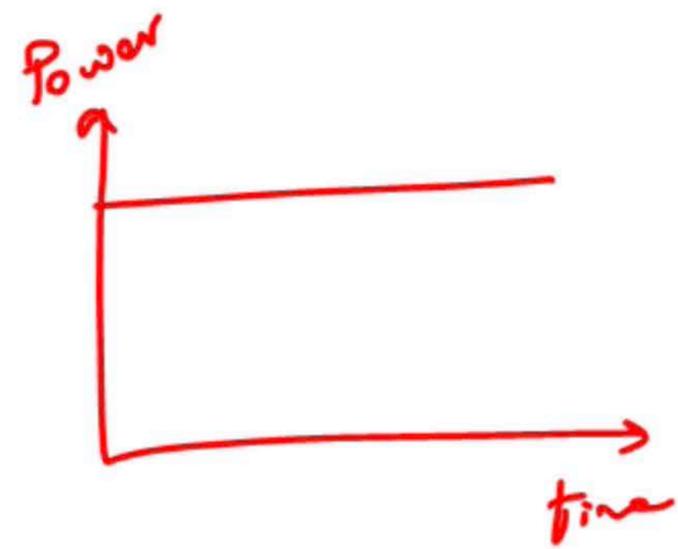
$$\begin{aligned}
 \vec{D} &= \epsilon_0 \epsilon_r \vec{E} && \text{Electronic susceptibility} \\
 &= \epsilon_0 (1 + \chi) \vec{E} \\
 &= \epsilon_0 \vec{E} + \vec{P} && \text{Polarization}
 \end{aligned}$$

Capture Effects Tools Help

Duration: 1:33:18

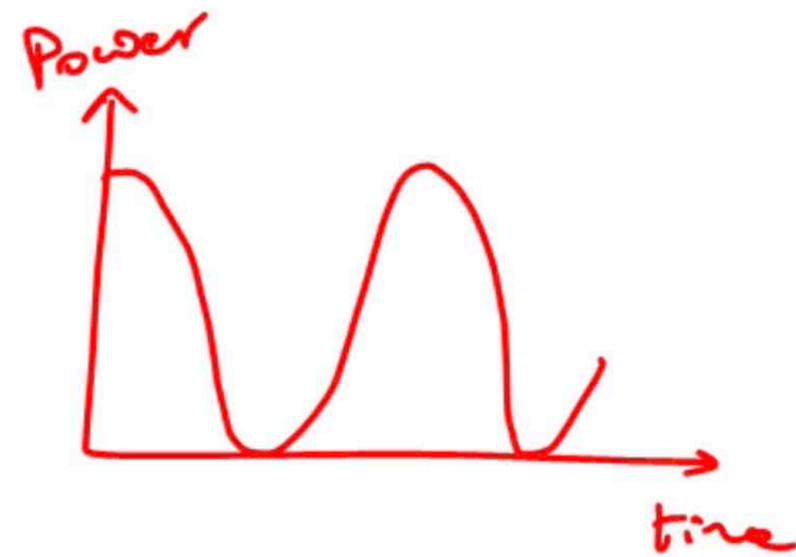
Audio

Delete Pause Stop



Polarization
RF Waves
Acoustic waves

②



① Polarization :

For an EM wave propagating in +z direction

$$\vec{E}(x, y, z, t) = (\hat{a}_x E_x + \hat{a}_y E_y e^{j\phi}) e^{j(\omega t - \beta z)}$$

① Polarization : For an EM wave propagating in +z direction

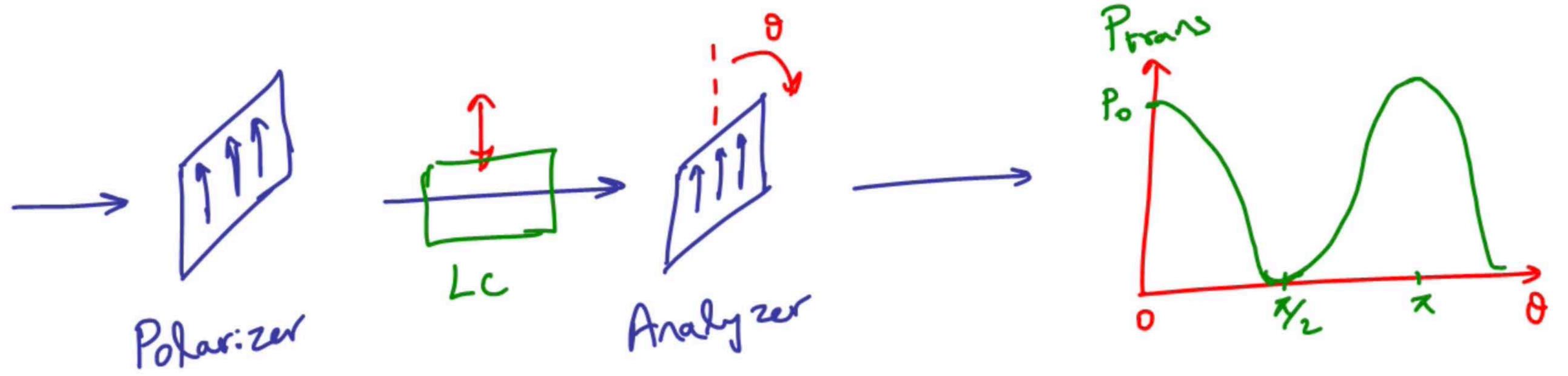
$$\vec{E}(x, y, z, t) = (\hat{a}_x E_x + \hat{a}_y E_y e^{j\phi}) e^{j(\omega t - \beta z)}$$

If $\phi = 0 \Rightarrow$ Linear polarization
($E_x = E_y \Rightarrow \theta = 45^\circ$)

If $\phi = \pm \pi/2 \Rightarrow$ Circular polarization

$$E_x = E_y$$

Otherwise \Rightarrow Elliptical polarization



Malus's law

$$P_0 \cos^2 \theta$$

