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# SOIL MECHANICS/GOTECHNICAL ENGINEERING I

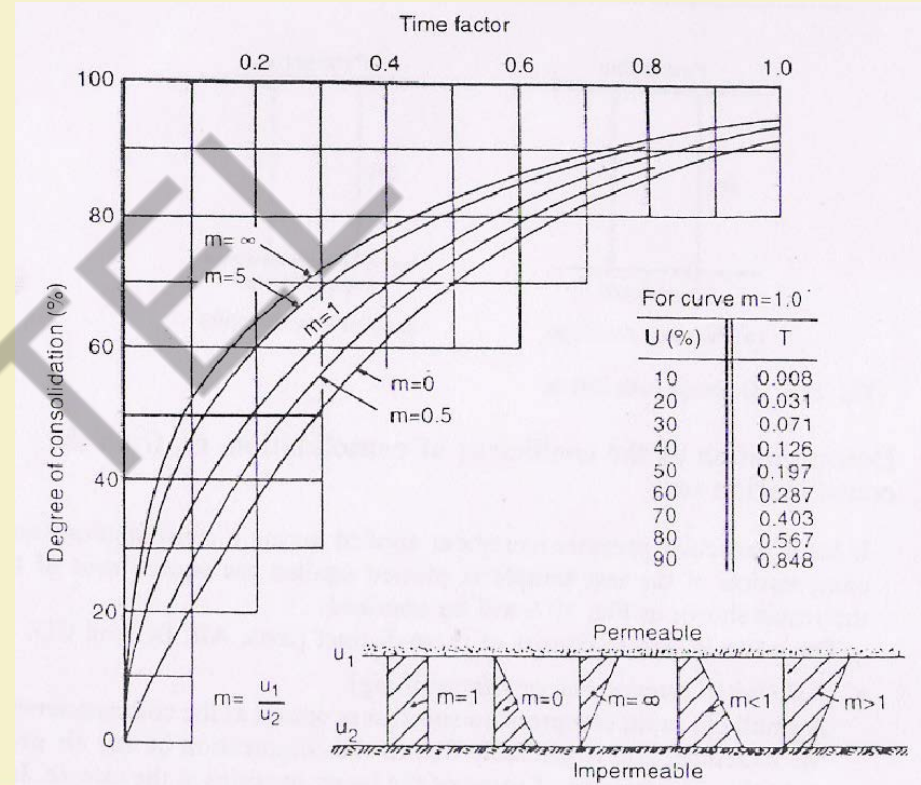
## COMPRESSIBILITY OF SOILS

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# COMPRESSIBILITY OF SOILS

$$U = 1 - \sum_{m=0}^{m=\infty} \frac{2}{M^2} e^{-M^2 T}$$

This is the relationship  
between U and T



# COMPRESSIBILITY OF SOILS

U%	0	10	20	30	40	50	60	70	80	90
T	0	0.008	0.031	0.071	0.126	0.197	0.287	0.405	0.565	0.48

T versus U data can be fitted approximately in two parts. U between 0 and 60% it can be fitted by the following equation

