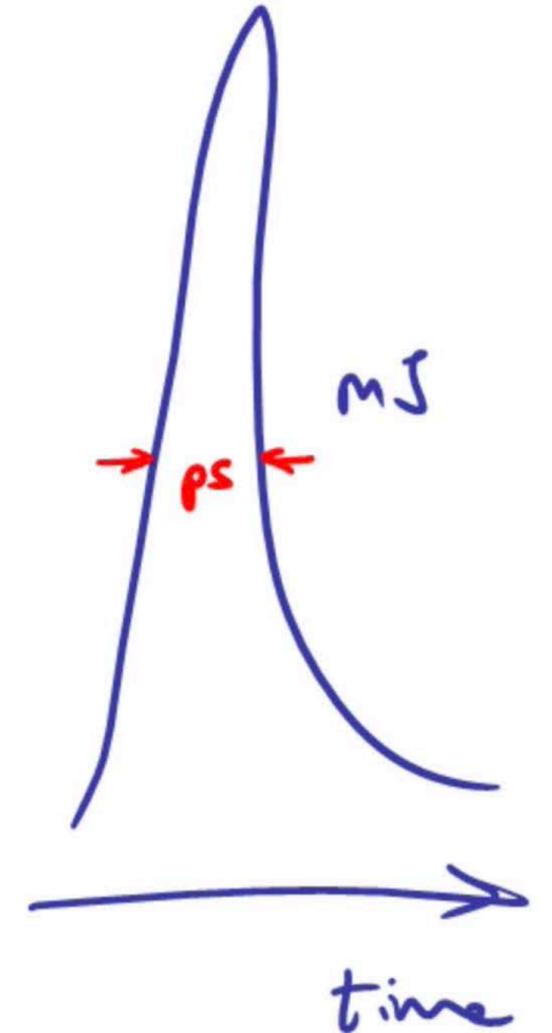
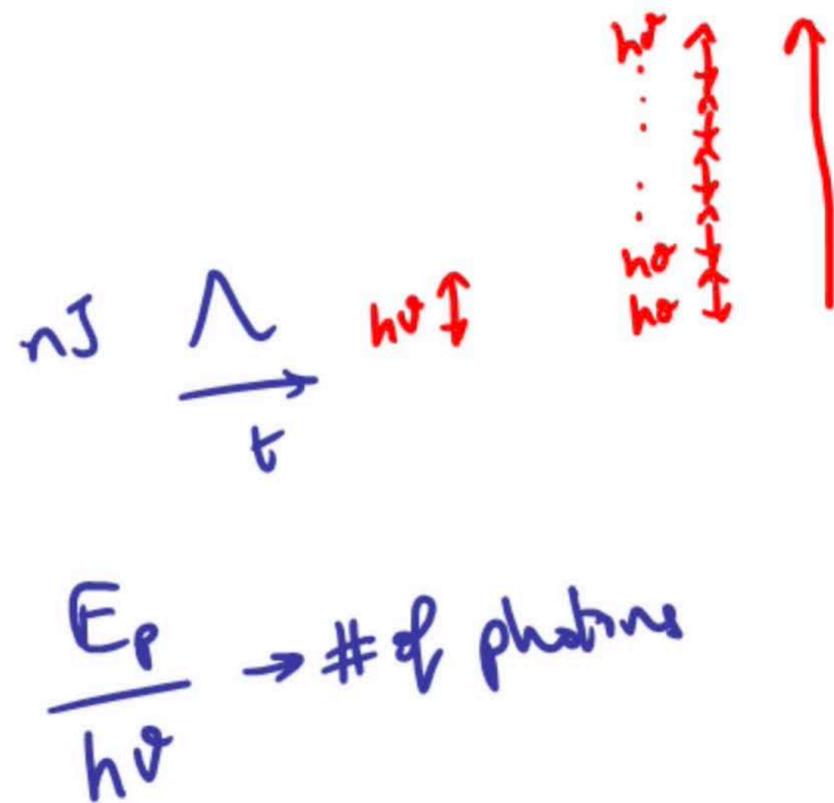


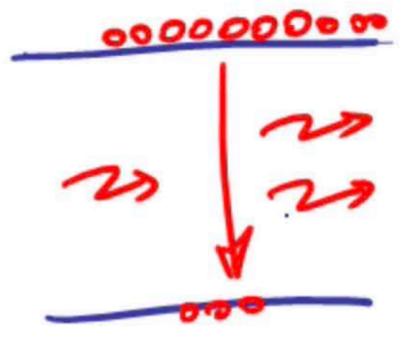
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$$N W_i = R - \frac{1}{2\tau_{21}} (N + N_a) \Rightarrow$$