$$T = \frac{\pi}{4} \left( \frac{U\%}{100} \right)^2$$

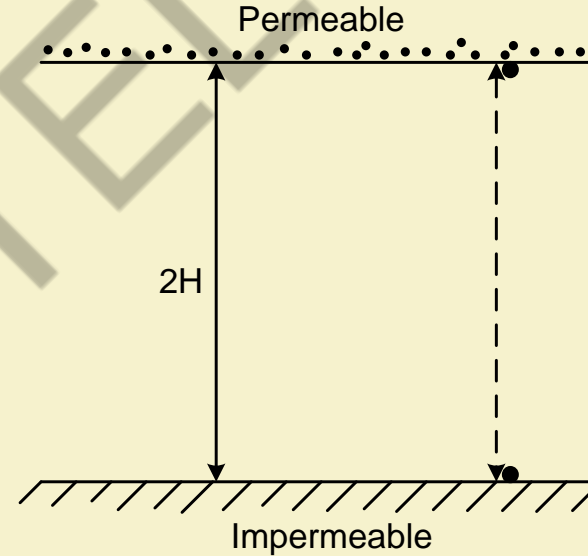
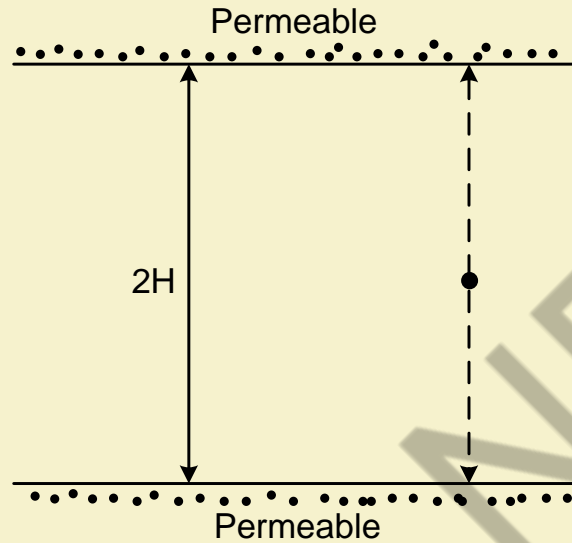
And the same can fitted for U between 60 and 100% by the following equation

$$T = 1.781 - 0.933 \log_{10}(100 - U\%)$$

# COMPRESSIBILITY OF SOILS

If the soil above and below the consolidating layer are pervious, the water under pressure in the layer will travel either upwards or downwards. This case is known as two-way drainage and the length of the drainage path, i.e., the maximum length that a water particle needs to travel for dissipating pore pressure from the consolidating layer = Thickness of the layer /2 =  $H$

# COMPRESSIBILITY OF SOILS

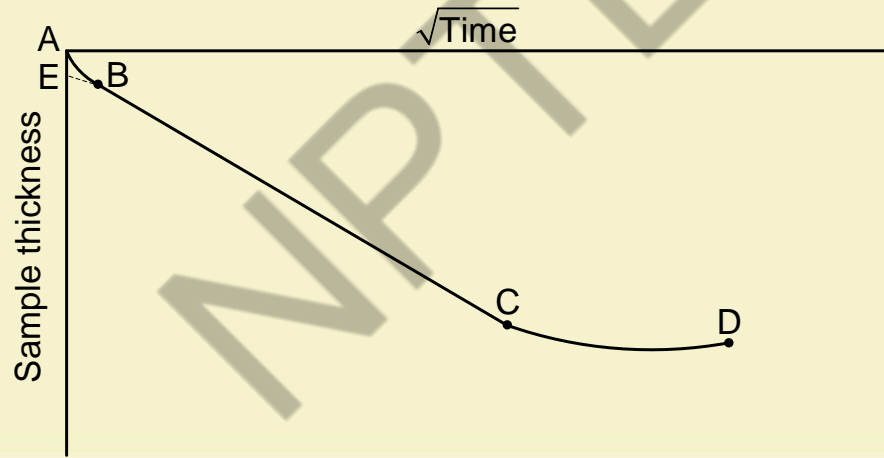


# COMPRESSIBILITY OF SOILS

If one of the soil layers either above or below the consolidating layer is impervious, water will travel in one direction and the case is known as one way drainage. The length of drainage path, i.e., the longest path a water particle need to travel for dissipating pore pressure for this case is  $H$

# COMPRESSIBILITY OF SOILS

If for a particular pressure increment applied during a consolidation test the compression of the test sample is plotted against the square root of time, the result shown in Figure in the next slide will be obtained.