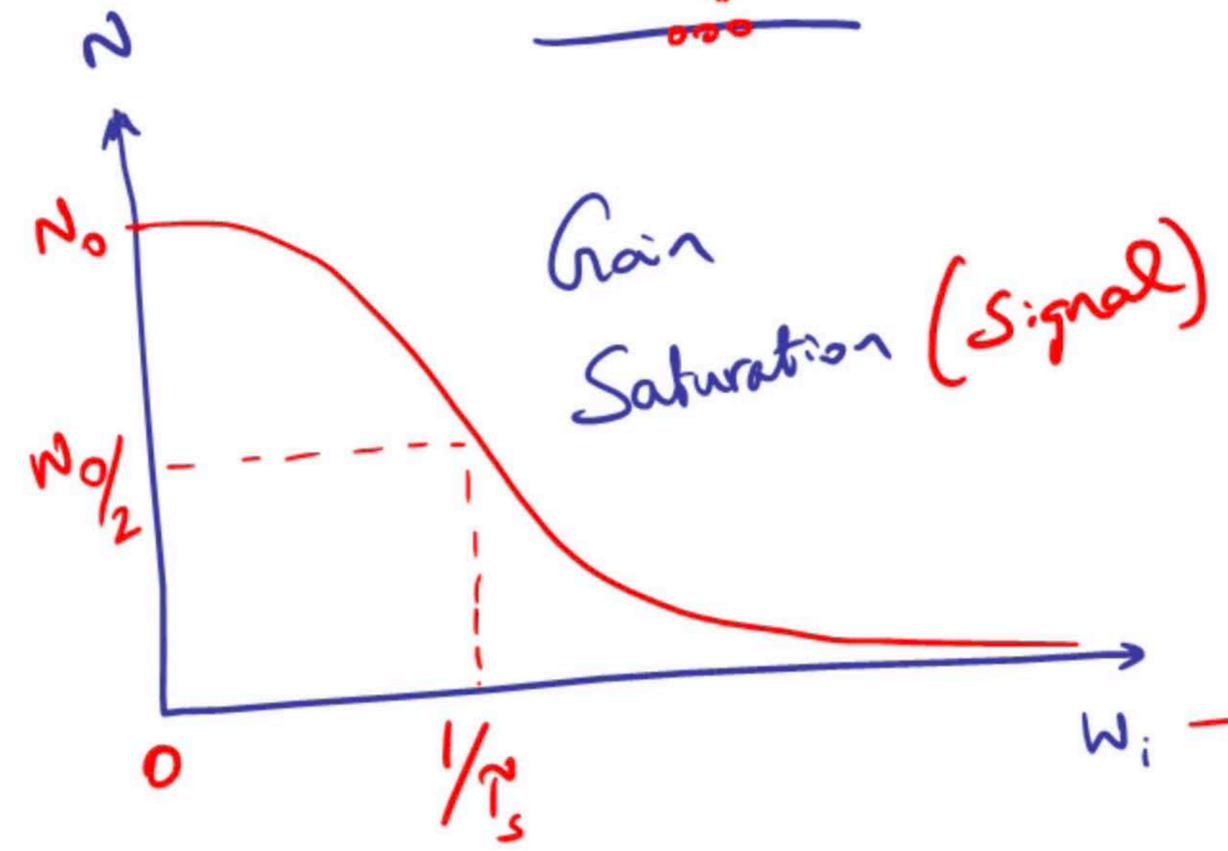
$$N = \frac{2\tau_{21}R - N_a}{2\tau_{21}W_i + 1}$$