# COMPRESSIBILITY OF SOILS

The curve is seen to consist of three distinct parts: AB, BC and CD

1. AB (Initial Compression or Frictional lag): A small but rapid compression sometimes occurs at the commencement of the increment and is probably due to the compression of any air present or to reorientation of some of the larger particles in the sample. In the majority of tests this effect is absent and points A and B are coincident. Initial compression is not considered to be due to any loss of water from the soil and should be treated as a zero error for which a correction is made



# COMPRESSIBILITY OF SOILS

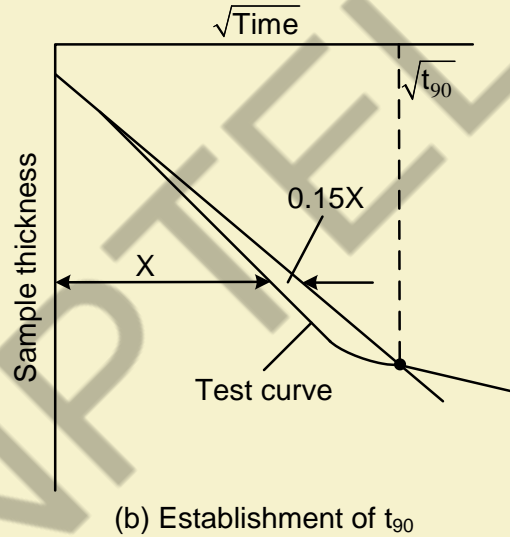
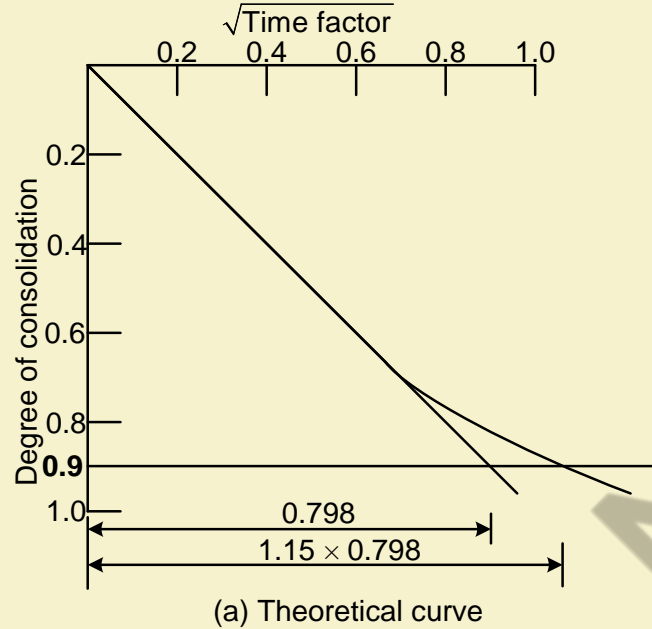
2. BC Primary compression: All the compression in this part of the curve is taken as being due to the expulsion of water from the sample, although some secondary compression will also occur. When the pore pressure has been reduced to a negligible amount it is assumed that 100 percent consolidation has been attained
3. CD (Secondary compression): The amount by which this effect is evident is a function of the test conditions and can hardly be related to an insitu value

# COMPRESSIBILITY OF SOILS

To evaluate the coefficient of Consolidation it is necessary to establish the point C corresponding to 100% consolidation, but it is difficult from a study of the test curve to fix C with accuracy and a procedure in which the test curve is fitted to the theoretical curve becomes necessary

Method by Taylor (1948): If the theoretical curve  $U$  against  $\sqrt{t}$  is plotted for the case of a uniform initial excess pore pressure distribution, the curve will be like that shown in the fig a in the next slide. Up to values of  $U$  equal to about 60 percent, the curve is a straight line of equation  $U = 1.13\sqrt{t}$ , but if this straight line is extended to cut the ordinate  $U = 90$  percent the abscissa of the curve is seen to be 1.15 times the abscissa of the straight line. This fact is used to fit the test and theoretical curves

# COMPRESSIBILITY OF SOILS



# COMPRESSIBILITY OF SOILS

With the test curve a corrected zero must first be established by projecting the straight line part of the primary compression back to cut the vertical axis at E. A second line starting through E is now drawn such that all abscissas on it are 1.15 the corresponding values on the laboratory curve, and the point at which this second line cuts the laboratory curve is taken to be the point representing 90 percent primary consolidation.