$$N = \frac{N_0}{1 + \tau_s W_i}$$

where $\tau_s = 2t_{sp}$

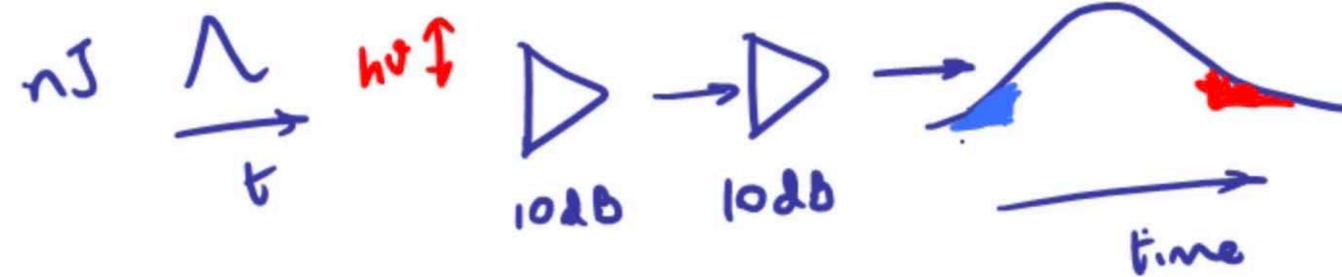
$$N_0 = 2Rt_{sp} - N_a$$



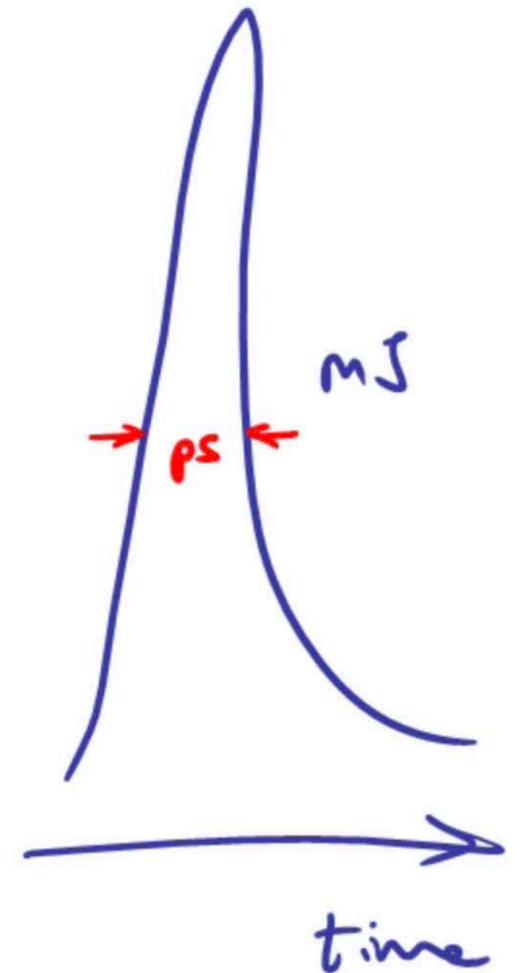
flux density of incoming signal photons $\rightarrow \phi_s \sigma$

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$$\frac{E_p}{h\nu} \rightarrow \# \text{ of photons}$$



Tutorial Session on Ray Optics & Wave Optics:

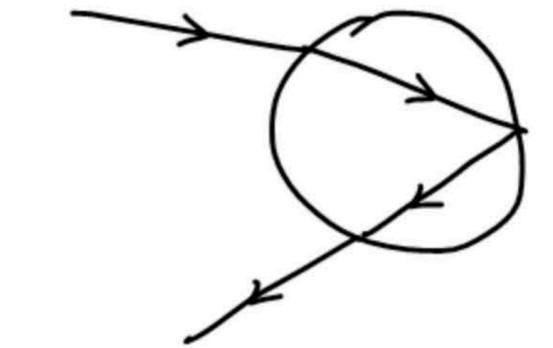
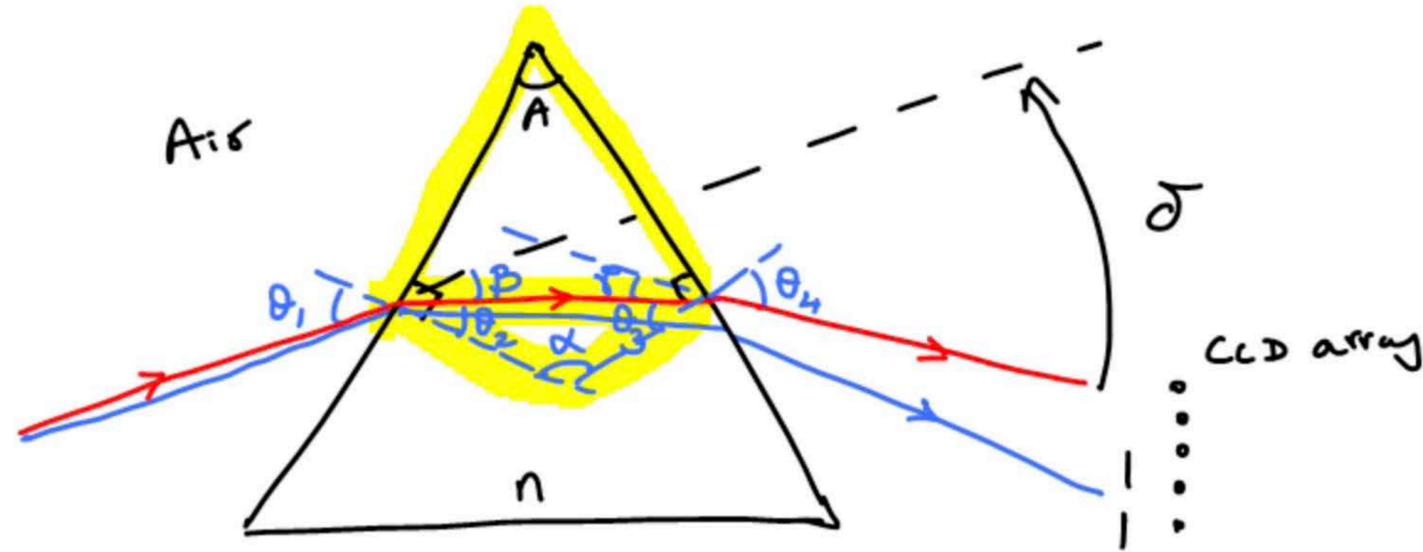
Example 1: Dispersion in a prism (min) $\lambda \rightarrow \frac{c}{n(\lambda)}$ \rightarrow velocity of light within a medium

$$n_{\text{blue}} = 1.34$$

$$n_{\text{red}} = 1.33$$

Paraxial approximation

$$n_1 \theta_1 = n_2 \theta_2$$



$$\delta = (n-1)A$$

$$A = 10^\circ$$

$$\delta_{\text{red}} = (1.33 - 1)10^\circ = 3.3^\circ$$

$$\delta_{\text{blue}} = (1.34 - 1)10^\circ = 3.4^\circ$$

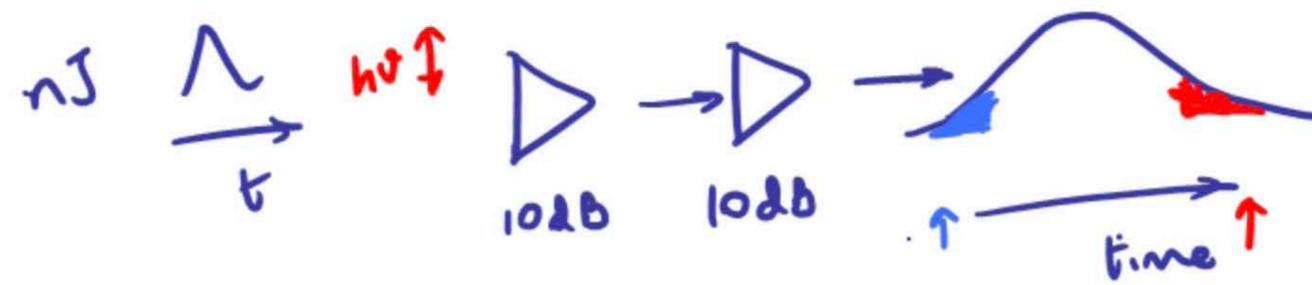
$$\Rightarrow 0.1 \text{ deg}$$

$$\left. \begin{aligned} \alpha + A &= 180^\circ \\ \theta_2 + \theta_3 + \alpha &= 180^\circ \end{aligned} \right\} \Rightarrow A = \theta_2 + \theta_3$$

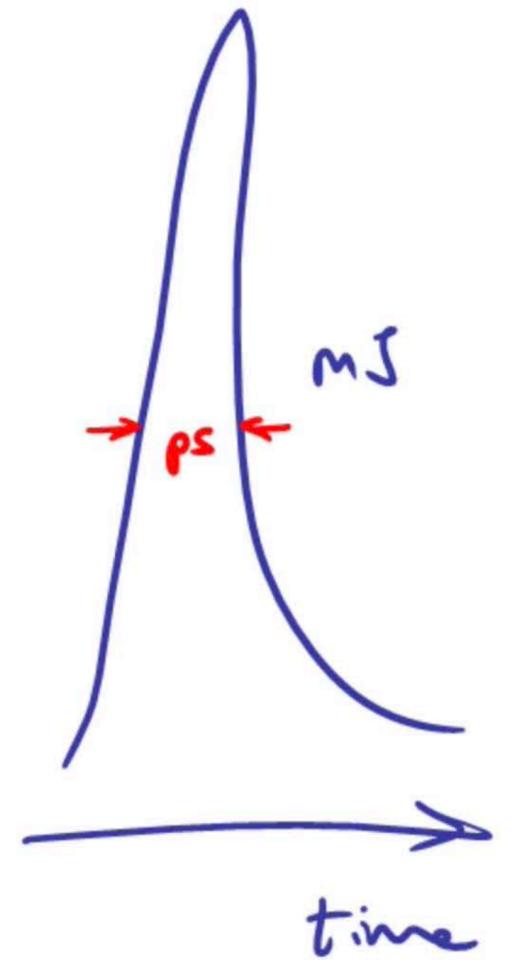
$$\begin{aligned} \delta = \beta + \gamma &= \theta_1 - \theta_2 + \theta_4 - \theta_3 = \theta_1 + \theta_4 - A \\ &= n\theta_2 + n\theta_3 - A = (n-1)A \end{aligned}$$