To obtain  $c_v$ ,  $T_{90}$  is first found from the theoretical curve that fits the drainage conditions,  $t_{90}$  is determined from the test curve.

# COMPRESSIBILITY OF SOILS

$$t_{90} = \frac{T_{90}H^2}{c_v}$$

Time factor corresponding to 90 percent degree of consolidation is 0.48

Hence 
$$t_{90} = \frac{0.48H^2}{c_v}$$

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# COMPRESSIBILITY OF SOILS

Coefficient of consolidation by log of time method: Similarity between  $\log T$  vs  $U$  curve and sample thickness vs  $\log t$  is observed (shown in the next slide). Hence sample thickness versus  $\log$  plot can be utilised to determine the coefficient of consolidation.

Determination of thickness corresponding to 100% consolidation: The intersection formed by the final straight line produced backward and the tangent to the curve at point of inflection is accepted as the 100% primary consolidation point and the dial reading designated as  $R_{100}$



# COMPRESSIBILITY OF SOILS

Determination of thickness corresponding to 0% primary consolidation:

Step 1: select two points on the initial parabolic portion of the curve in such a way that time are in the ratio of 1:4

Step 2: The difference in thickness between these two points is then equal to the difference between the first point and the dial reading corresponding to zero primary consolidation. If  $z$  is the ordinate difference between A and B, a point C will be chosen at  $z$  above point B. Intersecting the horizontal through point C to Dial reading axis gives the point corresponding to zero primary consolidation