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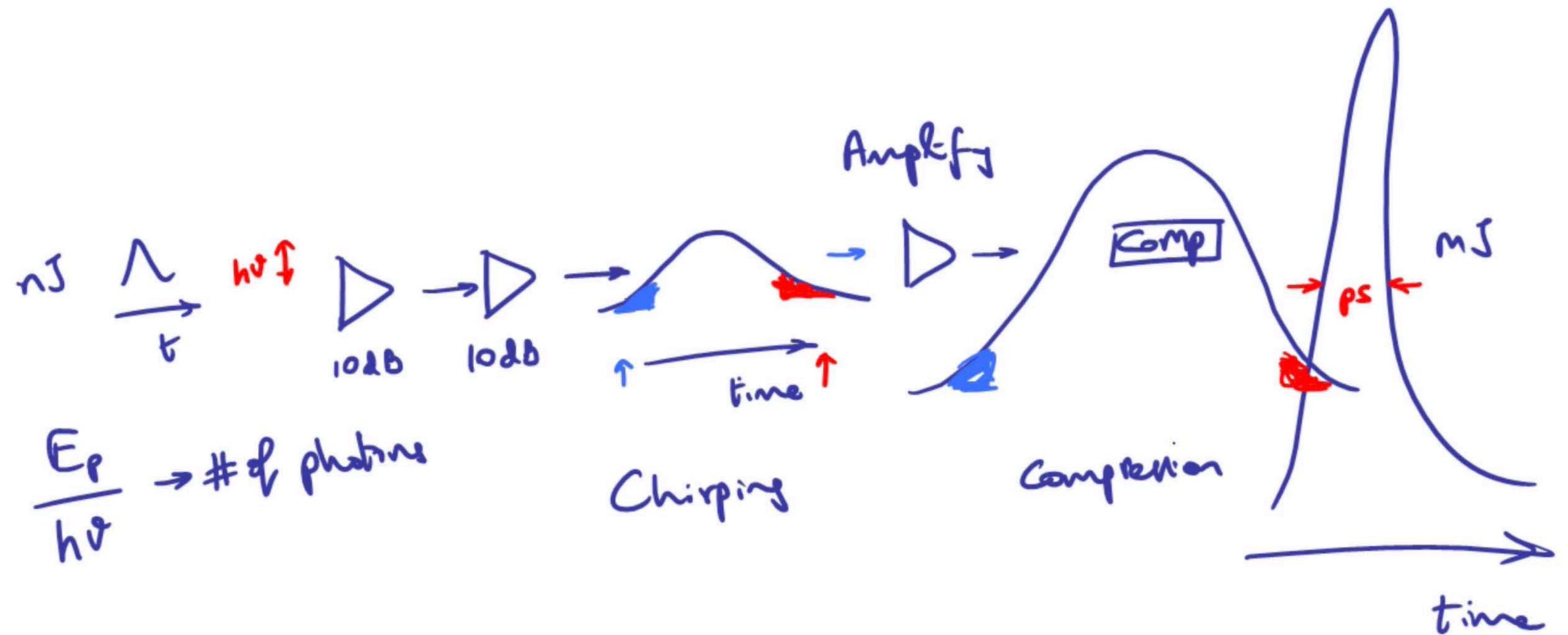