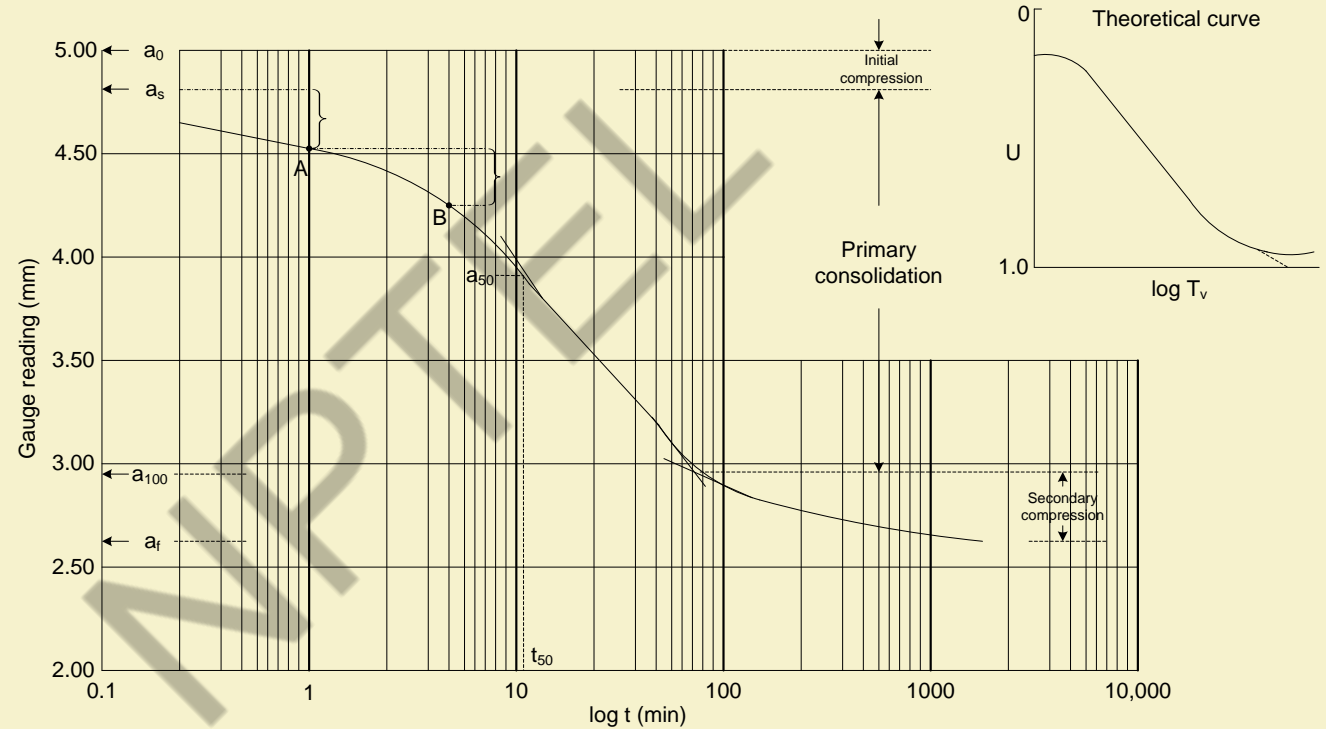
# COMPRESSIBILITY OF SOILS

Step 3: The interval between 0 and 100% consolidation is divided into equal intervals of percent consolidation. Since it has been found that the laboratory and the theoretical curves have better correspondence at the central portion, the value of  $c_v$  is computed by taking the time  $t$  and time factor  $T$  at 50% consolidation.

$$T_{50} = \frac{c_v t_{50}}{H^2} \quad \text{Or} \quad c_v = \frac{T_{50} H^2}{t_{50}}$$

# COMPRESSIBILITY OF SOILS

Coefficient of consolidation by log of time method



# COMPRESSIBILITY OF SOILS

If two layers of the same clay soil with different drainage path  $H_1$  and  $H_2$  are acted upon by the same pressure increase and reach the same degree of consolidation in times  $t_1$  and  $t_2$  respectively, then theoretically their coefficients of consolidation must be equal as must their time factor  $T_1$  and  $T_2$

$$T_1 = \frac{c_{v1} t_1}{H_1^2}$$

$$T_2 = \frac{c_{v2} t_2}{H_2^2}$$

Equating: 
$$\frac{t_1}{H_1^2} = \frac{t_2}{H_2^2}$$

# COMPRESSIBILITY OF SOILS

## Important terminology and its implication:

Coefficient of volume compressibility,  $a_v$  or  $a_v = \frac{de}{dp}$  = slope of  $e$  versus  $\log p$  plot ( $m^2/kN$ )

$m_v = \text{coefficient of volume compressibility} = \frac{a_v}{1 + e}$  (unit same as  $a_v$ ,  $m^2/kN$ )

$$m_v = \frac{dH}{H_1} \frac{1}{dp} = \frac{1}{H_1} \frac{dH}{dp}$$

$$\text{total settlement} = \rho_c = m_v dp H$$

# COMPRESSIBILITY OF SOILS

$$\frac{dH}{H_1} = \frac{de}{1 + e_1}$$

Where  $H_1$  is the original thickness and  $e_1$  is the initial void ratio

$$e = \frac{H - H_s}{H_s}$$

$$c_c = \frac{e_1 - e_2}{\log\left(\frac{p_2}{p_1}\right)}$$

Approximate value of  $c_c$   $c_c = 0.009(w_L - 10)$

$$\rho_c = \frac{c_c H_1}{1 + e_1} \log_{10} \frac{p_2}{p_1}$$

Normally consolidated clay

# COMPRESSIBILITY OF SOILS

Over consolidated – when  $\sigma_c'$  is larger than  $\sigma_0'$ , the clay is known to be overconsolidated

$$\sigma_0' + \Delta\sigma < \sigma_{pc}' \quad \rho_c = \frac{c_r H}{1 + e_0} \log_{10} \left( \frac{\sigma_0' + \Delta\sigma}{\sigma_0'} \right)$$

$$\sigma_0' + \Delta\sigma > \sigma_{pc}' \quad \rho_c = \frac{c_r H}{1 + e_0} \log_{10} \left( \frac{\sigma_{pc}'}{\sigma_0'} \right) + \frac{c_c H}{1 + e_0} \log_{10} \left( \frac{\sigma_0' + \Delta\sigma}{\sigma_{pc}'} \right)$$

# COMPRESSIBILITY OF SOILS

Time factor,  $T = \frac{c_v t}{H^2}$

$$T = \frac{\pi}{4} \left( \frac{U\%}{100} \right)^2 \quad \text{For } U < 60\%$$

$$T = 1.781 - 0.933 \log_{10}(100 - U\%) \quad \text{For } U > 60\%$$

U is the degree of consolidation = consolidation attain at time t / total expected consolidation settlement,  $c_v$  is the coefficient of consolidation, H is half the thickness of the layer for double drainage and thickness of the layer for single drainage



# COMPRESSIBILITY OF SOILS

Determination of  $c_v$ :

1. Taylor's root time method: determine  $t_{90}$  from the plot and procedure proposed by Taylor and determine

$$c_v = \frac{0.48H^2}{t_{90}}$$

2. Casagrande's log time method: determine  $t_{50}$  from the plot and following the procedure proposed by Casagrande and determine

$$c_v = \frac{0.197H^2}{t_{50}}$$

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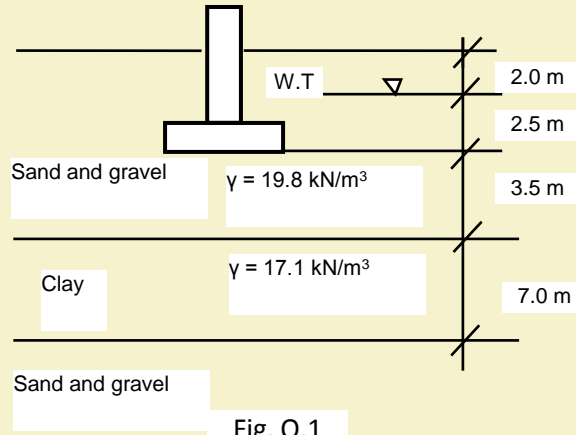
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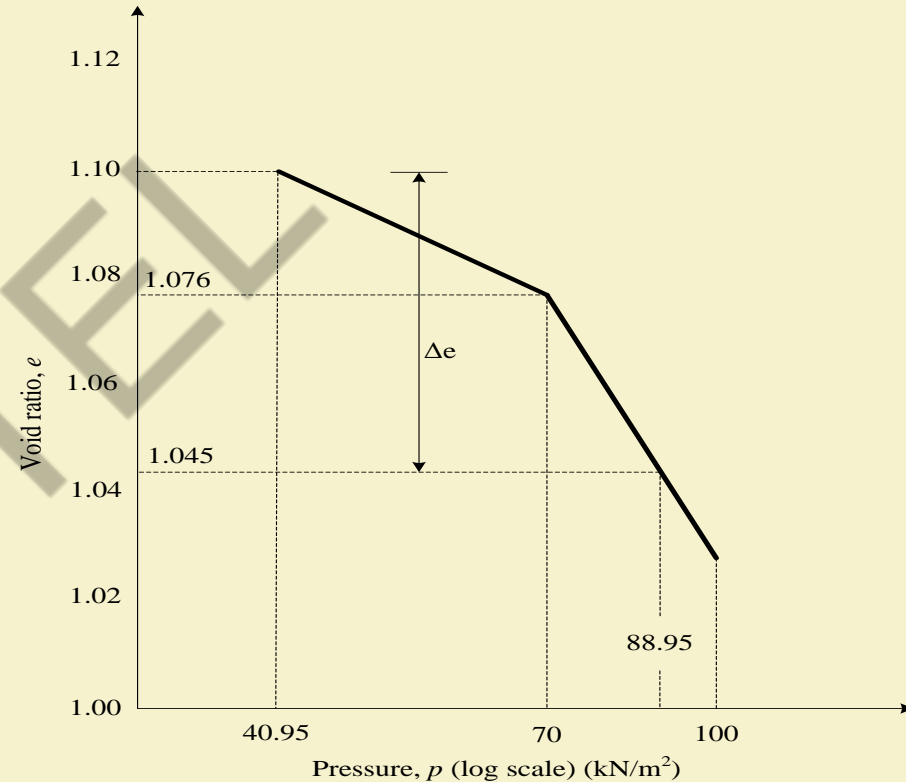
# COMPRESSIBILITY OF SOILS