$$\frac{E_p}{h\nu} \rightarrow \# \text{ of photons}$$



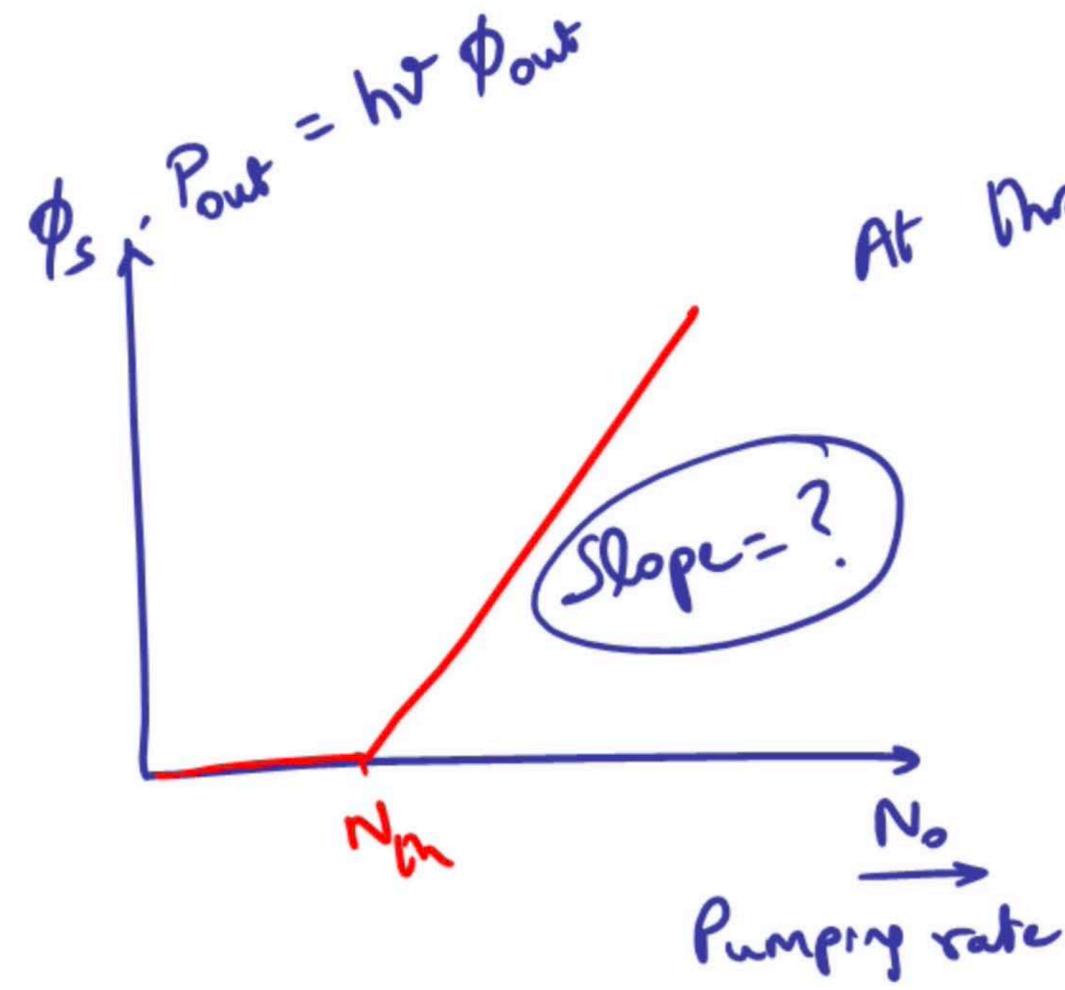
Chirped Pulse Amplification

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$$\frac{r_0(\nu)}{1 + \phi_s(\nu)/\phi_{sat}} = \alpha_r \Rightarrow$$

$$\phi_s(\nu) = \begin{cases} \phi_{sat} \left[\frac{r_0(\nu)}{\alpha_r} - 1 \right] & r_0(\nu) > \alpha_r \\ 0 & r_0(\nu) \leq \alpha_r \end{cases}$$

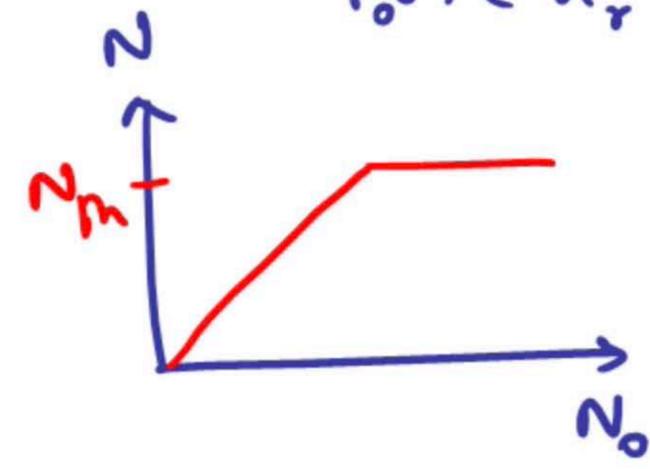


At threshold,

Photon flux $\phi_s(\nu)$

$$N_m \cdot \sigma(\nu) = \alpha_r$$

$$\phi_s(\nu) = \begin{cases} \phi_{sat} \left(\frac{N_0}{N_m} - 1 \right) & N_0 > N_m \\ 0 & N_0 \leq N_m \end{cases}$$