A foundation is to be constructed at a site where the soil profile is as shown in Fig. Q. 1. The base of the foundation is 2.5m by 2.5m and, it exerts a total load of 2000 kN, which includes the weight of the structure, foundation and soil surcharge on the foundation. The initial void ratio and compression index of the compressible clay layer is respectively, 1.2 and 0.60. Determine the settlement of the foundation due to the primary consolidation of the clay layer.

# COMPRESSIBILITY OF SOILS

A 10 m thick clay layer has a saturated unit weight of  $18 \text{ kN/m}^3$  and void ratio of 1.1. The water table is at the ground surface. Laboratory consolidation test is conducted on a specimen collected from the middle of the clay layer. The field consolidation curve interpolated from the laboratory test results is shown in the figure. Determine the consolidation settlement if 2 by 2 m footing constructed on the surface of the clay layer with a load (i) 1000 kN and (ii) 1800 kN



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During a pressure increment a consolidation test sample attained 25 per cent primary consolidation in 5 minutes with a mean thickness of 18 mm. How long would it take a 20 m thick layer of the same soil to reach the same degree of consolidation if (i) the layer was drained on both surfaces and (ii) it was drained on the top surface only?

# COMPRESSIBILITY OF SOILS

**A 19.1 mm thick clay sample, drained both at top and bottom, reached 30 percent consolidation in 10 minutes. How long would it take the sample to reach 50 per cent consolidation?**

# COMPRESSIBILITY OF SOILS

Results obtained from a consolidation test on a clay sample for a pressure increment of 100 – 200 kN/m<sup>2</sup> were:

Determine the coefficient of Consolidation of the soil

Thickness of the sample(mm)	Time (min)
12.200	0
12.141	0.25
12.108	1.0
12.075	2.25
12.046	4
11.985	9
11.922	16
11.865	25
11.827	36
11.809	49
11.800	64

# COMPRESSIBILITY OF SOILS

How long would a layer of this clay, 10 m thick and drained on its top surface only, take to reach 75 per cent primary consolidation?

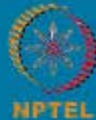
If the void ratios at the beginning and end of the increment were 0.94 and 0.82 respectively, determine the value of the coefficient of permeability

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# COMPRESSIBILITY OF SOILS

In an oedometer test, a clay specimen initially 25 mm thick attains 90% consolidation in 10 minutes. In the field, the clay stratum from which the specimen was obtained has a thickness of 6.0 m and sandwiched between two sand layers. For a structure constructed on this clay layer, the ultimate settlement is estimated as 200 mm. Estimate the settlement at the end of 100 days after construction.

# COMPRESSIBILITY OF SOILS

A reasonably homogeneous layer of clay, 4 m thick, is expected to experience an ultimate settlement of 160 mm. After 3 years the average settlement was measured to be 55 mm. How long will it take for the average settlement to double (110 mm)?



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