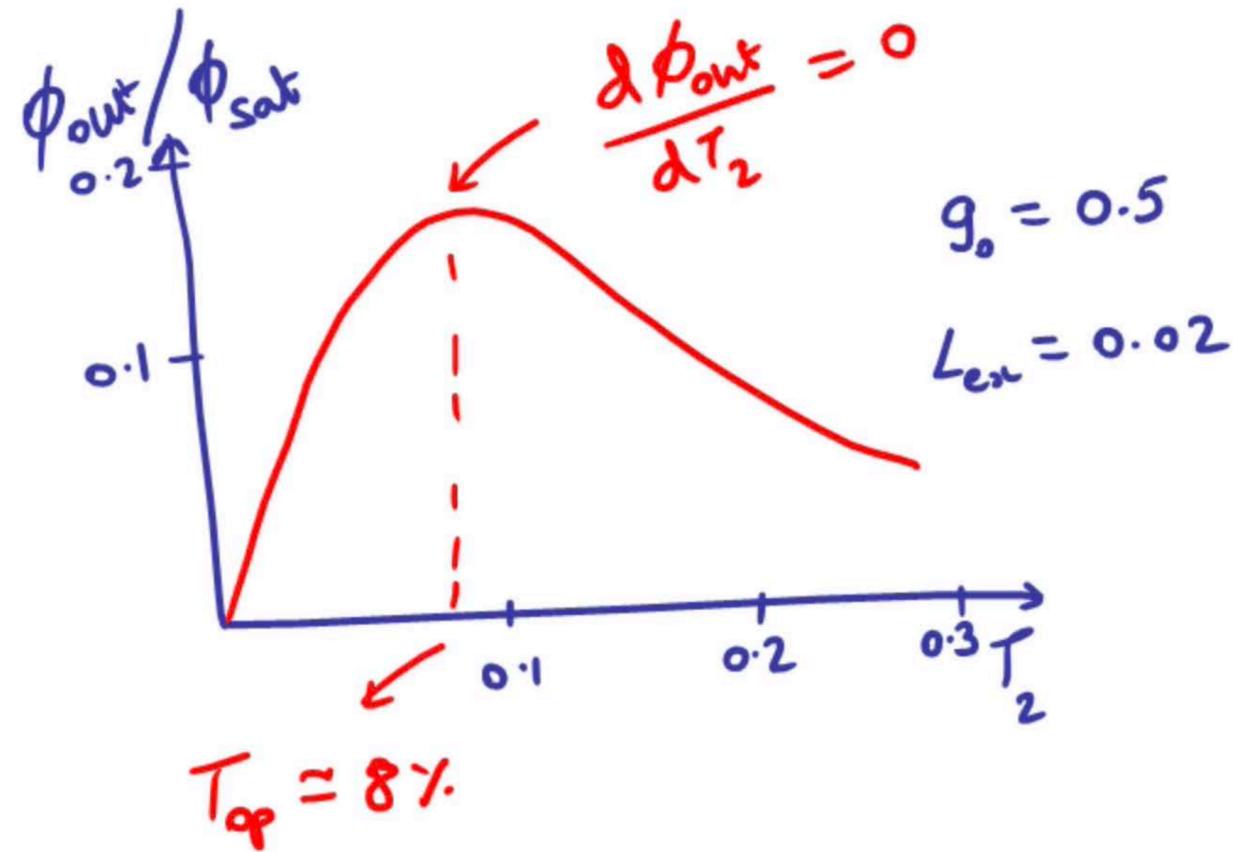


$$N_0 > N_m$$

$$N_0 \leq N_m$$

Optimization of Output Coupling.

Assume $R_1 = R_2$. $\phi_{out} = \frac{\phi_s}{2} \cdot T_2$



$$= \frac{\phi_{sat} T_2}{2} \left(\frac{g_0}{\alpha_r} - 1 \right)$$

$$= \frac{\phi_{sat} T_2}{2} \left[\frac{g_0 \cdot 2L}{L_{ex} - \ln(1-T_2)} - 1 \right]$$

$\frac{d\phi_{out}}{dT_2} = 0$ & when $T_2 \ll 1$

$$\ln(1-T_2) \approx -T_2$$

$$T_{op} = (g_0 L_{ex})^{1/2} - L_{ex}$$

$g_0 = g_0 \cdot 2L$
Gain factor

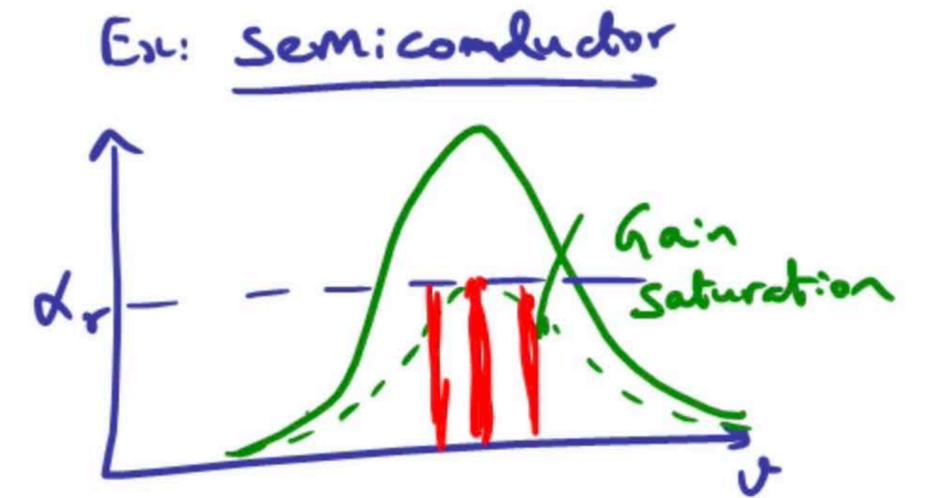
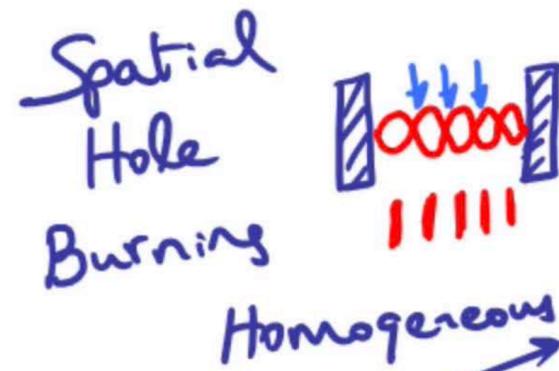
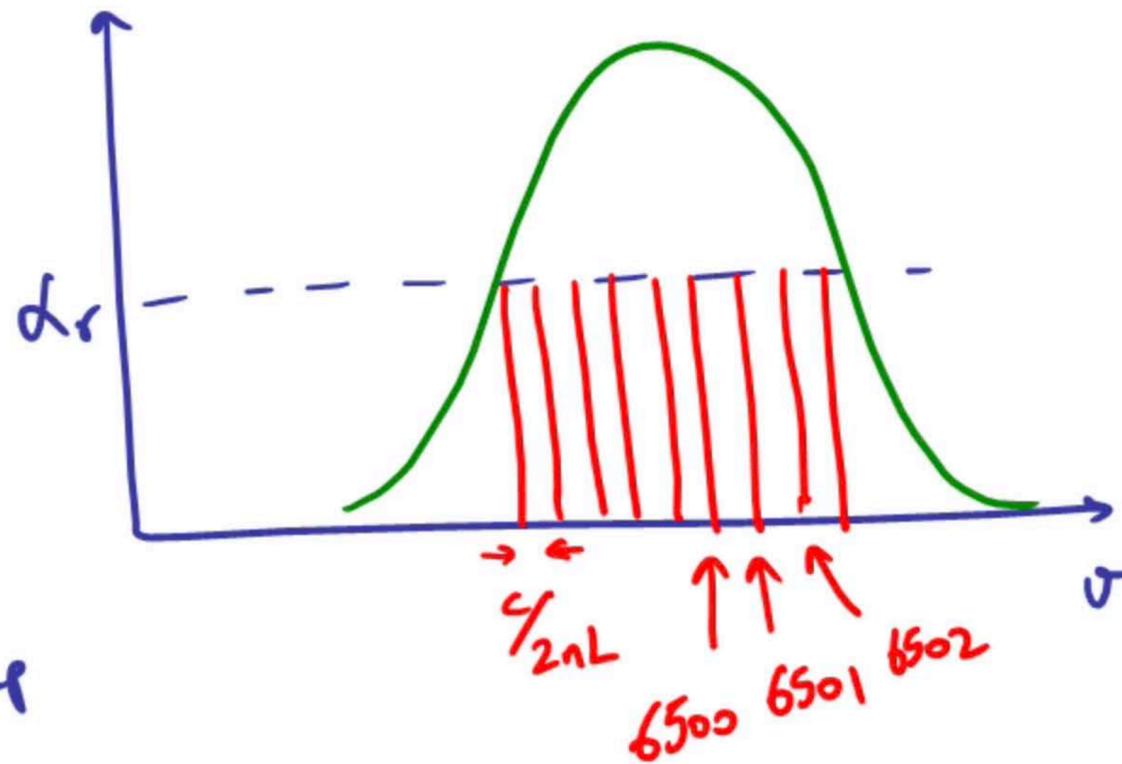
$$\alpha_r = \alpha_{int} + \alpha_{m1} + \alpha_{m2}$$

$$= \alpha_L + \frac{1}{2L} \ln\left(\frac{1}{R_2}\right)$$

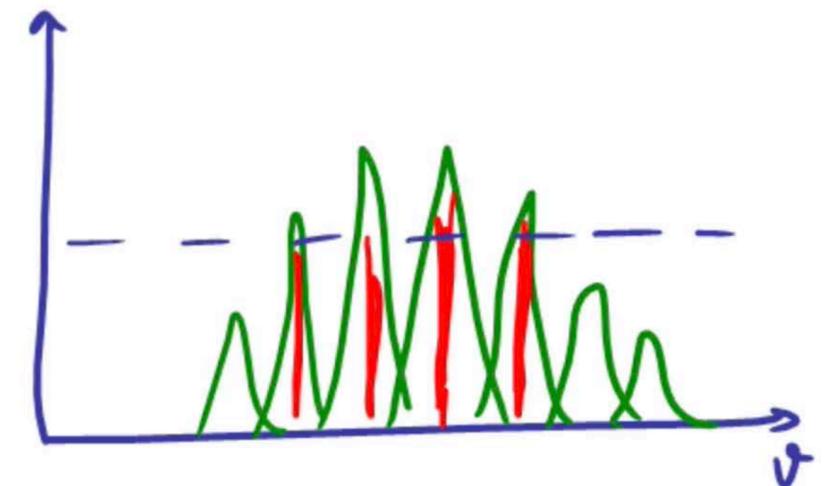
$$= \alpha_L - \frac{1}{2L} \ln(1-T_2)$$

$$= \frac{1}{2L} [L_{ex} - \ln(1-T_2)]$$

$$L_{ex} = 2L (\alpha_{int} + \alpha_{m1})$$



Inhomogeneous



Ex: Nd: glass

